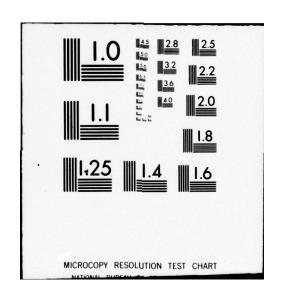
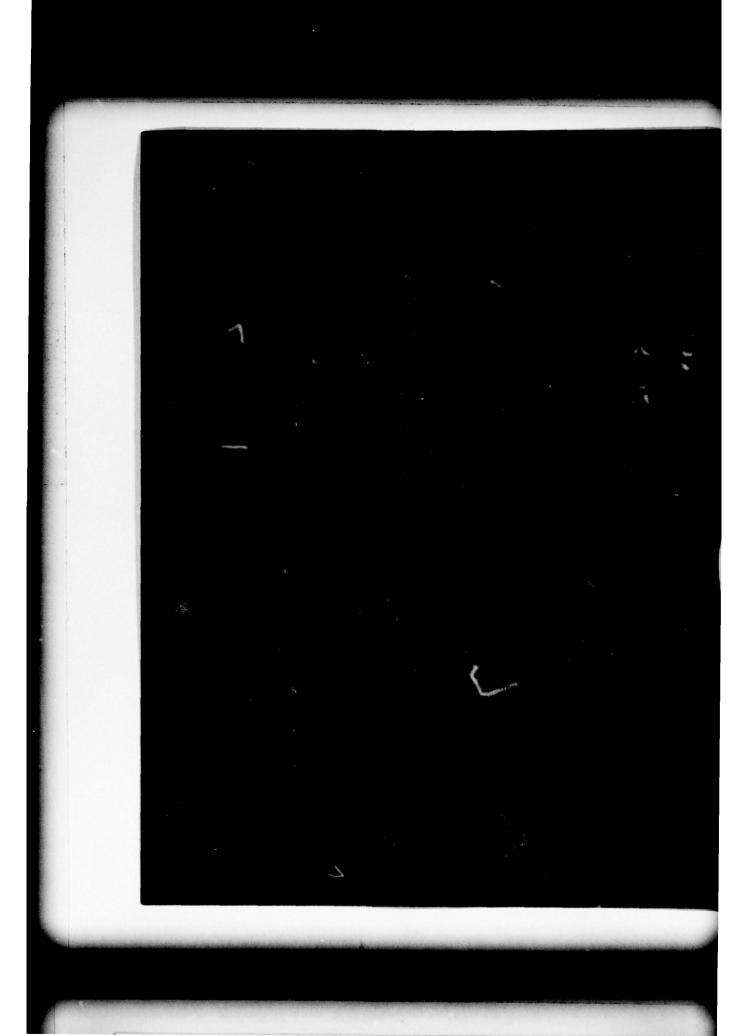
AD-A079 549 NAVAL RESEARCH LAB WASHINGTON DC SHOCK AND VIBRATION--ETC F/G 20/11 THE SHOCK AND VIBRATION DIGEST. VOLUME 11, NUMBER 12, (U) DEC 79 J NAGLE-ESHLEMAN UNCLASSIFIED NL 1 OF 2 AD A 079549



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# SVIC NOTES

With this issue we complete another year and come to the end of a decade. This is the Annual Index issue. It is, in effect, a measure of our accomplishments in the DIGEST during the past year. Look at it critically with a view to guiding us in our future efforts. Our goal is to provide a useful current awareness journal in the shock and vibration field. Any suggestions on how this can become a better publication would be most welcome. Furthermore, if you see an item or an article in the DIGEST which you consider wrong, or your viewpoint differs from that of the author, let us know about it. Letters to the Editor are often the beginning of fruitful interchange.

It seems appropriate to look at some highlights of SVIC activities during 1979. Our "International Survey of Shock and Vibration Technology" was published and seems to have been well received. This survey is being extended to countries not covered in the original effort. The 49th Shock and Vibration Bulletin has been printed and distributed. The 50th Symposium in Colorado Springs was a definite success, with about 325 in attendance. Our thanks to the hosts – the Air Force Flight Dynamics Laboratory and the U.S. Air Force Academy – for providing the support to make this possible. As you read this column, SVM-11 – a monograph on calibration of shock and vibration transducers – will be available. A monograph on the balancing of rotating machinery is expected to be available before the end of the fiscal year. All of these publications may be purchased from SVIC.

In September, I had the privilege of serving as Acting Chairman of Committee TC108 of the International Standards Organization in Moscow. This committee is concerned with international standards on vibration and shock. At the Moscow meeting, I was able to establish dialogue with several Soviet experts on shock and vibration with a view to opening direct channels for interchange on technical matters of mutual interest. The prospects are promising and I will keep DIGEST readers informed on any significant progress.

Plans are afoot to establish a stronger link between SVIC and other DoD information analysis centers. Details are not yet worked out, but direct discussions within the IAC community on goals, methods of operation, and mutual problems should result in better information service from all sources. This becomes increasingly important with the realization that timely availability of technical information plays an important role in the new thrusts to spur innovation and increase productivitity.

I am pleased to announce that Mrs. Carol Healey is assuming a principal role in customer relations at SVIC. Many of you know Carol from the symposia. She is pleasant and efficient, and now becomes your first contact relative to SVIC services and publications. I know that she will see that your needs are met.

As we close out the year, I extend my personal best wishes to all DIGEST readers for a happy holiday season and a prosperous new decade.

H.C.P.

# **EDITORS RATTLE SPACE**

#### THE PLENARY SESSION

The 50th Shock and Vibration Symposium was successful because it was well planned by the staff and technical advisory group of the SVIC. Although a full report on the meeting will appear next month, it is worthwhile to assess the value of the plenary session at this technical meeting.

A number of plenary sessions were held during the Symposium. These sessions, scheduled before the regular technical sessions, featured lectures by established shock and vibration engineers. The Elias Klein Memorial Lecture -- newly instituted by the SVIC to commemorate its founder -- was given in one plenary session. The plenary lectures -- each about one hour in length -- were used by the speakers for different purposes: technology review, prediction of future events, discussion of advanced technical concepts, and historical perspectives. Each of the four speakers selected a topic within the scope of his technical interest.

The plenary lectures provided continuity and added an atmosphere of formality to the Symposium usually evident only in the opening session — which has always been more formal than that of any other technical meeting. Not only were the plenary sessions interesting but they also contained valuable new technical information and insights not typical of technical papers.

In my opinion, the plenary sessions at the 50th Shock and Vibration Symposium provided a new and effective way for technology transfer. I hope that more engineers will have the opportunity to participate in such lectures in the near future.

R.L.E.

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#### **VEHICLE-GUIDEWAY INTERACTION PROBLEMS**

J. Genin\* and E.C. Ting\*\*

Abstract - This article discusses three general methods for studying vehicle-guideway interaction problems: moving force approximation, massless guideway approximation, and moving mass approximation. The trolley problem at the Sandia Laboratories is also summarized.

This article is an update and extension of a previous literature review on the dynamic interaction of bridge structures and vehicles [1]. The first review focused on the effects of the kinematical coupling that occurs as a vehicle traverses a flexible guideway. The mathematical difficulties of the problem were discussed, and suitable methods for analyzing the resulting boundary value problem were reviewed. A summary of the traditional modal expansion technique and an algorithm capable of handling a variety of vehicle-guideway interaction problems were also given.

Before the advent of high-speed digital computers the prime concern in studies of the vehicle-guideway interaction problem was proper treatment of the kinematical coupling term that arises in the mathematical formulation of the problem. Physically, the coupled or mixed derivative term arises when the effect of the transverse inertia of the vehicle on the dynamical properties of the system is accounted for. When this effect is considered, the resulting boundary value problem is commonly referred to as the moving mass problem.

Much of the earlier research on vehicle-guideway problems involved attempts to obtain closed-form solutions to serve as design aids. The methods of solution were generally within the mathematical framework of modal expansion and linear transformation techniques. Because these basic techniques are not readily amenable for handling the coupling terms, however, the effects of the vehicle inertia term were often ignored in the analysis.

When these effects are ignored, the boundary value problem is commonly called the moving force approximation. Some techniques neglect the inertia effects of the guideway. This assumption is frequently made in studies of the response of a vehicle traveling on a lightweight structure, such as a cable. The foregoing are extreme approximations in modeling the vehicle-guideway interaction problem.

Although modern computational techniques have eliminated the need for many of the limitations and simplifications previously imposed - especially in modeling the physical system - the work of many researchers seem to be traditional. The majority of studies are attempted either to extend the sophistication of the field equations or to include more complex forcing functions and boundary conditions. A moving force approximation is usually assumed, and a modal expansion technique is used as a solution method. Although modal analysis can be incorporated with iterative processes to accommodate the inertia effects of a vehicle, serious drawbacks in numerical calculations and limitations in practical applications exist. Detailed discussions of these points are available [1]. It has become increasingly doubtful that future developments based on the classical approach can be incorporated into engineering design and synthesis procedures, particularly as computational facilities become more readily available and more precise modeling is required for the simulation of a physical system.

#### GENERAL METHODOLOGY

Moving force approximation. There is sufficient justification for using the moving force approximation, provided its limitations are understood. The moving force approximation provides an adequate model for the moving mass problem if the order of magnitude of the transverse acceleration

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term is insignificant compared to the static inertia term of the traversing vehicle. Such cases arise when the vehicle is traveling at a low speed and the vehicle mass is a much smaller value than that of the guideway. The moving force approximation has been applied to design charts (e.g., Cooper loadings) and dynamic impact factor tables (as found in various bridge design codes) that have been developed to analyze the dynamic characteristics of highway and railway bridges.

A summary of early pre-computer work on the moving force approximation is available [2]. An excellent account of the evolution of the concept of dynamic impact factors has been published [3].

In the majority of early moving force studies, the guideway was modeled as a Bernoulli-Euler beam with simply-supported end conditions. Concentrated and uniformly distributed forces were used to model the vehicle loads.

Most recent developments are extensions of these analyses and simulate the dynamic heave response of new vehicle concepts for high-speed ground transportation and personal rapid transit systems. Vehicle suspension systems in particular are being considered to obtain more precise models. A typical model usually contains a set of sprung masses (passenger compartment), a set of unsprung masses (chassis), linear elastic springs, and linear viscous dampers. This discrete model is flexible and can represent a wide range of suspension designs -- wheels, magnetic suspensions, and air-cushioned suspensions [4-7]. Although the inclusion of the suspension system complicates the analysis, the basic formulations remain linear and uncoupled. Hence, modal analysis yields excellent results.

As indicated above, another area in which considerable attention has recently been focused is improvement of the mathematical descriptions for the forcing functions – effects of surface roughness and irregularities occurring in the guideway [8-10] – on the vehicle guideway system. Numerical results have also been obtained for vehicles traversing multispan, simply-supported, and continuously supported guideways [10-15].

Analyses that include more novel guideway models have also been considered. Guideways modeled by

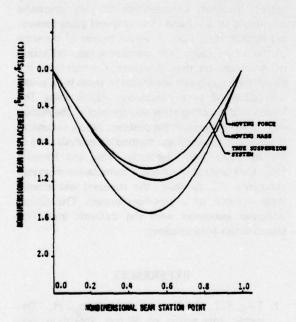
sophisticated beam theories or foundations without tensile resistance have also been studied [16, 17] but are usually complex and appear to have limited application.

A series of interesting problems recently considered [18-20] involves horizontally curved guideways with tandem vehicle loads. Dynamic amplifications of the critical moment and the rotation angle of the curved guideway can be as much as five times that of the corresponding static values. Further, above a critical traversing speed, multiple curved span responses can be several times higher than those occurring for single spans. Data were substantiated with scaled model tests. The dynamic effects for angular motion of the guideway are apparently considerably higher than those for heave motion; it would seem, therefore, that further studies in this area of angular motion for two-dimensional guideway structures are warranted.

Massless guideway approximation. The massless guideway approximation is the limiting case for a large vehicle mass/guideway mass ratio. Mathematically, such approximations do not lead to computational advantages when such techniques as modal expansion, finite differences, finite elements, and Fourier series expansions are used [11, 21-24], especially when high vehicle traversing speeds are considered. Thus, in those cases in which the moving force approximation is not valid, the massless structure approximation is a poor choice for a mathematical model.

A physical system that naturally fits the category of a massless guideway is a cable car traversing a taut cable. Although the formulation of the problem is simplified by eliminating the cable inertia effect, the resulting analysis can become more difficult if a modal expansion technique is attempted. This is so because the lack of bending rigidity in the cable results in discontinuities similar to those found in transverse wave propagation problems. Wave solutions for a mass traversing with constant velocity have been obtained [25, 26]. Kanning [27] recently studied the problem using both a polynomial expansion and an integral formulation previously introduced [1, 28]. Because the integral formulation employs an influence function that can incorporate the discontinuities in the deflection shape, it has distinct advantages in the computational process.

Moving mass approximation. With the moving mass approximation two distinct categories of mathematical models must be differentiated. One model (the classic moving mass problem) disregards the effects of the vehicle suspension system when the transverse inertia terms caused by the vehicle-guideway interaction are considered. The other model accounts for the effects of the vehicle suspension system in the derivation of the transverse inertia terms. The difference in the two models is demonstrated in the figure; the two problems are solved for a consistent set of vehicle and guideway parameters, and the guideway deflection is plotted as the traveling vehicle passes the three-quarter span point. For comparative purposes the moving force solution is also presented in the figure.



Transverse Displacement of a Simply
Supported Beam as the Traversing Vehicle
Passes the Three-Quarter Span Point.
Vehicle Speed = 90 m/s. Mass of
Vehicle/Mass of Guideway = 0.67

The trends shown in the figure are consistent for all cases [28, 29]. They become more pronounced when higher mass ratios and/or vehicle traversing speeds are considered. Note that the traditional design procedure, the moving force approximation, leads to the largest deformations — hence the largest stresses — in the guideway. When the true suspension

system is considered, the lightest guideway design is feasible. Note also that the moving force approximation yields an undesirable (and incorrect) condition: that the maximum deflection occurs at approximately mid-span.

These results were obtained using an algorithm developed by the authors [28, 29]. Other relatively recent efforts dealing with problems associated with the vehicle guideway problem are available [30-34].

#### SANDIA'S TROLLEY PROBLEM

An interesting physical problem, known as Sandia's trolley problem, has recently attracted much attention; it falls in the category of a moving mass problem. The Shock Simulation Department of Sandia Laboratories, Albuquerque, New Mexico, has utilized a cable trolley system to perform aerial experiments [35]. Trolleys carrying various payloads are launched from fixed positions at selected times and travel predetermined paths along a steel cable.

The steel cable, which has a diameter of 35 mm and a fracture strength of 750 kN, is stretched across a 1.5 km wide canyon. One end of the cable is anchored to a rock outcrop; the other end continues over a supporting sheave and down to a hoisting winch. The winch is used to control the tension in the cable and to position the cable to desired sag dimensions. For example, a tension of 490 kN yields a sag of 30 m and results in a cable transverse wave speed of 307 m/s.

The trolley-cable interaction problem is an interesting analytical study because, in contrast to the usual low, constant velocity assumption, the vehicle moves at a high velocity that varies as a function of time. Further, the sag is such that the static cable shape plays an important role in the dynamic response of the vehicle. In Sandia's initial studies [36, 37], the dynamics of a cable with an accelerating force were adopted to obtain an approximate solution. In the first study [36], the inertia of the moving mass was neglected, and the mass was modeled as a constant force. The second study [37] accounted for part of the inertial effects; the mass was modeled as a constant force plus a force proportional to the square of the vehicle velocity (an inertia term). The inertia was thus approximated as the centrifugal force due

to a mass traversing a constant curvature represented by the static cable shape. The moving mass considered in the study was small compared to the cable mass, so that this approximation gave reasonable results up to a fairly high velocity.

In a recent field test, a sudden and dramatic cable failure occurred as a trolley was accelerated through the transverse wave speed of a cable. A movie of the incident showed a sharp kink in the cable between the two supports of the trolley. Analysis of the system, accounting for the inertia of the moving mass [38], revealed that, when a mass is accelerated or decelerated through the transverse wave speed of an ideal string, two oppositely-traveling discontinuities are propagated in the string. These discontinuities are not predicted by the moving force analysis; thus, it is necessary to include all the kinematical terms representing the trolley-cable interactions.

The foregoing problem has also been considered by Ting and Kanning [39]. They used an integral formulation [27] that proved to be efficient and accurate.

#### OTHER MATHEMATICAL TECHNIQUES

The basic methods of analysis previously reviewed [1] were the modal analysis, finite difference, finite element, and series expansion methods. Two other mathematical techniques are worthy of comment: the modeling technique known as bond graphs [40] and use of the computational tools known as Lagrangian multipliers [41].

Bond graphs in essence represent a subtle alternative to the conventional technique of free body diagrams for developing the equations of motion of a system. Originally the technique found great favor among researchers in automatic controls because of its similarity to the conventional block diagram procedure. The method itself is related to a concept known as a mathematical tree [42, 43]. A variety of applications for bond graphs have been given [44]; papers on current applications to mechanical systems are available [45, 46].

The Lagrangian multiplier technique is, in a sense, another bond graph form [47]. The equations of motion for each component of the system are devel-

oped for each free body diagram; the interaction forces, or Lagrangian multipliers, are represented as external forces on the system. With the appropriate constraint equations a numerical procedure can be developed to determine the interactive forces at each point in time. An interesting feature is that the constraint equation can be written in terms of an error function that can be minimized numerically.

### RELATED DYNAMIC INTERACTION PROBLEMS

A class of fluid problems lends itself to the same mathematical framework as the vehicle-guideway system. Included are problems of pipe structures submerged in a parallel flow field and pipes conveying laminar fluid flow. A recent review of the state of the art by Chen [48] contains a large collection of references on these problems. Conceptually, the pipe-flow interactions are similar to those for a guideway subjected to a continuous vehicle mass. The kinematical coupling term also appears in the mathematical formulation of the problem. Modal expansion is again the predominant method of analysis used in the literature [49]. Recently, Ting and Kanning [50] have applied the integral formulation discussed previously [1] to study the transient and steadystate response of a pipe-flow system. The critical velocities associated with the dynamic instability phenomenon were obtained.

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# LITERATURE REVIEW survey and analysis of the Shock and Vibration literature

The monthly Literature Review, a subjective critique and summary of the literature, consists of two to four review articles each month, 3,000 to 4,000 words in length. The purpose of this section is to present a "digest" of literature over a period of three years. Planned by the Technical Editor, this section provides the DIGEST reader with up-to-date insights into current technology in more than 150 topic areas. Review articles include technical information from articles, reports, and unpublished proceedings. Each article also contains a minor tutorial of the technical area under discussion, a survey and evaluation of the new literature, and recommendations. Review articles are written by experts in the shock and vibration field

This issue of the DIGEST contains review articles on flow-induced vibration of nuclear reactor fuel; and a survey of structural optimization under dynamic constraints.

Dr. M.W. Wambsganss and Dr. T.M. Mulcahy of Argonne National Laboratory have concluded their two-part article on flow-induced vibration of nuclear reactor fuel. Part II covers design considerations.

Dr. M.A.V. Rangacharyulu of the Birla Institute of Technology & Science, Pilani, India, and Professor G.T.S. Done of The City University, London, have co-authored an article which reviews the literature since 1970 on structural optimization under dynamic constraints. Methods used with continuous and discrete modes are described for free vibration problems. Methods for forced vibration problems and nonconservative problems are also discussed.

## FLOW-INDUCED VIBRATION OF NUCLEAR REACTOR FUEL Part II: Design Considerations

M.W. Wambsganss and T.M. Mulcahy\*

Abstract - This two-part article focuses on the role of reactor fuel in flow-induced vibrations in nuclear reactors. Part I is on mathematical modeling of the fuel assemblies. Part II describes design considerations.

### DESIGN EVALUATION VIBRATION TESTING

It is generally necessary to resort to testing for final evaluation of each new component design from the standpoint of flow-induced vibration. Although reduced geometry scale models are often employed to investigate the potential for flow-induced vibration, fuel assemblies, because of their more manageable size and readily achievable flow-rate requirements, lend themselves to full-scale testing. Despite the fact that fuel assembly tests are full-scale, out-ofpile design evaluation tests, in general, must be considered as model tests, for, even in those cases in which the fuel assembly is prototypic, the environmental conditions are generally not simulated. Water, for example, is typically used to simulate sodium; air-water mixtures are used to simulate the two-phase flow condition associated with boiling; and air is often used to simulate CO2 or helium. In addition, the model tests are often performed at ambient temperatures and, of course, radiation and relative thermal expansion effects are not present. Consequently, test results must be extrapolated to reactor operating conditions, or, if possible, the tests must be shown to be conservative.

Design evaluation tests are generally carried out using prototypic fuel rods with simulated fuel pellets; depleted uranium and lead pellets have been used. Water is typically used as the test fluid in the evaluation of PWR (pressurized water reactor) and fast

(sodium-cooled) reactor fuel assemblies; air-water mixtures are often used to simulate the two-phase (steam-water) flow that occurs in BWRs (boiling water reactors) and reactors of the CANDU-BWR (Canadian deuterium uranium-boiling water reactor) type. Instrumentation includes accelerometers, strain gages, and velocity sensors for measurement of pin motion. Tests are carried out to evaluate specific designs; parameter studies are used to evaluate the effects of particular design features. Because of the complexities involved and the differences in fuel assembly designs, results from one test are usually not directly applicable in the design evaluation of another assembly. Nevertheless, results from different tests do provide insights and trends that are useful in test design and in the analysis and interpretation of results.

The design evaluation of fast reactor fuel assemblies has been reported [59, 64-66].\*\* Both grid spacers [59, 64, 65] and wire wrapped spacers [66] are included. Hess et al [65] have reported the results of endurance tests in sodium at temperatures to 650°C (1200°F). Kinsel [66] has reported on fullsized, 217-pin fuel assembly tests in water at temperatures of 38°C, 76°C, and 93°C (100°F, 169°F, and 200°F); 93°C (200°F) water closely simulates the viscosity of sodium at reactor operating temperatures. Kinsel found that pin vibration response is essentially unaffected by fluid temperature. Irradiation tests of wire-wrapped fuel bundles in EBR-II have shown that wear occurs between fuel pin and wire wrap; the wear has been correlated with fuel-pin-bundle porosity [67], which is computed as the difference between the inside dimension of the fuel duct and the theoretical dimension of the fuel pin bundle, divided by the number of rings of fuel pins making up the bundle; porosity is given in distance/ring. The greater the bundle porosity the greater the wear.

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<sup>\*\*</sup>For a complete list of References, see the November, 1979, issue of the Digest.

The proprietary nature of the light water reactors has limited the information available on designs and test results. As new fuel assemblies evolve, design evaluation testing is performed but usually only the fact that tests have been done is published in the open literature [68]. In an early study, Pavlica and Marshall [69] performed tests on a PWR 4 x 4 assembly of fuel rods with spacer grids of the spring type. They investigated the effect of the number of spacers and temperature (70°F and 150°F) on rod response; results showed that the temperature effect was not great. Carmignani et al [70] also performed tests on a 4 x 4 rod bundle of a BWR design. Six different assembly configurations were tested to evaluate the effect of spacer position, number, and design on rod response. Vibration amplitude decreased as the number of spacers increased. Results were compared with predictions using available empirical correlations [11, 62, 63]; for one test configuration reasonable agreement was achieved. Walton et al [38] have reported the results of in-core monitoring; fuel assembly lateral frequency decreased due to irradiation effects.

A large amount of work has been reported on the CANDU reactor fuel [33, 71-74]. The CANDU fuel assembly design is unique in the sense that the fuel rods are assembled in fuel bundles that are loaded end-to-end on a central support to form what is called a fuel string. Forrest and Hancox [71] investigated the effect of support structure motion as a source of excitation for the fuel string. Their test results indicated an apparent reduction in the effect of mechanical excitation as the flow was increased; at flow velocities above 13 m/s the measured motion was determined to be due to fluid excitation; the mechanical excitation effect was negligible. Card [72] studied the effect of upstream noise generators and determined that they have an important effect. Forrest and Monti [33] used steamwater flow introduced at the inlet to simulate twophase flow, which occurs at the outlet of the fuel string; rms-displacement increased with quality, peaking at 13%; reducing axial tension resulted in a considerable increase in lateral response.

At the 1973 Conference on Vibration Problems in Industry a group of papers [75-79] had to do with the design evaluation of the AGR (advanced gas reactor) fuel. The papers discuss the effect of roughness on flow-induced vibration response [75], the

effect of reactor noise as simulated by loudspeakers [76], vibrations during on-power loading [77], and full-scale testing [78, 79]. The gas coolant in the AGR is  $CO_2$ ; Whitton and Hammill [80] have discussed the differences in vibration response resulting from the use of  $CO_2$ , helium, and air as test fluids.

The measurements involved in design evaluation testing are often difficult and require state-of-the-art instrumentation, particularly small and relatively sensitive equipment; for in-reactor testing, survival at high temperatures and in a radiation environment are also required. Miniature accelerometers, strain gages, and variable reluctance transducers have been used; many of the references given above include discussions of instrumentation and measurement techniques; in some cases the descriptions are detailed. More exotic methods of detection involve the use of neutron flux measurements as an indicator of fuel rod motion [81, 82].

#### VIBRATION DAMAGE

A significant amount of work has been devoted to the mathematical modeling of parallel flow-induced vibrations, the measurement and characterization of the pressure field, the development of empirical prediction methods, and the performance of laboratory and in-reactor tests to measure fuel rod response in particular fuel assemblies. After the response has been characterized, the next very difficult step is to relate the vibration response to damage and to develop a set of acceptance criteria. Because of the small amplitudes of parallel flow-induced vibration, fatigue is generally not a failure mechanism of concern. Rather, fretting/wear is the failure mechanism of most importance [3, 4] because of inherent clearances between reactor fuel rods and support grids, or between fuel pin and wire wrap. Several papers [67, 76, 78, 83-85] refer to fatigue and wear assessments but, for the most part, do not contain details. An exception is Schmugar [84, 85] who discusses wear theory and models and describes a procedure for determining wear from fluid forces and rod response. Although the procedure was implemented and checked with test results, no details are given.

Fretting or wear failure due to parallel flow excitation has not occurred, to the authors' knowledge, except where defective parts allowed vibration above design levels [4]. Some cross flow is an integral part of fuel assembly heat-transfer design [70]. Only unforeseen components of cross flow have been responsible for fuel element failure by fretting. However, the occurrence of fretting is minimal, and in PWR practice the damaged fuel rods are often operated over their full reactivity lifetime [4].

Prediction of wear from basic pressure field and vibration response data is apparently in the developmental stage. The fuel rods employed in design evaluation tests are usually inspected to determine if a particular design produces abnormal amounts of wear; endurance testing is performed for critical conditions to determine wear rates [3, 70]. However, wear testing is still performed [70] in operating reactors to provide confidence in design. The best assessment of the reliability of a new fuel assembly design is perhaps the performance of a currently operating design.

### SUMMARY AND CONCLUDING REMARKS

Nuclear reactor fuel rods are subjected to excitation forces consisting of both fluid-borne pressure fluctuations and structurally transmitted motion imparted to the supports. The structurally-transmitted forces are associated with rotating machinery, such as pumps, and their transmission is highly dependent on the overall system design. The fluid-borne pressure fluctuations include both nearfield and farfield contributions. The farfield contributions are system dependent - they are functions of the pumps and piping arrangement, including valves, elbows, and headers and of the location of these components relative to the inlet to the fuel assemblies. The nearfield contribution is locally generated within the boundary layer and is modified by wake flows from such inherent disturbances as are provided by support grids, spacers, and wire wrap.

Mathematical modeling to predict response via the equations of motion is syymied because the forcing function, which consists of wall pressure fluctuations, must be characterized. Semi-empirical correlations for response are available; however, they are generally accurate only within an order-of-magnitude and

consequently are useful only in providing early design guidance. Therefore, designers have found it necessary to resort to full-scale testing for design verification. However, there is uncertainty even in full-scale testing because prototypic conditions of high temperature, radiation environments, and, perhaps most important, system features as they effect structuralborne vibration and farfield noise, are not easily achieved; it is necessary to extrapolate results to operating conditions. Nevertheless, design evaluation tests have proved beneficial in identifying potential problems and in contributing to design modifications and fixes. An area in which relatively little work has been reported is that of predicting fretting/wear based on knowledge of fluid pressures and rod response. Most wear data for new fuel assembly designs are obtained in full-scale flow tests and operating reactors.

In summary, awareness, on the part of the designer, of the potential for flow-induced vibration, coupled with the use of empirical correlations and tests, have resulted in fuel assembly designs that have proved to be reliable and free from flow-induced vibration damage; the authors know of no fuel rod failure caused by parallel flow-induced vibration. In this regard, it is interesting to note that a conclusion of an international working group on fast reactors was (at the time of the meeting) that "it appears that there are not serious vibrations problems existing in LMFBR fuel assemblies" [86]. However, as basic designs change (for example, spacer designs or flow paths) and as coolant flow velocities increase, it becomes necessary to reexamine the potential for flow-induced vibrations using the design tools and background experience available at the time.

There continues to be an active interest in fuel rod/assembly vibration; in particular an International Conference on Vibration in Nuclear Plants held at Keswick, England, in 1978. Unfortunately, the "Proceedings" were not available to the authors in time to include the papers in this review article. Two international conferences have been held this year that included papers on fuel vibration: 5th International Conference on Structural Mechanics in Reactor Technology in August in Berlin, and Symposium on Practical Experiences with Flow Induced Vibrations in September in Karlsruhe, Germany.

# A SURVEY OF STRUCTURAL OPTIMIZATION UNDER DYNAMIC CONSTRAINTS

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Abstract - This article reviews the literature since 1970 on structural optimization under dynamic constraints. Methods used with continuous and discrete models are described for free vibration problems. Methods for forced vibration problems and nonconservative problems are also discussed.

Methods of structural analysis have developed tremendously over the past two decades, due mainly to the advent of digital computers capable of speedily handling large arrays of numbers. As confidence has grown in the ability to predict the detailed performance of a structure, so has the desire to improve the design in a systematic way toward the optimum. The need to reduce structure weight without compromising structural integrity is all important in aerospace applications, and much of the motivation behind the development of structural optimization methods has been due to this factor. Furthermore, development has been assisted by making use of mathematical methods drawn from such fields as operations research and optimal control theory.

A well-posed problem of optimal structural design involves specifying:

- (i) the purpose of the structure
- (ii) the geometric design constraints
- (iii) the behavioral constraints
- (iv) the design objective, which acts as a basis for choice between acceptable alternative designs

When the problem is expressed mathematically, the constraints become simple bounds on variables in (ii) above, or on functions (iii); the design objective (iv) is expressed mathematically as an objective function to be minimized. Much of the earlier literature was concerned with problems having relatively simple behavioral constraints; e.g., minimum weight

design for various static loading conditions. However, papers dealing with the more complicated dynamic constraints have also been appearing in the literature in increasing numbers, and this survey is specifically concerned with this aspect.

Comprehensive reviews covering the whole field of structural optimization are available [1-6]. Reviews on the more specialized aspects, in which dynamic constraints are involved, have also been published [7-9].

The bibliography covered in this review extends mainly from 1970 onward; the greatest volume of work appeared in 1975 and 1976. References are classified according to problem free vibration, forced vibration, and nonconservative systems -- but a range of different methods of optimization applies to each problem. Before the particular problems are considered, the various methods available will be briefly surveyed.

### GENERAL METHODS OF STRUCTURAL OPTIMIZATION

The general methods fall into three broad categories:

- (a) optimality criterion methods
- (b) mathematical programming methods
- (c) optimal control methods

In (a) an optimality condition relating to the behavior of the structure is derived; the premise is that when the structure is sized to satisfy this condition, the objective function automatically attains an optimum value. The fully stressed or uniform strength design is an example of the early use of optimality criteria. The methods, which often yield computationally efficient solutions, have been

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extended to dynamic situations. There are some problem areas, however, such as those caused by multiple minima, multiple constraints, and active and passive grouping by members [4]. Methods using iterative schemes derived from the necessary conditions of optimality (Kuhn-Tucker conditions) are sometimes classed as optimality criterion methods even though they are purely numerical in nature.

The mathematical programming methods are applicable to a wide range of problems, of which structural optimization represents only one particular application. The general matrix methods of structural analysis form a mathematical basis on which numerical search procedures are used to progress to the optimum. The capability to deal with all types of objective and constraint functions makes these programming methods very versatile. Textbooks [10-12] provide lucid expositions of various algorithms used in programming techniques. Moe [13] presented a survey of mathematical programming methods with special emphasis on penalty function methods. A recent review [5] examined two important techniques (optimality criteria and programming methods) and related them via a Lagrangian function.

In methods based on the optimal control approach extensive use is made of calculus of variations, but the structure is represented by a continuous model, and the behavior is described by differential equations. The nondiscrete nature of the approach imposes limitations. An advantage is that various questions can be discussed using the continuous approach and optimal control theory: the existence and uniqueness of optimal solutions, the creation of an exact solution as a check for discrete methods, and the development and interpretation of optimality criteria.

Only very recently have optimal control techniques been applied to large framed structures having many members. The basic algorithm for optimization is based on the steepest descent optimal control techniques of Bryson and Ho [14]. A distinction is made between state and design variables associated with the problem, and the variables are related only through the equilibrium equations. The variables are treated independently in the optimization process. This distinction allows the designer to take advantage of efficient structural analysis methods and to eliminate explicit dependence on the state variables

through adjoint relationships. Haug and Arora [15] presented a survey of optimal design problems in the area of mechanical systems that can be addressed by this technique. The textbook by Bryson and Ho [14] is an excellent reference for optimal control techniques and the methods used in solving the resulting boundary value problems.

#### **SPECIFIC PROBLEMS**

The various problem areas and the methods used in structural optimization under dynamic conditions are described in this section.

#### Free Vibration Problems

Among the first problems of optimization under dynamic conditions were those involving the free vibrations of simple structural elements and framed structures; minimum weight designs having constraints on the natural frequencies and sectional areas are typically sought. Pierson [7] has given an account of work done during the 1960s; much of it was concerned with the minimization of weight for a specified fundamental frequency. The approach adopted generally depends on whether the system being investigated is continuous or discretely modeled.

Continuous models. A steepest descent method for solving continuous minimum weight problems with a specified fundamental frequency has been applied to a portal-frame design [16]. Weisshaar [17] made interesting observations on the optimum design of simple one-dimensional continuous systems with constraints on higher mode natural frequencies using variational methods. If the reference structure has periodic eigenfunctions, the optimum structure has periodic eigenfunctions. If this is the case and if the eigenvalues are integral multiples of each other, the optimum solutions for higher natural frequency constraints can be generated from the fundamental solution; the weight saving is not a function of which natural frequency is fixed.

Some authors have employed a piecewise uniform approximation to continuous problems [18-21]. Haug, Pan, and Streeter [18], using such an approximation coupled with a steepest descent method, studied frequency constrained minimum weight beams and plates. Cardou [19, 20] treated axial and

torsional vibration of beams, and Sippel and Warner [21] solved flexural vibration problems with frequency constraints using a Lagrangian multipliers approach.

Armand [22] presented an interesting application of a classical distributed parameter optimal control method to plates for fixed fundamental frequency. Minimum weight designs of stiffened cylindrical shells for maximum separation of the two lowest natural frequencies were presented using a sequential constrained minimization technique [23]. De Silva and Grant [24] tackled an interesting problem of maximizing a linear combination of natural frequencies of a turbine disc for a given weight. An optimal control approach was used; computation was via a penalty function approach coupled with a hill climbing technique.

Pappas [25] used a direct search procedure coupled with a gradient-based direction-finding algorithm to study the optimal frequency separation problem for cylindrical shells. Patnaik and Maiti [26] used programming techniques to study the problem of the interaction of different constraints, especially the static instability and natural frequencies of stiffened structures. Weisshaar [27] presented two approximate solutions to frequency-constrained problems for simple structural elements: a shooting technique used in optimal control theory and a perturbation technique. They are suitable for small-scale problems having few design variables.

Haug, Arora, and Matsui [28] used a steepest descent optimal control method to design a minimum weight continuous problem. The method, coupled with constraint error compensation, converges quite rapidly. Pierson [29] used a similar approach of state space formulation and a gradient projection algorithm to design minimum weight beams for fixed natural frequencies. More than one frequency can be constrained.

Elwany and Barr [30] studied some optimization problems in torsional vibration using a variational method with a view to maximize a given natural frequency for a fixed weight, or equivalently to minimize weight for a fixed frequency. Constraints are implemented through Lagrangian multipliers; the resulting nonlinear equations are solved numerically. Cardou and Warner [31] applied an optimality

criterion to simple axially vibrating bars and portal frames under frequency and section constraints (the use of the term sandwich structures in the title of this reference is misleading).

Discrete models. Mathematical programming methods and optimality criterion methods are extensively used for the structures represented by discrete models. Attempts have been made to extend optimal control methods to cover these problems. Rubin [32] developed a procedure in which the fundamental frequencies can be subjected to an inequality constraint. The process follows two alternating cycles; initially a steepest descent gradient iteration is used to change frequency until it lies within a prescribed margin. Then the weight is minimized using a steepest descent algorithm. Occasional correction steps using frequency modification cycles are needed to maintain the desired frequency change.

Fox and Kapoor [33] used Zoutendijk's method of feasible directions to solve frequency constrained problems. Setlur and Kapoor [34] presented a parametric differentiation method in conjunction with the penalty function approach. The design is treated as a function of the penalty parameter to determine the appropriate parameter. A sequential method is used that requires both first and second derivatives of the objective function.

Pappas and Amba Rao [25] also proposed a penalty function approach to treat both static and dynamic optimization problems with inequality constraints. The objective function is formulated with an appropriate penalty function; the function is appended so that a reasonably symmetric ridge is created at the acceptable/unacceptable region. A direct search method coupled with a local search technique is used to move along the ridge to the optimum. The method performed very well, but large-scale problems were not tested.

A sequential unconstrained minimization technique involving a variable metric algorithm was used to design large framed structures for a fixed fundamental frequency [35]. The concept of design variable linking was used to reduce the number of variables, thus increasing the efficiency of the optimization process. An extended interior penalty function method was implemented for determining the transition between the interior and extended por-

tions; this method was a powerful algorithm for general inequality constrained problems [36] and can easily be applied to implement frequency constraints. Minimization can be carried out in both feasible and infeasible regions.

Reddy and Rao [37] studied some optimization problems related to machine tool structures represented by finite elements. Minimum weight designs with constraints on natural frequencies and chatter stability were obtained through a penalty function method, thus increasing the scope of application of programming techniques. Schmit and Miura [38] incorporated an efficient combination of finite element techniques and mathematical programming techniques. Several approximation concepts — design variable linking, constraint approximations, and constraint deletion — were used.

An energy density criterion has been derived; a recursive relation for the design variables was derived so that the design can be continuously improved [39]. Taig and Kerr [40] also derived an optimality criterion and a related recursive relation. They considered constraints on dynamic stiffness, strength, and sectional areas of members. These methods were very efficient for large structures.

Recently an efficient algorithm [41] has been proposed that is similar to one for mechanical design problems with natural frequency constraints [37]. A similar technique has been used to study the effect of shear formation and rotary inertia on optimum beam designs with frequency constraints [42]. Yoshimura [43] used an energy density optimality criterion to study the design of machine tool structures for minimum chatter conditions and frequency constraints.

An optimal control method using a steepest descent algorithm has been applied to the design of plane frames with constraints on deflection, strength, and natural frequencies [44, 45]. A similar algorithm was used to design mechanical systems [28]. These applications of optimal control techniques to large-scale problems are noteworthy.

Rizzi [46] presented a general procedure for structural optimization with several constraints, including frequency constraints. He used a recursion relation derived from the necessary conditions of Kuhn-

Tucker and a procedure to delete the inactive constraints. The method has excellent covergence properties. Flewry and Geradin [47] showed how the optimality criterion method can be interpreted from a mathematical programming point of view and have proposed a generalized form of optimality criterion based on the Kuhn-Tucker conditions of the exact problem. The solution obtained is thus identical to that obtained by mathematical programming for a problem using inverse design variables and linearized constraints.

Arora and Haug [48] developed a hybrid method that combines the best features of both optimality criterion methods and state space gradient projection methods used in optimal control theory. The potential of the method is demonstrated; such hybrid methods may lead to more efficient design procedures.

Recent contributions have appeared in a special journal issue on structural optimization [49-51]. Two general purpose optimization algorithms were applied to a beam axial vibration problem [49]. The Kuhn-Tucker optimality criteria were used in conjunction with the finite element method, with the usual constraints on natural frequencies and design variables [50]. The application is to a thinwalled shaft and a turbine shaft. The use of second order frequency sensitivities in conjunction with SUMT was described [51].

#### Forced Vibration Problems

The optimum design of shock and vibration isolators is an early example of structural optimization under forced vibration conditions; methods of mathematical programming have been applied [52]. In general, the total structural weight must be minimized subject to constraints on the displacements and stresses, when both are functions of time and the design variables. The displacements satisfy the usual equations of motion that now include forcing terms. The problem is simplified if sinusoidal excitation is considered. Frequency constraints can be included in the formulation.

Mróz [53] and Plaut [54] employed energy methods connected with Rayleigh's inequality to design minimum weight structures under simple harmonic excitations for a specified deflection. A common feature of their approaches is that the forcing fre-

quency is limited from above by the fundamental frequency of the optimal configuration. Similar problems have been examined using optimal control techniques with the frequency restriction removed [55, 56]. Maximum allowable stress amplitude and minimum cross-sectional area constraints were imposed. The analyses revealed that the design space in the absence of damping can contain many disjoint feasible regions and that multiple optima exist. Seireg and Hamad [57] noticed similar features; they used a combination of gradient based search and a univariate search to arrive at the optimum design. State space gradient projection methods [28, 29] do not seem to have been applied to this class of problem, but they can easily be extended.

Some steps have recently been taken to design structures under stochastic loading [58-61]. Rao [58] used standard mathematical programming techniques to design beam and platelike structures under blast and acoustic loading with constraints on the probability of failure. Narayanan and Nigam [59] applied a SUMT method using the gradient method of Fletcher and Powell to design sheet stringer panels subjected to jet noise excitation. They considered constraints on stresses, fatigue life, and natural frequencies. Design in a seismic environment has also been studied [60, 61].

Fox and Kapoor [33] examined some discrete problems described earlier and obtained numerical results for several truss problems. A single sine wave-forcing function was assumed. The objective was to obtain partial derivative information so that efficient minimization techniques could be used. A shock spectral method was used to remove time dependency in the dynamic response constraints. The actual displacements and stresses were replaced by conservative upper bounds.

Cheng and Botkin [62] used a similar approach to design minimum weight damped frames subjected to general dynamic loads. The method of analysis is based on modal superposition; the dynamic amplification factors were obtained from the shock spectrum. The peak dynamic response was constrained. Cassis and Schmit Jr. [63] also studied frame problems; they included the dynamic response quantities treated parametrically in time in the formulation of optimization design problem.

Approximation concepts applied elsewhere [36, 38] have been extended to the dynamic response regime. The realization of the disjoint nature of the design space leads to the choice of an exterior penalty function method incorporating the Davidon, Fletcher, and Powell minimization algorithm. Successful implementation is facilitated by using dummy constraint boundaries and a new approach to the move limit problem. The need for move limitation arises from the use of approximate analysis techniques based on Taylor's series expansions for dynamic response quantities. It has been shown how an interior penalty function can be applied to problems of optimum design for dynamic loads [36].

An algorithm has been presented for studying piecewise uniform structures [64]. Constraints were imposed on displacements, stresses, frequency, and design parameters. The time-dependent constraints were transformed to equivalent functional constraints; a state space steepest descent algorithm (optimal control theory) was used. The same authors [65] have also developed the state space approach to sensitivity analysis and optimization of structures under transient dynamic excitations. The gradient projection algorithm used by Pierson [29] can also be employed on these problems.

An energy density based optimality criterion was used to devise a recursive relation to design large structures subjected to dynamic loading with constraints on displacements and stresses [66, 67]. The aperiodic forcing function was represented by a Fourier integral in determining the dynamic response. The optimality criterion derived for normal modes was used as an approximation to design in the dynamic mode, which is replaced by a combination of normal modes. Sciarra [68] used a recursive relation based on the strain energy distribution to reduce vibratory response for harmonically excited structures with minimum weight penalty.

#### Nonconservative Problems

A class of problems closely related to problems with natural frequency constraints is that of optimal design with such specific aeroelastic eigenvalues as divergence speed or flutter speed. In general, the earlier attempts to design minimum weight structures for flutter constraints adopted a mathematical programming point of view or applied a Lagrangian multiplier approach.

Several interesting one-dimensional panel and axisymmetric circular cylindrical shell optimization problems, for which the flutter speed is held constant, have been formulated and solved. The design of cantilever columns under follower forces [69-72] falls into the same category. In some early papers various one-dimensional problems were treated using optimal control techniques. The resulting two-point boundary value problem was solved with shooting techniques. Armand and Vitte [73] and Weisshaar [74] used a similar approach to treat minimum weight panel design problems with flutter constraints.

Plaut [75] applied a two-term Ritz procedure to the related problem of maximizing the critical flutter parameter for a given mass of piecewise uniform thick panels. Pierson [76] and Pierson and Russell [77] proposed a discrete approximation to continuous panel problems; finite difference equations and a gradient projection algorithm were used in conjunction with a penalty function technique.

Pierson [78, 79] also used a gradient projection optimal control algorithm incorporating conjugate gradient directions of search to treat the same kind of problem, and Pierson and Genalo [80] extended the method to treat two-dimensional panel problems that fall into the category of distributed parameter optimal control problems. Inplane loads and minimum section constraints were allowed. The algorithm differs from the usual projection operator in optimal control theory in three ways: the requirement for terminal state constraint satisfaction at each iteration, the method of step size selection along projected directions of search, and the treatment of control parameters. It is more efficient than earlier approaches, in which two-point boundary problems that arise from necessary conditions of optimality must be solved; the terminal state values are sensitive to initial guesses of thickness distribution and control parameters.

Several types of mathematical programming methods have been successfully applied to flutter optimization in conjunction with finite element formulation. Craig [81] used a gradient projection algorithm to design a supersonic panel with a flutter constraint. Rudisill and Bhatia [82, 83] used a gradient search technique incorporating an approximate sequence of gradient searches that increase flutter velocity and a gradient mass search that

reduces flutter velocity; when the desired velocity is reached, a gradient projection algorithm maximizes the flutter speed at constant mass. This is similar to the process of Rubin [32] for frequency constraints. Simodynes [84] used a similar approach. In these procedures the step size in the search is arbitrary. Rao [85] has an interior penalty function method to design large structures to a flutter constraint.

Haftka [86, 87] used the same method in the context of continuous flutter constraints, which are treated as parametric constraints. The idea of an equivalent minimum constraint was used to simplify the problem. Gwin and Taylor [88] used a feasible direction method, and Craig and Erbug [89] proposed a gradient projection algorithm to study minimum weight flutter constrained problems. Special features were the use of analytical expressions for gradients (calculated only for active constraints), constraint tolerances, and a return vector for whenever constraints are violated. These speed up convergence. Weisshaar [90] also used a gradient projection method based on a Fletcher-Reeves conjugate direction search with a refined finite element formulation. Phea and Chi [91] employed approximations in the general nonlinear programming problem and then applied linear programming techniques.

A search technique with a defined step size has been presented for the minimization of mass for fixed flutter speed [92]. The flutter speed was exactly satisfied at each resizing step; step size was determined by a direct minimization of mass for each set of flutter derivatives calculated. Niblett [93] investigated three different mathematical programming approaches based on gradient projection; he applied the most economical to a swept wing example. A number of philosophical questions relating to flutter optimization were also addressed.

Several researchers have employed optimality criterion techniques to solve flutter optimization problems. The important steps are the derivation of necessary conditions to be satisfied by a locally optimum design and a recursive procedure to realize these conditions. Pines and Newman [94] derived a rigorous optimality condition for flutter-constrained minimum-weight design problems. The energy density criterion thus derived can be viewed as the nonconservative equivalent of the Lagrange energy density optimality criterion [39]. An iterative

scheme was used to arrive at the optimum design. Newman's work is significant in that he used an integral formulation; the iterative procedure for satisfying the optimality criterion is integrated with the flutter solution, thereby improving the efficiency. Taig and Ker [40] developed a resizing algorithm based on a general optimality theorem to design flutter constrained structures.

Wilkinson et al [95] also used an optimality criterion method. They examined several ad hoc optimality criteria. They obtained a uniform flutter velocity derivative criterion for flutter critical elements and a fully stressed design criterion for strength critical elements. Their approach provides a design for both flutter and strength constraints.

Segenerich and McIntosh [96] used a hybrid method that is essentially a direct numerical search technique having the direction of move related to the optimality criterion. Haftka et al [97] presented a comparative study of optimality criterion-based methods and programming methods for flutter optimization; the former methods were rated better. McIntosh and Ashley [98] developed an heuristic design algorithm based on an optimality criterion and compared the results to those obtained by a search scheme based on the method of feasible directions. They too considered that the former technique was a better candidate for large structures with multiple constraints. They also showed how the optimality criterion might be constructed when the aeroelastic constraint is written in the time domain. Their work suggests that complete mathematical rigor is not always necessary in a procedure for design optimization.

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## ANNUAL ARTICLE INDEX

#### **FEATURE ARTICLES**

	ISSUE	PAGES
Lund, J.W.	1	5-10
Evaluation of Stiffness and Damping Coefficients for Fluid-Film Bearings		
Rao, S.S.	2	3-12
Structural Optimization Under Shock and Vibration Environment		
Holzer, S.M.	3	3-6
Dynamic Snap-Through of Shallow Arches and Spherical Caps		
Rieger, N.F.	4	3-5
Damping Properties of Turbine Blades		
Murthy, P.N.	5	7-11
Some Recent Trends in Aircraft Flutter Research		
Migliore, H.J. and Webster, R.L.	6	3-16
Current Methods for Analyzing Dynamic Cable Response		
Ginsberg, J.H.	7	3-8
Recent Developments for the Nonlinear Distortion of Non-Dispersive		
Acoustic Waves. Part I: Planar Waves and the Basic Method		
Ginsberg, J.H.	8	3-12
Recent Developments for the Nonlinear Distortion of Non-Dispersive		
Acoustic Waves. Part II: Multidimensional Systems		
Bort, R.L.	9	9-15
A History of Shock Testing of Ships with Underwater Explosions		
Gibson, R.F. and Wilson, D.G.	10	3-11
Dynamic Mechanical Properties of Fiber-Reinforced Composite Materials		
Nelson, F.C.	11	3-9
A Review of Substructure Analysis of Vibrating Systems		
Genin, J. and Ting, E.C.	12	3-9
Vehicle-Guideway Interaction Problems		

#### LITERATURE REVIEWS

	ISSUE	PAGES
Berman, A.	1	13-16
Parameter Identification Techniques for Vibrating Structures		
Mugridge, B.D.  Noise Characteristics of Axial and Centrifugal Fans as Used in Industry - A Review	1	17-24
Reddy, J.N. Finite Element Modeling of Structural Vibration: A Review of Recent Advances	1	25-39
Radeş, M.  Analysis Techniques of Experimental Frequency Response Data	2	15-24
Mazumdar, J.  A Review of Approximate Methods for Determining the Vibrational Modes of Membranes	2	25-29
Kalinowski, A.J.  A Survey of Finite Element-Related Techniques as Applied to Acoustic  Propagation in the Ocean. Part I: Finite Element Method and Related Techniques	3	9-16
Iwatsubo, T. Stability Problems on Rotor Systems	3	17-26
Kalinowski, A.J.  A Survey of Finite Element-Related Techniques as Applied to Acoustic Propagation in the Ocean. Part II: Transparent Boundary Simulation Techniques	4	7-16
Johns, D.J. Wind-Excited Behavior of Structures. II	4	17-29
Jones, D.I.G.  High Temperature Damping of Dynamic Systems	5	13-18
Sakata, T.  Reduction Methods for Problems of Vibration of Orthotropic Plates. Part I:  Exact Methods	5	19-26
Sakata, T.  Reduction Methods for Problems of Vibration of Orthotropic Plates. Part II:  Generalized Reduction Method for Generally Orthotropic Plates with Arbitrary  Shape	6	19-22
Plunkett, R. Shock and Vibration Instrumentation	6	23-24
Hobaica, E.C.  Behavior of Elastomeric Materials Under Dynamic Loads - II	7	11-18

#### LITERATURE REVIEWS (CONTINUED)

	ISSUE	PAGES
Baker, W.E.	7	19-24
Approximate Techniques for Plastic Deformation of Structures Under Impulsive Loading. II	al of property	15-24
Pope, L.D.	8	15-18
Update on the Low Wavenumber Content of TBL Pressure Fields		10-10
Agrawal, B.N. and Evan-Iwanowski, R.M.	8	19-22
Nonstationary and Nonlinear Vibration Analysis		19-22
Volin, R.H.	9	17-33
Techniques and Applications of Mechanical Signature Analysis		55
Beards, C.F.	9	35-41
Damping in Structural Joints		and the fi
Bert, C.W.	10	13-23
Recent Research in Composite and Sandwich Plate Dynamics		
Mayne, R.W.	10	25-33
Optimization Techniques for Shock and Vibration Isolator Development		20 00
Wambsganss, M.W. and Mulcahy, T.M.	11	11-22
Flow-Induced Vibration of Nuclear Reactor Fuel. Part I: Modeling		
Derby, T.F.	- 11	23-28
Computer Programs: Shock and Vibration Isolation		20 20
Nambsganss, M.W. and Mulcahy, T.M.	12	11-13
Flow-Induced Vibration of Nuclear Reactor Fuel. Part II: Design Considerations		
Rangacharyulu, M.A.V. and Done, G.T.S.	12	15-25
A Survey of Structural Optimization Under Dynamic Constraints		

# **BOOK REVIEWS**

#### STABILITY THEORY AND ITS APPLICATIONS TO STRUCTURAL MECHANICS

C.L. Dym Noordhoff, 1974

This short, interesting text is a good introduction to some of the modern stability methods for continuous structures. Applications are sprinkled throughout. The material is suitable for self study or for a graduate engineering course.

In the author's words, "...the book has three principle parts: 1) The development of the Lyapunov direct method and of the minimum energy principle for discrete systems; 2) Analogous development of the Lyapunov functional method and of the minimum energy approach for continuous systems; 3) Applications." In particular, the analysis of imperfection sensitivity as pioneered by Koiter and elaborated by Budiansky and Hutchinson is carried out for a number of simple examples including columns, arches, and circular and rectangular plates.

Again, in the author's words, "...we intend to be informal rather than rigorous in our presentation." This is an attractive feature of the book but has, perhaps, led to sloppiness in some of the mathematics. For example, in the analyses of three different problems on pages 37, 38, and 41, the author states that the time derivatives of certain Lyapunov functions are negative definite whereas, in fact, they are only negative semi-definite as functions of <u>all</u> the state variables. To include asymptotic stability in this case one must invoke the notion of invariant sets.

In summary, Professor Dym has given us a concise, up-to-date introduction to some of the newer practical methods for the stability analysis of structures.

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# AN INTRODUCTION TO OPTIMAL ESTIMATION OF DYNAMICAL SYSTEMS

J.L. Junkins Sijthoff & Noordhoff International Publishers B.V. Alphen an den Rijn, The Netherlands, 1978

The text presents a carefully developed theory and numerous applications of estimation of dynamic systems. Examples are used throughout to describe the class of problems being discussed and to illustrate use of the computational algorithms that are developed. The examples range from simple, but applicable, idealizations to realistic problems. Statistics of measurement error are accounted for in each class of problems treated.

An introductory chapter on least square approximation develops the least squares method for both batch and sequential data. Linear systems are introduced with examples; necessary and sufficient conditions for optimal estimation are derived. Batch problems are treated, including constraints that zero error shall occur in selected observations. Sequential data are then treated and several forms of state update equations derived. Finally, nonlinear estimation is introduced and least square differential correction algorithms are derived.

The second chapter is devoted to a brief and somewhat more rigorous treatment of minimum variance estimation. Optimum state estimation matrices are derived, both with and without a priori estimates of the state and its co-variance matrix. Selection of the weighting matrix in the least square method to provide minimum variance estimation is discussed.

Applications of parameter estimation methods are presented in the third chapter. Planar triangulation and spacecraft trajectory and orientation determination are treated as elementary to moderately complex examples. Modeling the earth's topography and modeling gravitational potentials are presented as more challenging examples.

An introduction to the theory of ordinary differential equations is provided in Chapter 4 in preparation for dynamic systems. Reduction of arbitrary ordinary differential equations to first-order form is discussed. Differentiability of the solution with respect to initial state and model parameters is derived for both linear and nonlinear systems. A brief introduction to numerical integration theory is presented.

This theory is then combined in Chapter 5 with ideas developed in Chapters 1 and 2 to develop a theory of estimation of dynamic systems. Methods and algorithms are developed for estimation of initial state, model parameters, and the state of a dynamic system at a discrete sequence of points in time. The latter result is extended by taking the limit, as the time grid goes to zero, to obtain conditions and algorithms for continuous state estimation. Finally, sequential estimation of nonlinear dynamic systems is briefly treated.

In the final chapter, methods of Chapter 5 are used to solve optimal estimation problems involving projectile trajectories and satellite photogrammetry.

The text is clearly written at a technical level and should be accessible to advanced senior undergraduate students, first-year graduate students, and practicing engineers and scientists. The author's insights and care in formulating and solving illustrative examples will greatly aid the applications-oriented reader. Presentations of none but essential mathematical concepts and the basic theory of minimization, probability, and linear algebra make the text essentially self-contained. The text is recommended to anyone with a moderate mathematical background who wants to gain access to the methods and more advanced literature on optimal estimation of dynamical systems:

E.J. Haug University of Iowa Iowa City, Iowa 52242

### THE DYNAMICAL BEHAVIOR OF STRUCTURES - 2ND EDITION

G.B. Warburton Pergamon Press, Maxwell House, Elmsford, NY, 1976

This delightful little book, written by a master structural dynamicist, is a complete revision, up-dated to provide information on current thinking. The book contains six major chapters plus five appendixes.

Chapter I discusses the single-degree-of-freedom system and responses due to harmonic motion, hysteretic damping, shock response, and transient response including Duhamel's integral. The shock response section is too short for such an important topic. The chapter concludes with an introduction to random processes and random vibration.

Chapter II introduces the reader to dynamics of frames (harmonic and transient analysis). The use of matrix methods in multi-degree-of-freedom systems is described, as are the normal mode method of solution and complex eigenvalue procedures. The chapter concludes with random vibration, too short a discussion, but the reviewer considers this an excellent chapter.

Beam vibration plays an important role in structural dynamics. The author leads us from simple beam theory to the more complex, with general end conditions in Chapter III. Harmonic, simple, and transient responses are described. The author packs a tremendous amount of information into a small section, including the Rayleigh—Ritz for uniform and non-uniform beams and an introduction to finite elements.

Chapter IV delves further into beam theory: the response to time-dependent boundary conditions, beam column vibration, beams in elastic foundations, shear deformation, and torsion. The chapter concludes with a discussion of the dynamic response of rigid-plastic beams.

Chapter V focuses upon vibrations of plates and shells. Most vibration texts omit these important topics. Transverse vibration of rectangular plates with simple end conditions are discussed, as are the use of Rayleigh-Ritz method and the finite element approach to in-plane vibration of plates. The author briefly discusses four- and eight-node isoparametric elements applied to plate design and then shows how they can be applied to transient response of plates. The dynamics of shells are considered, as is its matrix application.

In Chapter VI the author briefly considers fluid-structure dynamic interaction, which is emerging as an important phase of dynamics. Ground-structure dynamic interaction (important in earthquake applications) is briefly considered. Wind-induced vibration of structures is lightly touched upon. The reviewer would have liked more discussion of applica-

tions dealing with fluid structures utilizing random processes.

The appendixes include Fourier transforms, matrix properties, Lagrangian equations, and orthogonality conditions for beams. A short section on eigenvalue economizers has direct application to finite elements.

In summary, this is an excellent book considering the large number of topics that are discussed. The reviewer believes that the book could be enhanced by extending the sections on random vibrations and fluid-structure dynamic interaction and finite elements.

> H. Saunders General Electric Company Building 41, Room 319 Schenectady, New York 12345

### **BOOK REVIEWS: 1979**

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# **SHORT COURSES**

# **DECEMBER**

# SURFACE BLASTING

Dates: December 5-7, 1979
Place: Washington, D.C.

Objective: This is a field-oriented course on commercial surface blasting (quarries, open pits and construction). The course uses a variety of presentation techniques, including movies, problem solving, question and answer sessions and special "hands-on" exercises. Topics to be covered are: commercial explosives in use today; detonation methods; rock breakage; blast design; blasting economics; and blasting and the neighbors.

Contact: E.I. du Pont de Nemours & Co. (Inc.), Applied Technology Division, Room 35901, Wilmington, DE 19898 - (302) 774-6406.

# VIBRATION AND SHOCK SURVIVABILITY, TESTING, MEASUREMENT, ANALYSIS, AND CALIBRATION

Dates: December 10-14, 1979

Place: Ling Electronics, Anaheim, California

Dates: February 4-8, 1980
Place: Santa Barbara, California

Dates: April 7-11, 1980 Place: Dayton, Ohio

Objective: Topics to be covered are resonance and fragility phenomena, and environmental vibration and shock measurement and analysis, also vibration and shock environmental testing to prove survivability. This course will concentrate upon equipments and techniques, rather than upon mathematics and theory.

Contact: Wayne Tustin, 22 East Los Olivos St., Santa Barbara, CA 93105 - (815) 682-7171.

# MACHINERY VIBRATION ANALYSIS

Dates: December 11-13, 1979

Place: New Orleans, Louisiana

Objective: The topics to be covered during this course are: fundamentals of vibration; transducer concepts; machine protection systems; analyzing vibration to predict failures; balancing; alignment; case histories; improving your analysis capability; managing vibration data by computer; and dynamic analysis.

Contact: Bob Kiefer, Spectral Dynamics, P.O. Box 671, San Diego, CA 92112 - (714) 268-7100.

# **JANUARY**

# PROBABILISTIC AND STATISTICAL METHODS IN MECHANICAL AND STRUCTURAL DESIGN

Dates: January 7-11, 1980
Place: Tucson, Arizona

Objective: To provide practical information on engineering applications of probabilistic and statistical methods, and design under random vibration environments. Modern methods of structural and mechanical reliability analysis will be presented. Special emphasis will be given to fatigue and fracture reliability.

Contact: Dr. Paul H. Wirsching, College of Engineering, The University of Arizona, Tucson, AZ 85721 - (602) 626-3159/626-3054.

# FINITE ELEMENT ANALYSIS

Dates: January 7-11, 1980 Place: Tucson, Arizona

Objective: The purpose of this course is to provide structural engineering practitioners with an understanding of the fundamental principles of finite element analysis, to describe applications of the method, and to present guidelines for the proper use of the method and interpretation of the results obtained through it. Emphasis will be placed upon the

linear analysis of frameworks, plates, shells and solids; and dynamic analysis will also be treated.

Contact: Dr. Hussein Kamel, College of Engineering, The University of Arizona, Tucson, AZ 85721 - (602) 626-1650/626-3054.

# DYNAMIC ANALYSIS IN TURBOMACHINERY DESIGN

Dates: January 14-18, 1980 Place: Madison, Wisconsin

Objective: This course will be devoted to the understanding of mechanical phenomena involved in turbo-machinery design, including torsional and lateral shaft vibrations and vibrations of components such as rotating fan and turbine blades and non-rotating vanes. Topics to be covered include lumped parameter analysis of rotors in rigid and flexible bearings, internal and external damping, effects of coupled transverse and angular motion; lumped parameter and normal mode analysis of blade response allowing for effects of damping, hysteresis loop characteristics, slip at dovetails and at platforms; and vibrations of stationary vanes. Some state of the art experimental techniques will be discussed.

Contact: Dr. Donald E. Baxa, Dept. of Engineering, University of Wisconsin - Extension, 432 N. Lake St., Madison, WI 53706 - (608) 262-2061.

# **FEBRUARY**

# FIXTURE DESIGN FOR VIBRATION AND SHOCK TESTING

Dates: February 11-15, 1980
Place: Santa Barbara, California
Dates: March 10-14, 1980
Place: St. Petersburg, Florida

Objective: The relative mertis of various types of shakers and shock test machines are briefly considered, with most emphasis on electromagnetic shakers. The seminar will be devoted to practical and proven simplified design and fabrication techniques. An important area to be covered is that of evaluating a fixture once it is built.

Contact: Wayne Tustin, Tustin Institute of Technology, 22 East Los Olivos St., Santa Barbara, CA 93105 - (815) 682-7171.

## FINITE ELEMENTS IN BIOMECHANICS

Dates: February 18-21, 1980 Place: Tucson, Arizona

Objective: As a forum for the exchange of ideas, for the definition of the state-of-the-art, and for the presentation of new research results in biomechanics.

Contact: Professor Bruce R. Simon, Dept. of Aerospace and Mechanical Engineering, College of Engineering, The University of Arizona, Tucson, AZ 85721 - (602) 626-3752/626-3054.

# BALANCING OF ROTATING MACHINERY

Dates: February 26-28, 1980

Place: Shamrock Hilton, Houston, Texas

Objective: The seminar will emphasize the practical aspects of balancing in the shop and in the field. The instrumentation, techniques, and equipment pertinent to balancing will be elaborated with case histories. Demonstrations of techniques with appropriate instrumentation and equipment are scheduled. Specific topics include: basic balancing techniques (one- and two-plane), field balancing, balancing without phase measurement, balancing machines, use of programmable calculators, balancing sensitivity, flexible rotor balancing, and effect of residual shaft bow on unbalance.

Contact: Dr. Ronald L. Eshleman, Vibration Institute, 101 W. 55th St., Suite 206, Clarendon Hills, IL 60514 - (312) 654-2254/654-2053.

# MARCH

# MEASUREMENT SYSTEMS ENGINEERING

Dates: March 10-14, 1980 Place: Phoenix, Arizona

# MEASUREMENT SYSTEMS DYNAMICS

Dates: March 17-21, 1980 Place: Phoenix, Arizona

Objective: Program emphasis is on how to increase

productivity, cost-effectiveness and data-validity of data acquisition groups in the field and in the laboratory. Emphasis is also on electrical measurements of mechanical and thermal quantities.

Contact: Peter K. Stein, 5602 East Monte Rosa, Phoenix, AZ 85018 - (602) 945-4603/946-7333.

### **MACHINERY VIBRATIONS COURSE**

Dates: March 17-20, 1980

Place: Oakbrook Hyatt House, Oakbrook, IL Objective: This course on machinery vibrations will cover physical/mathematical descriptions, calculations, modeling, measuring, and analysis. Machinery vibrations control techniques, balancing, isolation, and damping, will be discussed. Techniques for machine fault diagnosis and correction will be reviewed along with examples and case histories. Torsional vibration measurement and calculation will be covered.

Contact: Dr. Ronald L. Eshleman, Vibration Institute, 101 W. 55th St., Suite 206, Clarendon Hills, IL 60514 - (312) 654-2254/654-2053.

# **BOUNDARY INTEGRAL EQUATION METHODS**

Dates: March 17-22, 1980

Place: University of Arizona, Computer Center Objective: The objective of this short course is to introduce the Boundary Integral Equation Method (BIEM) as an efficient numerical tool for the solution of various types of ground-water problems. The course is designed to provide a working knowledge of the BIEM so that the participants will be able to use and modify the existing computer programs and to develop their own programs for their specific problems.

Contact: Professor James A. Liggett or Professor Phillip L.-F. Liu, School of Civil and Environmental Engrg., Cornell University, Hollister Hall, Ithica, NY 14853 - (607) 256-3556/256-5090 respectively.

# **EXPLOSION HAZARDS EVALUATION**

Dates: March 31-April 4, 1980
Place: Southwest Research Institute

Objective: This course covers the full spectrum of problems encountered in assessing the hazards of accidental explosions, in designing the proper con-

tainment as necessary, as well as developing techniques to reduce incidence of accidents during normal plant and transport operations. Specific topics to be covered are: fundamentals of combustion and transition to explosion; free-field explosions and their characteristics; loading from blast waves; structural response to blast and non-penetrating impact; fragmentation and missile effects; thermal effects; damage criteria; and design for blast and impact resistance.

Contact: Wilfred E. Baker, Southwest Research Institute, P.O. Drawer 28510, San Antonio, TX 78284 - (512) 684-5111, Ext. 2303.

### APRIL

# ACOUSTICS AND NOISE CONTROL

Dates: April 14-18, 1980

Place: The University of Tennessee Space Inst. Objective: This is an introductory course dealing with the fundamentals of vibration and noise control. The equations governing the vibrations of continuous systems and sound propagation will be developed and certain elementary solutions derived to illustrate the basic characteristics of the wave motion. Sound propagation in the atmosphere, acoustic filters and resonators, and the attenuation of sound in rooms and ducts by acoustic treatment will be discussed. Fundamental measurement techniques and statistical parameters applicable to the description of noise will be presented.

Contact: Jules Bernard, The Univ. of Tennessee Space Institute, Tullahoma, TN 37388 - (615) 455-0631, Ext. 276.

# APPLICATIONS OF TIME SERIES ANALYSIS

Dates: April 14-18, 1980

Place: Institute of Sound and Vibration Re-

search, University of Southampton, UK

Objective: To provide a comprehensive treatment of time and frequency domain analysis methods for transient and stationary random signals summarizing essential theory and giving engineering applications. To present theories and some applications related to non-stationary processes, system identification and response of non-linear systems to stochastic excitation. To apply the theory to well conceived practical problems utilizing the computers in the Data Analysis Centre enabling participants to experience how new methods may be related to present day industrial requirements.

Contact: Dr. Joseph K. Hammond, Institute of Sound and Vibration Research, University of Southampton, Southampton, Hampshire, England, S09 5NH - 559122, Ext. 467.

# JUNE

# MACHINERY VIBRATIONS SEMINAR

Dates: June 24-26, 1980

Place: Mechanical Technology, Inc. Latham, New York

Objective: To cover the basic aspects of rotor-bearing system dynamics. The course will provide a fundamental understanding of rotating machinery vibrations; an awareness of available tools and techniques for the analysis and diagnosis of rotor vibration problems; and an appreciation of how these techniques are applied to correct vibration problems. Technical personnel who will benefit most from this course are those concerned with the rotor dynamics evaluation of motors, pumps, turbines, compressors, gearing, shafting, couplings, and similar mechanical equipment. The attendee should possess an engineering degree with some understanding of mechanics of materials and vibration theory. Appropriate job functions include machinery designers; and plant, manufacturing, or service engineers.

Contact: Mr. Paul Babson, MTI, 968 Albany-Shaker Rd., Latham, NY 12110 - (518) 785-2371.

# NEWS BRIEFS news on current and Future Shock and Vibration activities and events

# 1979 SAE AEROSPACE MEETING

The 1979 SAE Aerospace Meeting will be held at the Hyatt House at the Los Angeles Airport on December 3-6.

Topics to be covered are: Simulation - state of the art review; The need and prospects for multi-role transport aircraft; Advances in dynamic analysis & design; Advances in dynamic & modal analysis/testing; Options for heavy lift rotorcraft; and Options for high speed rotorcraft.

Registration fees are as follows: SAE members - no fee (membership card must be shown); Nonmember guests - \$15.00 daily (will be credited toward the combination of membership initiation fee and first year's dues, when elected, if application is made within six months), and \$48.00 for the entire meeting; College students - \$1.00 (college ID cards must be shown).

Papers will be on sale at \$1.95 each during the meeting in the SAE Publication Sales Area. Papers may also be ordered from SAE Headquarters at the following prices: Members \$1.95 each and Nonmembers \$2.95 each.

A tour of the Continental Airlines Maintenance Facilities will be held on Wednesday evening, December 5.

For further information or a complete program contact: Phil Columbus, SAE Headquarters, 400 Commonwealth Drive, Warrendale, PA 15096 - (412) 776-4841.

# **ABSTRACT CATEGORIES**

### **ANALYSIS AND DESIGN**

Analogs and Analog Computation **Analytical Methods Dynamic Programming** Impedance Methods Integral Transforms Nonlinear Analysis **Numerical Analysis Optimization Techniques Perturbation Methods** Stability Analysis Statistical Methods Variational Methods Finite Element Modeling Modeling Digital Simulation Parameter Identification **Design Information Design Techniques** Criteria, Standards, and **Specifications** Surveys and Bibliographies **Tutorial** Modal Analysis and Synthesis

### **COMPUTER PROGRAMS**

General Natural Frequency Random Response Stability Steady State Response Transient Response

# **ENVIRONMENTS**

Acoustic

Periodic
Random
Seismic
Shock
General Weapon
Transportation

# **PHENOMENOLOGY**

Composite
Damping
Elastic
Fatigue
Fluid
Inelastic
Soil
Thermoelastic
Viscoelastic

# **EXPERIMENTATION**

Balancing
Data Reduction
Diagnostics
Equipment
Experiment Design
Facilities
Instrumentation
Procedures
Scimulators
Specifications
Techniques
Holography

### COMPONENTS

Absorbers
Shafts
Beams, Strings, Rods, Bars
Bearings
Blades
Columns
Controls
Cylinders
Ducts
Frames, Arches
Gears
Isolators
Linkages
Mechanical
Membranes, Films, and Webs

Panels
Pipes and Tubes
Plates and Shells
Rings
Springs
Structural
Tires

# **SYSTEMS**

Ship

Spacecraft

Structural

**Transmissions** 

Turbomachinery

Useful Application

Absorber Acoustic Isolation Noise Reduction Active Isolation Aircraft Artillery Bioengineering **Bridges Building** Cabinets Construction Electrical Foundations and Earth Helicopters Human Isolation Material Handling Mechanical Metal Working and Forming Off-Road Vehicles Optical Package Pressure Vessels Pumps, Turbines, Fans, Compressors Rail Reactors Reciprocating Machine Rotors Satellite Self-Excited

# ABSTRACTS FROM THE CURRENT LITERATURE

Copies of articles abstracted in the DIGEST are not available from the SVIC or the Vibration Institute (except those generated by either organization). Inquiries should be directed to library resources. Government reports can be obtained from the National Technical Information Service, Springfield, VA 22151, by citing the AD-, PB-, or N- number. Doctoral dissertations are available from University Microfilms (UM), 313 N. Fir St., Ann Arbor, MI; U.S. Patents from the Commissioner of Patents, Washington, D.C. 20231. Addresses following the authors' names in the citation refer only to the first author. The list of periodicals scanned by this journal is printed in issues 1, 6, and 12.

# **ABSTRACT CONTENTS**

ANALYSIS AND DESIGN 42	EXPERIMENTATION 50	Structural
Analytical Methods 42	Balancing 50	
Optimization Techniques 42	Diagnostics 51	
Modeling	Equipment55	SYSTEMS
Criteria, Standards, and	Facilities	
Specifications43	Instrumentation	Noise Reduction 66
Surveys and	Scaling and Modeling 56	Active Isolation 67
Bibliographies 43	Techniques 56	Aircraft
	recimiques	Bridges 67
	COMPONENTS	Building
COMPUTER PROGRAMS44	COMI ONENIS.	Foundations and
	Shafts	Earth 68
General	Beams, Strings, Rods,	Helicopters 69
	Bars 56	Human
	Bearings	Isolation
	Blades	Mechanical
	Columns	Pumps, Turbines, Fans,
Acoustic	Controls 60	Compressors71
Periodic	Ducts 61	Rail
Random	Frames, Arches61	Reactors
Seismic	Gears 61	Reciprocating Machine 73
Shock	Linkages 62	Road
	Mechanical62	Rotors
	Membranes, Films, and	Ship
PHENOMENOLOGY48	Webs 62	Spacecraft
	Panels	Structural 76
Damping 48	Pipes and Tubes 63	Transmissions 76
Fatigue 49	Plates and Shells 64	Turbomachinery 76

# **ANALYSIS AND DESIGN**

# **ANALYTICAL METHODS**

(Also see Nos. 2236, 2237)

#### 79-2125

# The Role of Observations in Stochastic Linear Dynamic Models

T. Prasad and O. Ibidapo-Obe

Solid Mechanics Div., Univ. of Waterloo, Waterloo, Ontario, Canada N2L 3G1, Appl. Math. Modeling, 3 (4), pp 263-268 (Aug 1979) 4 figs, 3 tables, 20 refs

Key Words: Mathematical models, Stochastic processes

Emphasis is placed on using realistic observations for response evaluation in stochastic linear dynamic systems. A simulation study is performed. The structural model and the ensuing computational algorithms are presented, keeping in view their relevance to numerous applied problems of life sciences and technology.

# 79-2126

# The Effects of Internal Resonance on Impulsively Forced Non-Linear Systems with Two Degrees of Freedom

R.P. Vito and G. Cabak

School of Engrg. Science and Mechanics, Georgia Inst. of Tech., Atlanta, GA 30332, Intl. J. Nonlin. Mech., 14 (2), pp 93-99 (1979) 3 figs, 5 refs

Key Words: Internal resonance, Two degree of freedom systems

The method of multiple time scales is used to study the non-linear oscillations of impulsively forced systems under conditions of internal resonance. A partial analytical solution is obtained. The method is illustrated by an example in which the internal resonance effects are shown to be significant.

# 79-2127

Elastodynamics of Planar Mechanisms Using Planar Actual Finite Line Elements, Lumped Mass Systems, Matrix-Exponential Method, and the Method of "Critical-Geometry-Kineto-Elasto-Statics"

C. Bagci and S. Kalaycioglu

Tennessee Technological Univ., Cookeville, TN 38501 J. Mech. Des., Trans. ASME, <u>101</u> (3), pp 417-427 (July 1979) 32 figs, 1 table, 49 refs

Key Words: Mechanisms, Elastodynamic response

The article presents a general method for the elastodynamic analysis of planar mechanisms. It uses planar actual finite line elements and lumped mass systems to formulate the equations of motion of a mechanism. The matrix exponential method is introduced for the numerical solution of the equations of motion. Matrix displacement method of determining dynamic stresses using the generalized coordinate displacements is given. Elastodynamic analysis of a plane four-bar mechanism is performed for several cycles of kinematic motion, and the dynamic stresses are compared with those obtained by experiments.

# **OPTIMIZATION TECHNIQUES**

(Also see No. 2277)

### 79-2128

# Computational Techniques in Optimal State-Estimation -- A Tutorial Review

W. Kortum

German Research Ctr. for Aeronautics and Astronautics (DFVLR), Inst. for Dynamics of Flight Systems, Oberpfaffenhofen, Germany 8031, J. Dyn. Syst., Meas. and Control, Trans. ASME, 101 (2), pp 99-107 (June 1979) 2 figs, 3 tables, 19 refs

Key Words: Optimization, Dynamic systems, Reviews

The objective of this tutorial presentation is to review the main computational techniques of the state-estimation problem for linearizable dynamic systems where the design is oriented toward a minimum variance (quadratic loss, gaussian) estimation error. The continuous and the discrete estimation problem are both treated.

#### 79-2129

# Mechanism Optimization via Optimality Criterion Techniques

W.A. Thornton, K.D. Willmert, and M.R. Khan Clarkson College of Technology, Potsdam, NY 13676, J. Mech. Des., Trans. ASME, 101 (3), pp 392-397 (July 1979) 3 figs, 4 tables, 17 refs

Key Words: Mechanisms, Optimization

Presented in this paper are two new design techniques, based on optimality criteria, for selecting the cross-sectional sizes of the links within a mechanism. The objective is to minimize weight subject to stress and displacement (deformation) constraints. The mechanisms are assumed to be undergoing vibrational effects. These new optimality criterion methods are compared with a standard SUMT technique of nonlinear programming.

# MODELING

#### 79-2130

Modelling as an Aid in Measurement Technology, Part 1 (Modellbildung, ein Hilfsmittel der Messtechnik, Teil 1)

E.D. Gilles

Institut f. Systemdynamik und Regelungstechnik, Universität Stuttgart, Pfaffenwaldring 9, 7000 Stuttgart 80, West Germany, Techn. Messen-ATM, 46 (6), p 225 (June 1979) 13 figs, 16 refs (In German)

Key Words: Mathematical models, Measurement techniques

The use of mathematical models for the calculation of certain parameters in a mechanical system which cannot be measured directly is presented.

### 79-2131

Interactive Modeling and Analysis of Open or Closed Loop Dynamic Systems with Redundant Actuators R.J. Williams and A. Seireg

Pennsylvania State Univ., University Park, PA 16802, J. Mech. Des., Trans. ASME, <u>101</u> (3), pp 407-416 (July 1979) 11 figs, 39 refs

### Key Words: Mathematical models

This paper deals with the development of a computer-based procedure for the modeling and analysis of large displacement dynamic systems of the open or closed loop types. The procedure facilitates the construction of the model for such systems, automatically formulates the dynamic equations and provides the solution for any given input motion. The program is capable of analyzing complex systems with redundant force actuators utilizing a linear programming optimization scheme.

# CRITERIA, STANDARDS, AND SPECIFICATIONS

(See No. 2218)

# SURVEYS AND BIBLIOGRAPHIES

#### 79-2132

Recent Developments for the Nonlinear Distortion of Non-Dispersive Acoustic Waves. Part I: Planar Waves and the Basic Method

J.H. Ginsberg

School of Mech. Engrg., Purdue Univ., West Lafayette, IN 47907, Shock Vib. Dig., 11 (7), pp 3-8 (July 1979) 50 refs

Key Words: Reviews, Elastic waves

This two-part paper describes a perturbation procedure for investigating finite amplitude acoustic waves that depend on more than one spatial coordinate. The discussion focuses on wave motions that are non-dispersive in the linear approximation, in which case amplitude dispersion and self-refraction are the primary mechanisms for nonlinear distortion. Part I covers planar waves and the basic method.

# 79-2133

# Behavior of Elastomeric Materials Under Dynamic Loads - II

E.C. Hobaica

Electric Boat Div., General Dynamics Corp., Eastern Point Rd., Groton, CT 06340, Shock Vib. Dig., 11 (7), pp 11-18 (July 1979) 7 figs, 30 refs

Key Words: Reviews, Elastomers, Periodic excitation, Testing techniques

This review describes the properties of rubber and other elastomers when they are subjected to small amplitude sinusoidal stresses. Testing methods and data on dynamic properties are given.

blast waves or general time variant pressure waves. Solutions for a single constant area duct with the effects of viscosity at the wall are included. An example case is presented with a description of the single duct geometry, the applied nuclear blast parameters, and the code input parameters, including their magnitudes and their sources.

# 79-2134

# Approximate Techniques for Plastic Deformation of Structures Under Impulsive Loading. II

W.E. Baker

Southwest Research Inst., P.O. Box 28510, San Antonio, TX 78284, Shock Vib. Dig., 11 (7), pp 19-24 (July 1979) 4 figs, 1 table, 30 refs

Key Words: Reviews, Testing techniques, Impact response (mechanical)

Recent work on approximate techniques for plastic deformation of structures under impulsive loading is summarized. Research-oriented methods and design-oriented methods are described. Several design-oriented methods have been utilized by structural designers.

# **COMPUTER PROGRAMS**

# GENERAL

(Also see No. 2249)

### 79-2135

CEL Blast Wave Propagation Code for Air Ducts R.S. Chapler and R.H. Fashbaugh Civil Engrg. Lab. (Navy), Port Hueneme, CA, Rept. No. CEL-TN-1543, 64 pp (Jan 1979) AD-A066 259/3GA

Key Words: Shock wave propagation, Computer programs, Nuclear explosion effects, Ducts, Ventilation, Hardened installations

Refinement of a CEL hydrodynamic code for prediction of air blast propagation in variable area ventilation ducts was completed. Code solutions are one-dimensional and achieved using a refined finite-difference pseudo-viscosity method in a Lagrange formulation for solution of either classical nuclear

# **ENVIRONMENTS**

# ACOUSTIC

(Also see No. 2132)

#### 79-2136

# A New Type Flap Valve for Generating Sonic Booms in a Pyramidal Horn

J.J. Gottlieb, W. Czerwinski, N.N. Wahba, and R.E. Gnoyke

Inst. for Aerospace Studies, Toronto Univ., Ontario, Canada, Rept. No. UTIAS-208; CN-ISSN-0082-5255, 78 pp (Oct 1978)
N79-23755

Key Words: Sonic boom, Simulation

The design, operation and performance of a radically new type of sonic-boom generating flap-valve are described with emphasis on the ancillary cam, clutch, flywheel and electric motor system, and the air reservoir which is much larger than those used previously. An updated and greatly extended analysis describes the time varying reservoir conditions (e.g., pressure) and mass-flow rate of air through the flap valve, as well as the wave motion or characteristics of the traveling N-wave in the pyramidal concrete horn of traveling-wave sonic-boom simulation facility.

### 79-2137

# A Study of Scattering, Production, and Stimulated Emission of Sound by Vortex Flows

J.E. Yates

Aeronautical Research Associates of Princeton, Inc., NJ, Rept. No. NASA-CR-3139; ARAP-363, 62 pp (May 1979) N79-23756 Key Words: Fluid-induced excitation, Vortex noise, Acoustic scattering, Sound generation

The basic theory of aeroacoustics of homentropic fluid media is applied to the problems of sound scattering, production, and stimulated emission. A general theory of scattering from low speed three-dimensional vortex flows is presented. Specific results are given for the horseshoe vortex and vortex ring. The noise of an elementary corotating vortex pair in various flows is calculated.

appropriate farfield solution and expressed in terms of a scalar potential for the angular distribution of the scattered wave. This general method is adapted for a nonviscous random emulsion and the correlation function is expressed in terms of the intensity angular distribution of the scattered wave.

### 79-2138

# Potential Energy Effects on the Sound Speed in Liquids

B. Hartmann

Polymer Physics Group, Naval Surface Weapons Ctr., White Oak, Silver Spring, MD 20910, J. Acoust. Soc. Amer., <u>65</u> (6), pp 1392-1396 (June 1979) 1 fig, 22 refs

Key Words: Sound propagation, Liquids

Sound speed in liquids is calculated in terms of Mie potential parameters with the assumption that the intermolecular potential energy is the dominant factor. Using this simple model, it is shown that Beyer's parameter of nonlinearity, Rao's exponent, and the Gruneisen parameter are all simply related to each other.

### 79-2139

# Correlation Function Determination for Inhomogeneities Scattering an Acoustic Wave

J. Lewandowski

Dept. of Physical Acoustics, Inst. of Fundamental Technological Research, Polish Academy of Sciences, Warsaw, Poland, Arch. Acoust., 3 (4), pp 283-292 (1978) 7 refs

Key Words: Wave propagation, Wave diffraction, Elastic waves

A random inhomogeneous isotropic medium filling a domain immersed in an infinitely extended homogeneous isotropic medium is considered. The formulae describing the scalar potential of the scattered field are deduced for small and large distances from the domain of the heterogeneous material. The fluctuations of density and wave propagation velocity are treated as random variables of the space coordinates. The correlation function is calculated from the

### 79-2140

# Theoretical Study of Finite Amplitude Standing Waves in Rectangular Cavities with Perturbed Boundaries

M. Avdin

Naval Postgraduate School, Monterey, CA, 61 pp (Dec 1978)

AD-A066 356/7GA

Key Words: Sound waves, Resonant cavities

The effects of various geometrical boundary perturbations on finite-emplitude acoustical standing waves in a rectangular, rigid-walled cavity are investigated using non-linear theory. The standing waves that exist in an ideal cavity must be corrected when the boundaries are irregular. Three specific examples (stepped, linear and wedged perturbations) are worked out to demonstrate the corrections (in first order) near degeneracies for small perturbations. Those specific examples are compared to the experiments.

### 79-2141

# Virtual Modes and Mode Amplitudes Near Cutoff C.T. Tindle

Applied Research Labs., The Univ. of Texas at Austin, TX 78712, J. Acoust. Soc. Amer., <u>65</u> (6), pp 1423-1428 (June 1979) 5 figs, 8 refs

Key Words: Underwater sound, Normal modes

For a Pekeris model the contribution of the continuous mode integral is analyzed in terms of virtual modes with particular attention to cases with a discrete mode just below or just above cutoff. There is a steady change of amplitude as a virtual mode changes into a discrete mode. The mode amplitudes decay with range and analytic approximations valid in most practical situations are obtained.

#### 79-2142

# A Method of Predicting Noise Equivalent Level Value in Urban Structure

R. Makarewicz and G. Kerber Adam Mickiewicz Univ., Arch. Acoust., 3 (4), pp 231-248 (1978) 7 figs, 27 refs

Key Words: Urban noise, Noise prediction

The paper presents a method of predicting the noise equivalent level value in urban structure. The paper presents a solution of the problem of determination of the minimum number of the measurements of the parameter necessary to determine the noise equivalent level value with a preset accuracy.

# 79-2143

# An Analysis of Contoured Crystal Resonators Operating in Overtones of Coupled Thickness Shear and Thickness Twist

H.F. Tiersten and R.C. Smythe

Dept. of Mech. Engrg., Aeronautical Engrg. and Mechanics, Rensselaer Polytechnic Inst., Troy, NY 12181, J. Acoust. Soc. Amer., <u>65</u> (6), pp 1455-1460 (June 1979) 3 figs, 3 tables, 7 refs

Key Words: Quartz resonators, Variable cross section

A previous treatment of overtone modes in trapped energy resonators is extended to the case of plates with slowly varying thickness. The resulting single scalar equation is applied in the analysis of plano-convex contoured quartz crystal resonators, and a lumped parameter representation of the admittance, which is valid in the vicinity of a resonance, is obtained. The influence of piezoelectric stiffening, electrode mass loading, and electrical shorting is included in the analysis.

### PERIODIC

(Also see No. 2133)

### 70.2144

An Application of Newton's Diagram in the Periodic Solution of Quasiharmonic Oscillator, and the Stability of Such Solution (Une Application de Diagramme de Newton a la Recherche Des Solutions Periodiques D'un Oscillateur Quasiharmonique et L'etude de la

# Stabilite de Ces Solutions)

V. Carpent, J. Hubin, and G. Khmelevskaje-Plotni-kova

Facultes Universitaires Notre-Dame de la Paix, Namur, 61 rue de Bruxelles, Belgique, Intl. J. Nonlin. Mech., 14 (2), pp 67-80 (1979) 1 fig, 4 tables, 9 refs (In French)

Key Words: Periodic response

Periodic solutions of autonomous quasiharmonic systems are studied in the resonant case if the branching equation has multiple roots. Newton's diagram is used to find all the real solutions of this equation. The stability of the periodic solutions is also considered.

# RANDOM

# 79-2145

# Mathematical Model of the Stick-Slip Phenomenon J. Korycki

Working Liquids Group, Materials and Tech. Dept., Aviation Inst., Warsaw, Poland, Wear, <u>55</u> (2), pp 261-263 (Aug 1979) 1 fig, 6 refs

Key Words: Stick-slip response, Mathematical models

A mathematical model of the stick-slip phenomenon is presented which is related to the characteristic changes of the friction forces as a function of the slip speed. The model leads to simple differential equations without the necessity of using distribution equations. It can be utilized in a simple way to describe actual friction nodes.

### SEISMIC

# 79-2146

# Study of Selected Events in Pamirs in a Seismic Discrimination Context

P.A. Sobel, D.H. von Seggern, E.I. Sweetser, and D.W. Rivers

Seismic Data Analysis Center, Teledyne Geotech, Alexandria, VA, Rept. No. SDAC-TR-77-3, 74 pp (Oct 10, 1977)

AD-A066 325/2GA

Key Words: Seismic detection, Earthquakes

Eleven earthquakes with low reported M sub s for their m sub b from the Northern Pamirs were examined in a seismic discrimination context. Seismograms from ALPA, LASA, NORSAR, the HGLP and the WWSSN stations were studied for source mechanism, M sub s-m sub b, corner frequency, pP, complexity, and spectral ratio. All the Pamir events can be identified as earthquakes when their characteristics are compared to those of Kazakh explosions.

#### 79-2147

### Extraction of Seismic Waveforms

A.C. Strauss

Equipment Group, Texas Instruments, Inc., Dallas, TX, Rept. No. TI-ALEX(01)-TR-78-02, 75 pp (Sept 29, 1978)

AD-A066 711/3GA

Key Words: Seismic detection, Seismic waves

This report considers the effects on detectability and measurability resulting from attempts to extract seismic waveforms by application of cascaded processors and polarization filters.

### 79-2148

# Application of Ringdal's Method to Unbiased Measurement of the Ms-mb Relationship

A.C. Strauss

Equipment Group, Texas Instruments, Inc., Dallas, TX, Rept. No. TI-ALEX(01)-TR-78-03, 50 pp (Aug 31, 1978)

AD-A066 712/1GA

Key Words: Seismic detection, Seismic waves

Ringdal's maximum likelihood method of removing magnitude bias was tested by removing the apparent bias of surface wave magnitude estimates. Bias removal was demonstrated by comparing maximum likelihood estimates of M sub s obtained by a single sensor to those obtained by an array at the Alaskan Long Period Array (ALPA) site. Since the beamformed array has a lower detection threshold than the single-sensor reference site, it can serve as the standard by which to judge whether positive magnitude bias has been removed from the reference site surface wave magnitude estimates.

# 79-2149

# Short-Period Noise Envelope Statistics: A Basis for Envelope Detector Design

R. Unger

Equipment Group, Texas Instruments, Inc., Dallas, TX, Rept. No. TI-ALEX(01)-TR-78-05, 78 pp (Sept 26, 1978)

AD-A066 713/9GA

Key Words: Seismic detection, Seismic waves

This report focuses on the use of certain detection statistics, in particular the instantaneous amplitude or envelope, and the instantaneous power, in the design of a controlled false alarm rate detector. To achieve false alarm rate control, the detection statistic must be stationary, but need not be Gaussian. Parameters of a Gaussian process can be conveniently transformed into a stationary, normalized detection statistic.

# 79-2150

# Seismic Analysis of Internal Equipment and Components in Structures

J.L. Sackman and J.M. Kelly

Dept. of Civil Engrg., Univ. of California, Berkeley, CA, Engrg. Struc., 1 (4), pp 179-180 (July 1979) 7 figs, 20 refs

Key Words: Equipment response, Seismic response

In this paper, a rational approach to the design of lightly damped relatively light equipment in structures subjected to seismic loading or other forms of ground motion is presented. The analysis is carried out in the context of a model that consists of an N-degree of freedom structure to which is attached a single-degree-of-freedom component. An analytical method is developed whereby a simple estimate can be obtained of the maximum dynamic response of light equipment attached to a structure subjected to ground motion.

# SHOCK

(Also see Nos. 2134, 2135, 2272)

### 79-2151

The Structure of Shock Layers in Elastic-Plastic Media: Micro-Plastic Regime

R.W. Lardner and S. Ramakesavan

Dept. of Mathematics, Simon Fraser Univ., Burnaby, British Columbia V5A 1S6, Canada, Intl. J. Nonlin. Mech., 14 (2), pp 81-92 (1979) 5 figs, 15 refs

Key Words: Shock waves, Shock wave propagation, Elastoplastic properties

The Granato-Lücke theory of internal friction is used as the basis of a model of shock-wave formation and propagation in elasto-plastic solids below the general yield point. The structure of shock layers in such a model is shown to be in general asymmetric and, at sufficiently large jumps in strain, to exhibit oscillations in the strain at its trailing edge.

### 79-2152

# Extending Finite Element Methodology for a Class of Impact Problems

A.T. Change

Dept. of Mech. Engrg., Stevens Inst. of Tech., Hoboken, NJ, Rept. No. ARO-15522, 34 pp (Feb 1979) AD-A066 044/9GA

Key Words: Finite element technique, Impact response (mechanical)

This research has concentrated on a class of impact problems whose angle of impact is so shallow that the target impact disturbance might be considered as a surface wave problem. The theoretical background for the pressure distribution developed during impact is given in the last chapter.

### 79-2153

# Some Notes on the Dynamic Properties of Unsaturated Concrete

S.T. Wu

EBASCO Services, Inc., 2 Rector St., New York, NY 10006, Nucl. Engr. Des., <u>53</u> (1), pp 97-103 (June 1979) 9 figs, 1 table, 22 refs

Key Words: Concretes, Dynamic response

A simplified computation model is presented at the microscopic level to predict the dynamic behaviors of unsaturated concrete. The dynamic response to the stress waves are formulated and described. With certain assumptions, the transient mass flow from the hindered absorbed layer to the capillary pores can be evaluated in the transient state.

# **PHENOMENOLOGY**

# DAMPING

(Also see No. 2182)

### 79-2154

# Elastomer Mounted Rotors - An Alternative for Smoother Running Turbomachinery

J.A. Tecza, M.S. Darlow, S.W. Jones, A.J. Smalley, and R.E. Cunningham

Mechanical Technology Inc., Latham, NY, ASME Paper No. 79-GT-149

Key Words: Elastomeric dampers, Rotors (machine elements), Turbomachinery, Unbalanced mass response

This paper describes the design of elastomeric bearing supports for a rotor built to simulate the power turbine of an advanced gas turbine engine which traverses two bending critical speeds. The elastomer dampers are constructed to minimize rotor dynamic response at the critical speeds. Results are presented of unbalance response tests performed with two different elastomer materials.

### 79-2155

# The Response of a Single Degree of Freedom System with Quadratic Damping to Step and Impulse Inputs G. Jacazio and B. Piombo

Istituto di Meccanica Applicata alle Macchine, Politecnico, Torino, Italy, Mech. Res. Comm., <u>6</u> (3), pp 121-127 (1979) 4 figs, 3 refs

Key Words: Single degree of freedom systems, Quadratic damping

Single degree of freedom systems with quadratic damping are often encountered in mechanical systems; particularly in hydraulic systems where damping is often obtained by forcing oil to flow through a small orifice.

### 79-2156

A Design Point Correlation for Losses Due to Part-Span Dampers on Transonic Rotors W.B. Roberts

Dept. of Aerospace and Mech. Engrg., Univ. of Notre Dame, Notre Dame, IN, J. Engr. Power, Trans. ASME, 101 (3), pp 415-421 (June 1979) 11 figs, 20 refs

Key Words: Dampers, Fan blades

The design-point losses caused by part-span dampers are correlated for 21 transonic axial-flow fan rotors that have tip speeds varying from 350 to 488 meters per second and design pressure ratios of 1.5 to 2.0. The additional loss attributable to the damper and the total region along the blade height influenced are correlated with selected aerodynamic and geometric parameters.

79-2157

Oil Squeeze Film Dampers for Reducing Vibration of Aircraft Gas Turbine Engines

T. Miyachi, S. Hoshiya, Y. Sofue, M. Matsuki, and T. Torisaki

National Aerospace Lab., Tokyo, Japan, ASME Paper No. 79-GT-133

Key Words: Vibration dampers, Squeeze film dampers, Aircraft engines, Gas turbine engines

Theoretical analysis and experiments are carried out on cylindrical oil squeeze film dampers. The finite element method (FEM) is applied for calculating pressure distribution in the dampers with end seals and oil grooves. Measurements of the viscous damping coefficient of several dampers are conducted and compared with theoretical values. The effects of the dampers on the vibrational characteristics of engines are reviewed through theoretical analysis and experiments on an engine model. Then, the effects of squeeze film dampers on an actual engine are evaluated for design information.

**FATIGUE** 

(Also see No. 2184)

79-2158

The Effect of Frequency and Environment on the Fatigue-Crack Growth Behaviour of ASTM A533 Grade B Class 1 Weldment Material

C.J. Poon and D.W. Hoeppner

Univ. of Toronto, Toronto, Canada M5S 1A4, Intl. J. Fatigue, 1 (3), pp 141-152 (July 1979) 23 figs, 13 refs

Key Words: Fatigue (materials), Crack propagation

The effects of frequency and distilled water environment on the fatigue-crack growth characteristics of ASTM A533 Grade B Class 1 weldment material is studied with major emphasis placed on the crack growth along the weld centerline as well as along the heat affected zone (HAZ). A single deterministic fatigue-crack growth model based on the Four Parameter Weibull Survivorship Function is used.

79-2159

Environmental Dynamic Fatigue Crack Propagation in Nylon 66

H.A. ElHakeem and L.E. Culver

The National Inst. for Standards, Cairo, Egypt, Intl. J. Fatigue, 1 (3), pp 133-140 (July 1979) 9 figs, 1 table, 21 refs

Key Words: Fatigue (materials), Crack propagation

Standard samples of nylon 66 are pre-treated in either air, water, or dilute sulphuric acid and then notched and examined for fatigue crack propagation in the various environments. Tensile dynamic fatigue tests under constant sinusoidal load amplitudes are carried out at different frequencies.

79.2160

Gust Severity Effects on Fatigue Crack Propagation in Aluminum Alloy Sheet Materials

R.J.H. Wanhill

National Aerospace Lab., NLR, Amsterdam, The Netherlands, Intl. J. Fatigue,  $\underline{1}$  (3), pp 118-123 (July 1979) 10 figs, 16 refs

Key Words: Fatigue (materials), Crack propagation

Flight simulation fatigue tests are carried out on specimens of two aluminum alloys to investigate the effect of differing gust load experiences on fatigue crack propagation in 7075-T6 and the effect of gust load alleviation on 2024-T3. Two gust spectra were used: the Fokker F-27 spectrum for 7075-T6; and the reference spectrum TWIST for 2024-T3.

# **EXPERIMENTATION**

# BALANCING

# 79-2161 High Speed Rotor Balancing

W.D. Pilkev

Dept. of Mech. and Aerospace Engrg., Univ. of Virginia, Charlottesville, VA, Rept. No. UVA/525-088/MAE78/102, ARO-15080.7-E, 14 pp (Dec 1978) AD-A067 221/2GA

Key Words: Balancing techniques, Rotors (machine elements), Shafts (machine elements), Flexible rotors

This report summarizes the accomplishments of the final year of a study exploring new methods for balancing, analyzing, and designing flexible rotating shafts. A technique for identifying rotor bearing parameters is proposed. Then a quadratic programming formulation is presented for influence coefficient balancing with constraints. Finally, a method is developed for determining the optimal axial location of balancing planes.

# 79-2162 Synchronous Unbalance Response of an

Synchronous Unbalance Response of an Overhung Rotor with Disk Skew

D.J. Salamone and E.J. Gunter Allis-Chalmers Corp., Milwaukee, WI, ASME Paper No. 79-GT-135

Key Words: Balancing techniques, Rotors (machine elements)

This paper deals with the influence of disk skew on the synchronous unbalance response of flexible rotors in damped bearings. A simple overhung rotor is treated to illustrate the effects of various combinations of unbalance and disk skew on the amplitude and phase angle response at the disk and bearings.

### 79-2163

# Four Run Balancing Without Phase

P.O.L. Carlson

Electronic Dynamic Balancing Co., Hillside, IL, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 117-122, 7 figs

Key Words: Balancing techniques

The paper details the single plane balancing of a disc, flywheel or bladed fan such as a cooling tower fan. Other wider parts can be balanced at the center of gravity to accomplish a single plane balance.

### 79-2164

# An Introduction to a Unified Approach to Flexible Rotor Balancing

A.G. Parkinson, M.S. Darlow, A.J. Smalley, and R.H. Badgley

Univ. College of London, UK, ASME Paper No. 79-GT-161

Key Words: Balancing techniques, Flexible rotors, Rotors (machine elements)

Existing methods for the balancing of flexible rotors are discussed and a unified approach for such balancing is presented. A program for testing the method is also described.

### 79-2165

# Laser Balancing Demonstration on a High-Speed Flexible Rotor

R.S. DeMuth, R.A. Rio, and D.P. Fleming Mechanical Technology Inc., Latham, NY, ASME Paper No. 79-GT-56

Key Words: Balancing techniques, Lasers, Flexible rotors, Rotors (machine elements)

This paper describes a flexible rotor system used for twoplane laser balancing and an experimental demonstration of the laser material removal method for balancing. A laboratory test rotor was modified to accept balancing corrections using a laser metal removal method while the rotor is at operating speed. The laser setup hardware required to balance the rotor using two correction planes is described.

#### 79-2166

# Five-Plane Laser Balancing System for a Flexible Rotor

R.S. DeMuth

Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 123-128.9 figs. 2 refs

Key Words: Balancing techniques, Lasers, Flexible rotors

This paper describes the system for a five-plane laser balancing and experimental demonstration of the laser material removal method for balancing. A laboratory supercritical test rotor was modified to accept balancing corrections using a laser metal removal method while the rotor is at operating speed. The laser hardware required to balance the rotor using five correction planes is described. The optical table, laser module and laser controller were assembled and calibrated for material removal rates.

#### 79-2167

# TF30 Engine Trim Balancing and Vibration Diagnostic System

R.A. Rio, J. Rutledge, and F. Fanuele

Diagnostic Systems Section, Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 139-145, 3 figs, 1 table, 1 ref

Key Words: Balancing techniques, Diagnostic techniques, Aircraft engines

The Trim Balancing and Diagnostic System, installed in four TF30 engine test cells at the Oklahoma City Air Logistics Center (OC-ALC), is described. This project demonstrates the practical application of combining minicomputer technology with extensive rotor dynamics expertise to provide the Air Force with a system which solves many of the previously mentioned problems.

# DIAGNOSTICS

(Also see Nos. 2167, 2189)

### 79-2168

Machinery Vibration Monitoring and Analysis Semi-

# nar and Meeting Proceedings

Sponsored by Vibration Institute, Apr 1979, New Orleans, LA, Avail: Vibration Institute, 101 W. 55th St., Suite 206, Clarendon Hills, IL 60514

Key Words: Machinery vibration, Vibration monitoring, Diagnostic techniques

Twenty five papers presented at the Machinery Vibration Monitoring and Analysis Seminar and Meeting feature lectures on techniques for data analysis and problem identification and correction, and methods for evaluating and reporting data. The seminar was directed to individuals involved in the design, experimental testing, development and procurement of reciprocating and rotating machinery. Vibration problems likely to occur during the development and commissioning of new equipment are described. An annotated bibliography listing 198 items is also included. (Individual papers are also abstracted in this issue of the DIGEST).

#### 79-2169

# Random Test Generation for Fault Detection and Diagnosis

D.K. Goel

Ph.D. Thesis, Syracuse Univ., NY, 260 pp (1978) UM 7908534

# Key Words: Diagnostic techniques

A method of test generation is developed which aims at: eliminating the golden unit (a random test generation scheme in which the outputs of the golden unit and the circuit under test are compared); minimizing the length of the test sequence; reducing the complexity of deriving the tests; minimizing the chances of making a wrong decision; and minimizing the information required for reaching a decision about the state of the circuit. The testing procedure developed is analogous to the statistical hypothesis testing problem. Tests are derived for four different kinds of faults. The effectiveness of the tests is studied by randomly injecting faults into a circuit. A new testing procedure called the sequential probabilistic testing procedure is developed for the purpose of fault diagnosis. An algorithm is presented for computing the optimal sequential testing procedure for locating a fault.

# 79-2170

# The Practical Vibration Primer

C. Jackson

Gulf Publishing Co., Houston, TX, 1979, 114 pp, Avail: Vibration Institute, 101 W. 55th St., Clarendon Hills, IL 60514

Key Words: Diagnostic techniques, Machinery vibration, Books

The Practical Vibration Primer provides a working knowledge of the fundamentals required to evaluate malfunctions caused by excessive vibration. It begins with the basics of vibratory motion, and expands to cover the application of measurement and correction techniques. In addition to discussing motion-displacement, velocity, and acceleration of vibrating systems, with practical examples and illustrations to enhance understanding, the book describes various types of sensors used to measure vibration. Also provided are guidelines for selecting the proper machinery and structure vibration sensor. Other topics include logarithmic scaling, filters, phase and basic balancing (machine balancing techniques are illustrated with example problems), instrumentation, severity, thrust bearings, alignment, and information on how to avoid the common mistake of confusing strobe vibration analysis with probe vibration analysis.

### 79-2171

# Computer Managed Vibration Monitoring and Analysis of Plant Machinery

B. Buckley and J. Chavez

DYMAC Div. of Spectral Dynamics, San Diego, CA, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 183-189, 5 figs

Key Words: Diagnostic techniques, Turbomachinery

This paper describes some manufacturer's results in combining current computer and vibration instrumentation technology. This new system is dedicated to monitoring and analysis of plant turbomachinery (and auxiliary equipment) health and performance.

### 79-2172

# The Right Way to Overhaul Turbomachinery

J.D. Houghton

Shell Oil Co., Deer Park, TX, Hydrocarbon Processing, 58 (6), pp 129-136 (June 1979) 3 figs, 2 tables, 4 refs

Key Words: Diagnostic techniques, Turbomachinery

How to plan, execute and document turbomachinery overhauls are described based on data gathered on approximately 30 machines. Specific examples of what can go wrong and corrective action are also included.

#### 79-2173

# Investigating Steady State Vibrations in Large Engines and Reciprocating Compressors

T.J. Finneran

Ingersoll-Rand Co., Painted Post, NY, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 155-161, 10 figs

Key Words: Diagnostic techniques, Reciprocating engines, Periodic response

This paper is primarily concerned with the investigation of vibrations associated with large engines and reciprocating compressors, but is also applicable to other machinery. Its intent is to familiarize users of this equipment with some vibration principles, the major sources of excitation and the reasons why excessive vibrations may occur. It finally outlines investigatory procedures on vibration problems when they arise. First, the steps to be followed by observations; second, the steps to be followed using instruments. It concludes with some examples where these principles have been used.

# 79-2174

# Dynamic Analysis of a 7500 HP Induction Motor

J.E. Corley

Rotating Equipment, Arabian American Oil Co., Dhahran, Saudi Arabia, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 37-41, 6 figs

Key Words: Diagnostic techniques, Induction motors

This paper describes the diagnosis and analysis of two large four pole induction motors which are used in a crude oil loading system. The paper describes the techniques used to analyze the resonance and the experimental testing using an impedance analysis system to obtain the system stiffnesses necessary to model the system. The paper also presents the analysis of the recommended solution using an elliptical bearing to detune the horizontal resonance.

### 79-2175

# An Analysis Procedure for the Validation of On-Site Performance Measurements of Gas Turbines

R.K. Agrawal, B.D. MacIsaac, and H.I.H. Saravana-

Carleton Univ., Ottawa, Canada, J. Engr. Power, Trans. ASME, 101 (3), pp 405-414 (June 1979) 18 figs, 9 refs

Key Words: Diagnostic techniques, Gas turbine engines

In order to ensure accuracy and credibility of an engine health monitoring system, it is vital that the measurements used in the analysis process be accurate. An analysis procedure is developed to verify the accuracy of daily measurements taken from industrial gas turbines in the gas pipeline industry. The procedure is extended to use the measurements to develop an engine health monitoring system for this class of equipment which is based solely on existing instrumentation.

#### 79-2176

# Measurement Techniques for Preventing Fan Vibration Failures

P.K. Baade

Dynamics Research Div., Carrier Corp., Syracuse, NY 13221, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 27-36, 10 figs, 7 refs

Key Words: Fans, Diagnostic techniques, Critical speeds

This paper is concerned with the development of a practical measurement technique for predicting the critical speeds of propeller fans used in typical heating, refrigeration and air conditioning units. The paper reviews a typical fan failure history and describes tests conducted to diagnose the cause of the failure, as well as two different test methods which are candidates for an ASHRAE standard aimed at preventing such failures. Areas requiring further work are outlined.

### 79-2177

# Automating Signature Analysis for Predicting Machinery Failures

B.M. Rickert

Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 191-197

Key Words: Diagnostic techniques, Machinery, Vibration signatures, Signatures, Computer aided techniques

A system for nutomating the techniques of signature analysis, which reduces the cost of performing a detailed signature analysis by a factor of ten, is described.

#### 79-2178

# The Shock Pulse Method for Determining the Condition of Anti-Friction Bearings

K. Barthel

Testing Machines, Inc., Amityville, NY, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 199-204, 10 figs

Key Words: Diagnostic techniques, Shock pulse method, Antifriction bearings, Bearings

The Shock Pulse Method, which is based on monitoring the mechanical impacts caused by bearing damage and operating condition problems, is described. It allows a bearing's condition to be tested over its entire life.

#### 79-2179

# A Comparison of Vibration Measurement Techniques for Monitoring and Analysis

R.L. Fox

IRD Mechanalysis, Inc., Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 73-82, 15 figs

Key Words: Diagnostic techniques, Vibration measurement, Measuring instruments, Rotor-bearing systems

This paper discusses the three basic approaches in vibration measurement in terms of transducer selection and practical limitations. An evaluation of each measurement approach is made with consideration given to various rotor/bearing configurations as well as relative response to various specific machinery malfunctions and associated vibration characteristics. Recommendations and conclusions are supported with comparative spectrum analysis data of each measurement approach obtained on a variety of machinery installations.

### 79-2180

Identification of Gear Defects by Vibration Analysis
J.I. Taylor

Gardinier, Inc., Tampa, FL, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 93-105, 23 figs

Key Words: Diagnostic techniques, Vibration signatures, Gears

This paper describes procedures for identifying gear defects and/or problems. Analysis of vibration velocity signals in the time and frequency domains was utilized. The specific gear that causes the mesh problems can be identified by analyzing gear mesh frequencies.

### 79-2181

# Detection of Valve Leakage in Reciprocating Compressors by Demodulated Resonance Analysis

D.L. St. John

Shell Oil Co., Wood River, IL, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 177-182, 11 figs

Key Words: Diagnostic techniques, Valves, Compressors, Demodulated resonance analysis

This paper is a discussion of the relevant factors involved in successfully developing a technique to improve reciprocating compressor reliability and maintenance cost through the early detection of defective valves by demodulated resonance analysis.

### 79-2182

# An Effective Discriminant for Evaluating the Quality of Viscous Dampers Applied to EMD 20-645E3 Locomotive Engines

H. Hershkowitz

Applications Engrg., Scientific-Atlanta, Inc., Randolph, NJ, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 147-153, 6 figs, 4 tables, 7 refs

Key Words: Diagnostic techniques, Vibration dampers, Viscous damping, Torsional vibration

In situations where many different measured parameters describe the functional performance of a system, the meth-

ods of Multivariate Discriminatory Analysis allow the acceptreject criteria to be readily determined. This paper illustrates one such technique and demonstrates a means of estimating the quality of viscous torsional vibration dampers, where three measured parameters are associated with the determination.

### 79-2183

# Statistical Techniques for Automating the Detection of Anomalous Performance in Rotating Machinery K.R. Piety and T.E. Magette

Oak Ridge National Lab., Oak Ridge, TN 37830, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 163-176, 9 figs, 4 tables, 23 refs

Key Words: Diagnostic techniques, Statistical analysis, Automated testing, Rotating structures

A methodology for monitoring industrial rotating equipment which would upgrade ongoing programs and yet still be practical for implementation is investigated. An improved anomaly recognition methodology is formulated and implemented on a minicomputer system. The effectiveness of the monitoring system is evaluated in laboratory tests on a small rotor assembly, using vibrational signals from both displacement probes and accelerometers.

### 79-2184

# Simultaneous Monitoring of Acoustic Emission and Ultrasonic Attenuation During Fatigue of 7075 Aluminum

J.C. Duke, Jr. and R.E. Green, Jr.
College of Engrg., Virginia Polytechnic Inst. and State
Univ., Blacksburg, VA 24001, Intl. J. Fatigue, 1 (3),
pp 125-132 (July 1979) 9 figs, 40 refs

Key Words: Fatigue (materials), Diagnostic techniques, Acoustic emission

A thorough review of the previous work employing either technique (ultrasonic attenuation monitoring or acoustic emission monitoring) for the examination of aluminium during fatigue is presented.

# **EQUIPMENT**

(Also see No. 2150)

# INSTRUMENTATION

(Also see No. 2179)

### 79-2185

# Transient Analysis of Equipment-Structure Interaction at High Frequencies

J.L. Sackman and J.M. Kelly Weidlinger Associates, Menlo Park, CA, Rept. No. R-7828, DNA-4675F, 66 pp (May 1978) AD-A066 607/3GA

Key Words: Equipment response, Transient excitation

An analytical method is developed which yields a simple estimate of the maximum dynamic response of light equipment attached to a structure subjected to ground motions. The natural frequency of the equipment, modeled as a single-degree-of-freedom system, is considered to be close, or equal, to one of the natural frequencies of the N-degree-of-freedom structure. The approach is based on the transient analysis of lightly damped, tuned or detuned equipment-structure systems in which the mass of the equipment is small in comparison with that of the structure.

# **FACILITIES**

### 79-2186

# Measurements of Low-Velocity Flow Noise on Pressure and Pressure Gradient Hydrophones

R.A. Finger, L.A. Abbagnaro, and B.B. Bauer CBS Technology Center, Stamford, CT 06905, J. Acoust. Soc. Amer., <u>65</u> (6), pp 1407-1412 (June 1979) 7 figs, 9 refs

Key Words: Test facilities, Noise measurement, Fluid-induced excitation

A circular flow tank facility is developed which features extremely low acoustic and vibration ambient conditions. This facility is described, operating procedures associated with its use are presented, and limitations in the measurement procedures are mentioned. The flow facility is used to measure the noise output of pressure and pressure gradient hydrophones during actual flow conditions and results of these tests are presented and discussed.

#### 79-2187

Vibration Measurement - An Introduction to Piezoceramic Accelerometers and Associated Instrumentation - Part 2

D. Purdy

Noise Control Vib. Isolation, <u>10</u> (5), pp 178-181 (May 1979) 11 figs, 5 refs

Key Words: Vibration measurement, Measuring instrumentation. Accelerometers

In part 2 of this article, continued from the April 1979 issue, the conditioning of signals from piezoceramic accelerometers is discussed.

## 79-2188

# Concepts and Transducers Used in Measuring Dynamic Mass

R.R. Bouche

Bouche Labs., Sun Valley, CA, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 11-17, 7 figs, 7 refs

Key Words: Electrodynamic shakers, Vibration measurement, Measurement techniques, Measuring instruments

The general requirements for accurate dynamic mass measurements include using a small electrodynamic shaker together with an accelerometer and force gage having high sensitivities. The mechanical impedance or mobility can be computed from the measured dynamic mass simply by using the relationship between the velocity and acceleration for sinusoidal vibration motion. There are many important applications for the simplest form of dynamic mass measurements. These include measuring the dynamic mass at the driving point and the transfer dynamic mass while applying a single rectilinear force.

### 79-2189

# A Review of Machinery Analysis Instrumentation

J.S. Mitchell

Turbomachinery Consultant, San Juan Capistrano,

CA, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 1-9, 6 figs

Key Words: Machinery, Vibration analyzers, Measuring instruments

Vibration transducers, signal conditioning and some of the factors which must be considered in deciding which measurement to make are discussed. This paper is a condensation of three chapters in a comprehensive book on machinery analysis which will provide the reader with a good general basis for machinery analysis.

# **SCALING AND MODELING**

#### 79-2190

Use of Scaled Plastic Models in Mobility Studies
B.L. Bannister

Westinghouse Electric Corp., Lester, PA, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., New Orleans, LA, pp 19-23, 3 tables, 40 refs

Key Words: Scaling

This paper reviews the techniques that are used to design, construct and test scaled plastic models. Scaling laws, material characteristics, mobility analyses, experimental procedures, and test instrumentation are covered.

# TECHNIQUES

(See Nos. 2130, 2188)

# **COMPONENTS**

# SHAFTS

(Also see No. 2161)

### 79-2191

Shaft and Casing Motion of Large, Single Shaft, Industrial Gas Turbines

R.C. Eisenmann

North American Region, Bently Nevada Corp., Houston, TX, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 83-91, 10 figs

Key Words: Shafts, Gas turbines, Lateral vibration, Test equipment and instrumentation, Vibration tests

This paper addresses the shaft and casing vibration response characteristics of large, single shaft, industrial gas turbines. A contemporary suite of vibration transducers consisting of proximity displacement probes, velocity seismoprobes, and piezoelectric accelerometers are considered. The individual transducers are discussed, and the mechanical characteristics of gas turbines are reviewed. Finally, two specific machinery examples are presented to illustrate the various measurements, and data reduction techniques.

# BEAMS, STRINGS, RODS, BARS

### 79-2192

# Wave Motion in Micropolar Elastic Bars with Rectangular Cross Section

R.Y. Vasudeva and R.K. Bhaskara

Dept. of Appl. Mathematics, Andhra Univ., Waltair, India, Intl. J. Engr. Sci., 17 (8), pp 965-971 (1979) 9 refs

Key Words: Bears, Rectangular bars, Wave propagation, Frequency equation, Normal modes

Effect of couple stresses on the propagation of elastic waves in an infinite bar of rectangular cross section is studied in the framework of Eringen's micropolar theory of elasticity. The crosswise superposition technique is used to obtain the general solution and the frequency equation for longitudinal modes of vibration of the bar.

### 79-2193

# The Modelling of Net and Cloth Dynamics

C.M. Leech

Dept. of Mech. Engrg., The Univ. of Manchester Inst. of Science and Tech., Manchester, UK M60 1QD, J. Franklin Inst., 307 (6), pp 361-378 (1979) 6 figs, 17 refs

Key Words: Mathematical models, Grids (beam grids)

The dynamic modeling of dense nets, cloths and gridworks is approached through Hamilton's principle and Fourier series. The technique is examined in consequence of natural frequencies, travelling waves and wave propagation. The model is checked with previous results. The approach is extendible to laminates and to reinforcements.

### 79-2194

# Vibration Properties of Curved Thin-Walled Beams A. Rutenberg

Faculty of Civil Engrg., Technion-Israel Inst. of Tech., Haifa, Israel, ASCE J. Struc. Div., 105 (ST7), pp 1445-1455 (July 1979) 3 figs, 2 tables, 12 refs

Key Words: Beams, Curved beams, Bridges, Natural frequencies

A simple procedure is proposed to evaluate the out-of-plane vibration frequencies for a class of horizontally curved beams. The method is illustrated by a numerical example: a fixed-fixed curved highway with open cross-section.

# 79-2195

# On the Rectilinear Motion of an Inextensible String M. Kuipers

Dept. of Mathematics, Univ. of Groningen, Groningen, The Netherlands, J. Engr. Math., 13 (3), pp 249-256 (July 1979) 5 figs, 3 refs

Key Words: Strings, Chains, Normal modes

In this paper the rectilinear motion of a string or chain with no bending stiffness, which is arranged in a straight line and bent double is investigated. Two mechanisms, one of which is dissipative and the other is not are examined. The results of the calculations are compared with analogous computations in the literature.

# 79-2196 Inertial Effects of Masses Moving on Cables

J.L. Kanning Ph.D. Thesis, Purdue Univ., 163 pp (1978) UM 7914913 Key Words: Cables (ropes), Moving loads, Inertial forces

The effect of inertia on the motion of masses traveling on taut cables is investigated. An approximate analytical solution is presented. A numerical approach fully accounting for kinematical coupling effects is also presented. Finally, the numerical solution, developed for a moving point mass, is shown to be adaptable to systems with continuous moving masses, and the dynamic stability of tubular cantilevers conveying fluid is briefly investigated. The numerical results are compared with theoretical and experimental results from Gregory and Paidoussis.

# 79-2197

# Seismic Support: Speedy Determination of Frequency

A.K. Kar

Ebasco Services, Inc., New York, NY, ASCE J. Struc. Div., 105 (ST7), pp 1289-1306 (July 1979) 12 figs, 9 refs

Key Words: Cables (ropes), Seismic response, Nuclear power plants

Approximate formulas, based on the stiffness of the SDOF models, are presented to determine the natural frequencies very quickly and reliably. The formulas have the added advantage of demonstrating the contribution of different members to the frequency of a frame. The use of the formulas, presented in the paper, can considerably simplify the dynamic analysis of seismic supports for electrical cables and HVAC ducts in nuclear power plant and other structures.

### 79-2198

# Cable Spring Constants for Guyed Tower Analysis R.A. Skop

Appl. Mechanics Branch, Ocean Tech. Div., U.S. Naval Research Lab., Washington, D.C., ASCE J. Struc. Div., 105 (ST7), pp 1307-1318 (July 1979) 5 figs, 17 refs

Key Words: Cables (ropes), Towers, Guyed structures

In this paper new formulas are developed for calculating guy cable preloads and spring constants. The formulas are evolved for arbitrarily loaded guys containing any number of discrete masses and having arbitrary constitutive relations. The calculations of guy preloads and spring constants from these formulas are demonstrated by numerical examples.

# BEARINGS

(Also see No. 2178)

### 79-2199

# Dynamically Loaded Bearings Operating with Non-Newtonian Lubricant Films

Z.S. Safar

Mech. Engrg. Dept., Univ. of California, Berkeley, CA 94720, Wear, <u>55</u> (2), pp 295-304 (Aug 1979) 7 figs, 12 refs

Key Words: Bearings, Lubrication

The behavior of a laminar non-Newtonian film (power law) is studied for dynamically loaded bearings. An expression for the modified Reynolds equation in obtained for the non-Newtonian fluid film. The load-carrying capacity is obtained for various values of the viscometric exponent of the power law model.

#### 79-2200

# Predicting Wear in Misaligned Rolling Contact

P.A. Engel

IBM Corp., Endicott, NY, Mach. Des., <u>51</u> (17), pp 128-132 (July 26, 1979)

Key Words: Bearings, Wear, Alignment, Antifriction bearings

A new procedure for the determination of wear of rolling machinery components is described. The method shows how to determine the critical misalignment angle, given the contact geometry and elastic properties of two rolling surfaces. Then, from the critical misalignment angle, the maximum wear depth that can be expected at the contact area edge of the two surfaces is determined.

# 79-2201

# Analysis of Fitted Partial Arc and Tilting-Pad Journal Bearings

M.N. Abdul-Wahed, J. Frene, and D. Nicolas Institut National des Sciences Appliquees de Lyon, 69621 Villeurbanne, France, ASLE Trans., <u>22</u> (3), pp 257-266 (July 1979) 21 figs, 10 refs

Key Words: Bearings, Tilting pad bearings

As a step towards tilting fitted-pad bearing, calculated steadystate and dynamic characteristics are given for the finitelength fitted partial arc bearing for different values of bearing angle. Steady-state and dynamic characteristics are then given for a tilting-pad bearing with the load between pads. Results are compared with the similar clearance type bearing.

### 79-2202

# Geometry Effects in Tilting-Pad Journal Bearings G.J. Jones and F.A. Martin

The Glacier Metal Co., Ltd., Wembley, Middlesex, UK, ASLE Trans., 22 (3), pp 227-244 (July 1979) 14 figs, 2 tables, 12 refs

Key Words: Bearings, Tilting pad bearings, Geometric effects

A theoretical study is undertaken to show the influence of bearing geometry on the steady-state and dynamic behavior of tilting-pad journal bearings. The computer model used takes into account a different viscosity on each pad, turbulence in the oil film and pad inertia. The geometric changes considered include the pad clearance and the bearing clearance, the length/diameter ratio, the number of pads, and the orientation of the bearing with respect to the load direction. The major operating characteristics examined are oil film thickness, pad temperature, power loss, and oil film stiffness and damping.

### 79-2203

# Analytical and Experimental Determination of Surface Finish Effects on the EHD Performance of Ball Bearings

T.E. Russell and J.C. Clark

General Electric Co., Cincinnati, OH 45215, ASLE Trans., <u>22</u> (3), pp 286-292 (July 1979) 8 figs, 4 tables, 15 refs

Key Words: Bearings, Ball bearings, Fatigue tests, Surface roughness

An analytical and experimental analysis is conducted to determine the effects of surface finish on the elastohydrodynamic performance of a group of 168-mm bore diameter, gas turbine engine, main shaft ball bearings found to have discrepant outer raceway surface finishes.

### 79-2204

# Dynamics of Rolling-Element Bearings. Part 1: Cylindrical Roller Bearing Analysis

P.K. Gupta

Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, J. Lubric. Tech., Trans. ASME, 101 (3), pp 293-304 (July 1979) 8 figs, 14 refs

### Key Words: Bearings, Roller bearings

An analytical formulation for the roller motion in a cylindrical roller bearing is presented in terms of the classical differential equations of motion. Roller-race interaction is analyzed in detail and the resulting normal force and moment vectors are determined. Elastohydrodynamic traction models are considered in determining the roller-race tractive forces and moments. Formulation for the roller end and race flange interaction during skewing of the roller is also considered.

#### 79-2205

# Dynamics of Rolling-Element Bearings. Part II: Cylindrical Roller Bearing Results

P.K. Gupta

Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, J. Lubric. Tech., Trans. ASME, 101 (3), pp 305-311 (July 1979) 16 figs, 8 refs

### Key Words: Bearings, Roller bearings

Cylindrical roller bearing performance simulations are expressed in terms of the general motion of the bearing elements as derived by integrating the differential equations of motion. Roller skew as induced by relative race misalignment is simulated. The influence of geometrical parameters, such as roller/cage or race/cage clearance and radial preload, on the roller and cage motion is also investigated.

# 79-2206

# Dynamics of Rolling-Element Bearings. Part III: Ball Bearing Analysis

P.K. Gupta

Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, J. Lubric. Tech., Trans. ASME, 101 (3), pp 312-318 (July 1979) 5 figs, 19 refs

Key Words: Bearings, Ball bearings

An analytical formulation for the generalized ball, cage, and

race motion in a ball bearing is presented in terms of the classical differential equations of motion. Ball-race interaction is analyzed in detail and the resulting force and moment vectors are determined. The ball-cage and race-cage interactions are considered to be either hydrodynamic or metallic and a critical film thickness defines the transition between the two regimes. Simplified treatments for the drag and churning losses are also included to complete a rigorous analytical development for the real-time simulation of the dynamic performance of ball bearings.

# 79-2207

# Dynamics of Rolling-Element Bearings. Part IV: Ball Bearing Results

P.K. Gupta

Mechanical Technology Inc., 968 Albany-Shaker Rd., Latham, NY 12110, J. Lubric. Tech., Trans. ASME, 101 (3), pp 319-326 (July 1979) 24 figs, 9 refs

Key Words: Bearings, Ball bearings, Alignment

Dynamic simulations of the performance of a ball bearing are presented in terms of the general motion as obtained by integrating the differential equations of motion of the various bearing elements.

### 79-2208

# Elastohydrodynamic Contact Between Two Rollers Under Conditions of Unsteady Motion

S. Pytko and K. Wierzcholski

Dept. of Machines, Technical Univ. AGH, Krakow, Poland, Wear, <u>55</u> (2), pp 245-260 (Aug 1979) 2 figs, 2 tables, 3 refs

Key Words: Bearings, Rolling contact bearings, Rolling friction, Contact vibration, Elastohydrodynamic properties, Lubrication

An analysis of the elastohydrodynamic (EHD) contact between two rotating rollers in unsteady motion when one roller rolls around the other is presented.

### **BLADES**

### 79-2209

Optimization of Propeller Skew Distribution to Minimize the Vibratory Forces and Moments Acting at the Propeller Hub

M.G. Parsons and J.E. Greenblatt

Dept. of Naval Architecture and Marine Engrg., Michigan Univ., Ann Arbor, MI, Rept. No. UM/ NAME-206, MA-RD-940-79023, 66 pp (Dec 1978) PB-293 934/6GA

Key Words: Blades, Propeller blades, Marine propellers, Skew plates, Optimum design, Computer programs

The propeller skew design problem is formulated as an optimization problem to minimize a weighted, linear combination of the six vibratory forces and moments acting at the propeller hub. The SKEWOPT propeller skew optimization program is described. This interactive program was developed to perform the propeller skew optimization in a routine design setting. The vibratory forces and moments are evaluated using either a two-dimensional, sinusoidal gust theory or a three-dimensional, unsteady, lifting-line theory.

# **COLUMNS**

79-2210

Inelastic Response of Reinforced Concrete Columns Subjected to Two-Dimensional Earthquake Motion M.I.H. Suharwardy

Ph.D. Thesis, Univ. of Illinois at Urbana-Champaign, 225 pp (1979) UM 7915433

Key Words: Columns, Reinforced concrete, Earthquake response

This study was undertaken to determine the effects of two-dimensional earthquake motion on reinforced concrete (R/C) columns. An analytical model to represent the shear-deflection-axial load relationship of R/C columns is developed from stress-strain relations of steel and concrete. The analytical model compares favorably with experimental results for both uniaxial and biaxial loading conditions. The analytical model predicts significant changes in the strength, energy absorption capacity and accumulated damage responses of the column under biaxial deformations as compared to the corresponding responses under uniaxial deformations.

79.2211

Parametric Response of a Metallic Column at Elevated Temperature

G.J. Wang

Dept. of Mechanics and Materials Science, Rutgers Univ., New Brunswick, NJ 08903, Intl. J. Nonlin. Mech., 14 (2), pp 123-132 (1979) 5 figs, 13 refs

Key Words: Parametric resonance, Columns, Thermal excitation, Self-excited vibrations

The parametric response of a metallic column at elevated temperature is investigated, taking into account its non-linear viscous characteristics. An asymptotic method for the determination of the region of self-excitation and the amplitudes and phase angles for both stationary and non-stationary responses is outlined briefly.

# CONTROLS

(Also see No. 2181)

79-2212

Some Connections Between Modern and Classical Control Concepts

A.E. Bryson, Jr.

Paul Pigott Professor of Engrg., Stanford Univ., Stanford, CA 94305, J. Dyn. Syst., Meas. and Control, Trans. ASME, 101 (2), pp 91-98 (June 1979) 15 figs, 13 refs

Key Words: Control equipment, Structural synthesis

This is a tutorial paper that discusses the synthesis of optimum constant-gain feedback controllers for stationary linear systems. A fourth order example is used throughout the paper to help clarify the concepts.

79-2213

Experience with Experimental Applications of Multivariable Computer Control

D.E. Seborg and D.G. Fisher

Dept. of Chemical and Nuclear Engrg., Univ. of California, Santa Barbara, CA 93106, J. Dyn. Syst., Meas. and Control, Trans. ASME, 101 (2), pp 108-116 (June 1979) 12 figs, 38 refs

Key Words: Control equipment, Computer aided techniques

This paper summarizes experience gained over the past ten years in applying multivariable control techniques to a pilot

scale, double effect evaporator at the University of Alberta. It is possible to make meaningful comparisons between conventional control strategies and modern multivariable techniques including: optimal control, eigenvalue assignment, state estimation, adaptive control, frequency domain methods, time delay compensation, disturbance localization and model reference identification. The paper concludes with a discussion of the implications of this research for industrial application.

DUCTS

(Also see No. 2135)

### 79-2214

# A Statistical Theory for Sound Radiation and Reflection from a Duct

Y.C. Cho

Joint Inst. for Advancement of Flight Sciences, The George Washington Univ., NASA Langley Research Ctr., Hampton, VA 23665, J. Acoust. Soc. Amer., 65 (6), pp 1373-1379 (June 1979) 8 figs, 13 refs

Key Words: Ducts, Sound waves, Sound propagation, Sound reflection, Statistical analysis

A new analytical method is introduced for the study of the sound radiation and reflection from the open end of a duct. The sound is thought of as an aggregation of the quasi-particles-phonons. The motion of the latter is described in terms of the statistical distribution, which is derived from the classical wave theory. The results are in good agreement with the solutions obtained using the Wiener-Hopf technique.

# FRAMES, ARCHES

# 79-2215

# Reinforced Concrete Ductile Frames Under Earthquake Loadings with Stiffness Degradation

D. Soleimani

Ph.D. Thesis, Univ. of California, Berkeley, CA,533 pp (1978)
UM 7914772

Key Words: Frames, Reinforced concrete, Earthquake response

An extensive experimental and analytical research program for the inelastic response evaluation of ductile moment-resisting reinforced concrete multistory frame structures under strong earthquake motions is described. A twenty-story, four-bay strong column-weak beam reinforced concrete ductile frame, representing a typical office building, is designed in accordance with the seismic resistant 1970 UBC and 1971 ACI Code provisions. The influence of column axial deformations, flexural stiffness variations, and shear deformations on the static elastic analysis of the frame is examined.

# **GEARS**

(Also see No. 2180)

#### 79-2216

# Dynamic Behavior of Planetary Gear (4th Report, Influence of the Transmitted Tooth Load on the Dynamic Increment Load)

T. Hidaka, Y. Terauchi, and K. Ishioka Yamaguchi Univ., Tokiwadai, Ube, Japan, Bull. JSME, <u>22</u> (168), pp 877-884 (June 1979) 14 figs, 7 refs

Key Words: Gears

The influence of the transmitted tooth load on the dynamic increment load and others about a single-stage Stoeckicht planetary gear (Type 2K-H) constructed with spur gears is studied.

# 79-2217

# Why Gears Explode

R.J. Drago and F.W. Brown Boeing Vertol Co., Philadelphia, PA, Power Transm. Des., <u>21</u> (7), pp 77-80 (July 1979) 6 figs

Key Words: Gears, Resonant frequencies

Several experimental techniques for determining resonant frequencies and mode shapes of gearing components are described.

### 79-2218

Low-Cycle Fatigue and Ultimate Strength Related to Gear Design

W.L. Moore

The Boeing Co., Seattle, WA, J. Mech. Des., Trans. ASME, 101 (3), pp 373-379 (July 1979) 11 figs, 1 table, 16 refs

Key Words: Gears, Standards, Fatigue life

This paper describes the development of a method for assessing the ultimate tensile and limit load strength values required by MIL-A-8860(ASG) for aircraft actuator gear teeth, and the subsequent effect of a few very-high-load cycles with regard to bending and surface fatigue life. Background and application data are provided for gear teeth under relatively common load conditions that are not included in AGMA standards.

### LINKAGES

#### 79-2219

# Painless Analysis of Four-Bar Linkages

L.O. Barton

E.I. du Pont de Nemours & Co., Wilmington, DE, Mach. Des., <u>51</u> (17), pp 124-127 (July 26, 1979)

Key Words: Four bar mechanisms, Linkages

A technique is presented which simplifies the calculation of stresses, loads, vibration, and noise in a four-bar linkage by using elementary algebra and trigonometry to calculate link velocity and acceleration.

### MECHANICAL

### 79-2220

# Reaction Forces in Elastomeric Couplings

H. Schwerdlin

Lovejoy Inc., Downers Grove, IL, Mach. Des., <u>51</u> (16), pp 76-79 (July 12, 1979)

Key Words: Couplings, Flexible couplings, Testing techniques

Tests for the determination of reaction forces in flexible couplings caused by misalignment, speed and torque, and their effect on bearings, shafts, and other drive components are described.

### 79-2221

# Application of the Infinitesimal Operators of Translation and Rotation (No. 1. The Lineage of Dynamic Equations)

N. Oshima

Faculty of Engrg., Univ. of Tokyo, Hongo, Bunkyoku, Tokyo, Japan, Bull. JSME, 22 (168), pp 809-814 (June 1979) 4 figs, 2 refs

Key Words: Mechanical elements

Various mechanical quantities and conservation equations of dynamics can be arranged by means of appropriate infinitesimal operators. In the dynamics of point mass systems, the infinitesimal operators of translation and rotation yield various dynamical quantities from the energy form. Dynamics of a rigid body is considered from the view-point of infinitesimal operators.

#### 79-2222

# Coupling Response

H. Schwerdlin

Lovejoy Inc., Downers Grove, IL, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 57-62, 11 figs

Key Words: Couplings, Mechanical systems, Alignment

Reaction forces exerted on a mechanical system by the misalignment of couplings, torque, and speed were measured under controlled conditions. The system tested consisted of a four cylinder gasoline engine and disc brake dynamometer connected by a variety of flexible couplings.

# MEMBRANES, FILMS, AND WEBS

### 79-2223

# Forced Vibration of a Prestressed Rectangular Membrane: Near Resonance Response

V.O.S. Olunloyo and K. Hutter

Univ. of Lagos, Lagos, Nigeria, Acta Mech., 32 (1-3), pp 63-77 (1979) 2 figs, 5 refs

Key Words: Membranes (structural members), Rectangular membranes, Forced vibration, Resonant response, Viscous damping, Flexural stiffness, Anisotropy

Using singular perturbation the near resonance behavior of anisotropically prestressed thick rectangular membranes is analyzed to determine the effects of viscous damping, bending rigidity, prestress anisotropy and aspect ratio.

representative of laminated panels used in aircraft structures. Use is made of the shift hypothesis and shift factors of the epoxy matrix to study effects of environmental factors like temperature and moisture content.

### 79-2224

# Experiments on a Aerofoil at High Angle of Incidence in Longitudinal Oscillations

C. Maresca, D. Favier, and J. Rebont Institut de Mecanique des Fluides, Laboratoire Associe no. 3 du C.N.R.S., Marseille, J. Fluid Mech., 92 (4), pp 671-690 (June 27, 1979) 18 figs, 1 table, 12 refs

Key Words: Airfoils, Aerodynamic loads, Longitudinal response

Details of flow visualization, aerodynamic forces and pitching moment, static pressure and skin friction measurements are carried out on a symmetrical aerofoil at fixed angle of incidence in longitudinal oscillations parallel to the uniform airstream of a wind-tunnel.

### **PANELS**

### 79-2225

# Effects of Environment, Damping and Shear Deformations on Flutter of Laminated Composite Panels

S.N. Chatterjee and S.V. Kulkarni Materials Sciences Corp., Blue Bell Office Campus, Blue Bell, PA 19422, Intl. J. Solids Struc., <u>15</u> (6), pp 479-491 (1979) 8 figs, 2 tables, 34 refs

Key Words: Panels, Composite structures, Plates, Flutter, Damping effects, Transverse shear deformation effects

Flutter type instability of laminated fiber composite panels is studied based on piston theory aerodynamics and a laminated plate theory which includes the effects of shear deformations. Structural damping is considered in terms of frequency-dependent complex moduli of constituents. Stiffness of the laminae and the laminates are obtained by the use of well known elastic solutions and the dynamic elastic-viscoelastic correspondence principle. A modal method of solution is employed for obtaining flutter boundaries of panels which are constrained to deform in a state of plane deformation, i.e., cylindrical bending. Numerical results are reported for some Graphite/Epoxy laminates which are

# PIPES AND TUBES

### 79-2226

# Research on Wave Phenomena in Hydraulic Lines (5th Report, Coupled Vibration in Bending and Branching Lines)

S. Washio, T. Konishi, and T. Sonoda Kyoto Univ., Sakyo-ku, Kyoto, Japan, Bull. JSME, 22 (168), pp 833-840 (June 1979) 18 figs, 2 refs

Key Words: Piping systems, Lateral vibration, Hydraulic equipment, Coupled response

The roles of the lateral oscillation of a pipe in the coupled vibrations of pipes with oil in hydraulic circuits are studied. The vibrations are theoretically analyzed. Solid viscosity is introduced into the dynamics of a pipe wall to explain the damping of pipe oscillations. The pipe oscillation in the lateral direction is mathematically represented by several equations of bending vibration of a beam.

### 79-2227

# Dynamic Stability of a Liquid Carrying Pipe

A. Tylikowski

Inst. of Machine Design Fundamentals, Warsaw Technical Univ., Poland, Mech. Res. Comm., <u>6</u> (3), pp 141-146 (1979) 9 refs

Key Words: Pipes (tubes), Fluid-filled containers, Elastic foundations, Fluid-induced excitation

The stability of fluid carrying straight pipe laying on an elastic foundation is studied. Destabilizing effects of liquid motion as well as stochastic component of an axial force acting on the pipe are taken into consideration. The direct Liapunov-Movchan method is used to derive the sufficient stochastic stability conditions. Flexible hose with constant axial force and the liquid conveying pipe without elastic foundation are analyzed.

# **PLATES AND SHELLS**

### 79-2228

# Flutter of a Plate-Like Member in Horizontal Fluctuating Flow

E. Simiu and R.H. Scanlan
National Engrg. Lab., National Bureau of Standards,
Washington, D.C., Engrg. Struc., 1 (4), pp 207-210
(July 1979) 2 tables

Key Words: Flutter, Plates, Aerodynamic loads, Bridges

An investigation of the aerodynamic stability of a thin plate in horizontally fluctuating flow is considered in the solution of the problem of suspended-span bridge flutter.

### 79-2229

# Fluid Force on a Plate Moving Up-and-Down with a Finite Amplitude in the Still Fluid

H. Ueno and E. Kishioka

Faculty of Engrg., Kanazawa Univ., Kanazawa, Japan, Bull. JSME, 22 (168), pp 825-832 (June 1979) 17 figs, 3 refs

Key Words: Plates, Fluid-induced excitation

To investigate the fluid force acting on a body oscillating with a finite amplitude in a fluid extending to the infinite space, a brief theory is presented based on the virtual mass of the fluid taking into account the phase difference between the motion of the body and that of the virtual mass.

### 79-2230

# Experiments on Viscoplastic Response of Circular Plates to Impulsive Loading

S.R. Bodner and P.S. Symonds

Div. of Engrg., Brown Univ., Providence, RI 02912, J. Mech. Phys. Solids, <u>27</u> (2), pp 91-113 (Apr 1979) 21 figs, 2 tables, 13 refs

Key Words: Plates, Circular plates, Impact response (mechanical), Viscoplastic properties

Tests are described of circular plates of mild steel and commercially pure titanium loaded impulsively by means of explosive sheet. Three loading geometries are used, with magnitudes such that final deflections in the range from one to about seven plate thicknesses are produced. Clamping against radial as well as transverse deflections at the edge is provided. Parameters describing this behavior are obtained from stress-strain tests at low to intermediate rates together with published data for high strain rates. The measured final deflections and response times are compared with predictions of the mode approximation technique as extended to large deflections of viscoplastic structures.

# 79-2231

# Finite Viscoplastic Deflections of an Impulsively Loaded Plate by the Mode Approximation Technique

P.S. Symonds and C.T. Chon

Div. of Engrg., Brown Univ., Providence, RI 02912, J. Mech. Phys. Solids, <u>27</u> (2), pp 115-133 (Apr 1979) 5 figs, 22 refs

Key Words: Plates, Impact response (mechanical), Mode approximation technique, Viscoplastic properties

The application of the mode approximation technique to a fully clamped circular plate is described. Mode solutions for finite deflections are obtained from a sequence of instantaneous modes. Master solutions for chosen initial velocity amplitudes are constructed in nondimensional form. These depend weakly on a parameter of viscoplastic material behavior and size of structure, and so can be applied to a variety of loadings and structures. Finding each instantaneous mode shape and acceleration constitutes an eigenproblem, solved by finite elements with iterations. Comparisons with recent tests on steel and titanium plates are discussed in some detail.

### 79-2232

# The Effect of Mass Loading on a Stiffening Rib

B.L. Woolley

Naval Ocean Systems Center, San Diego, CA, Rept. No. NOSC/TR-286, 29 pp (Sept 1, 1978) AD-A066 614/9GA

Key Words: Acoustic scattering, Plates, Ribs (supports), Stiffening

In the scattering of an acoustic wave incident upon a ribreinforced plate, the effect of the rib can be characterized by a pair of impedances. One of these impedances is associated with the longitudinal vibrations of the rib, and the other impedance is associated with the flexural vibrations of the rib. This report calculates the impedances and the effect of mass loading on these impedances. The calculations are done for a thick or Timoshenko-Mindlin rib which is fluid loaded with the rib immersed either in water or air.

#### 79-2233

# Flow and Heat Transfer Due to Small Torsional Oscillations of a Disk About a Constant Mean

V.P. Sharma

Dept. of Mathematics, Indian Inst. of Tech., Kharagpur, India, Acta Mech., <u>32</u> (1-3), pp 19-34 (1979) 3 figs, 7 refs

Key Words: Disks, Torsional vibration

The paper deals with the study of flow and heat transfer in a viscous fluid from a disk performing small rotating oscillations about a constant mean. Separate solutions for low and high frequency ranges are developed.

# 79-2234

# Natural Frequencies of Thin-Walled Isotropic, Circular-Cylindrical Shells

Engrg. Sciences Data Unit, London, UK, Rept. No. ESDU-78004; ISBN-0-85679-226-8, 46 pp (1978) N79-21415

Key Words: Cylindrical shells, Natural frequencies, Flexural vibrations, Torsional vibration, Chimneys, Wind-induced excitation

Graphical and tabulated data for the estimation of the lower natural frequencies of thin-walled unstiffened shells are discussed. Natural frequencies of initially unstressed shells for both flexural and torsional vibration are considered. For each combination of these mode numbers there are three natural frequencies in which the vibrating motion is either primarily radial, axial, or circumferential. Natural frequencies of shells subjected to uniform static loads are considered, and shell modal density data are given. Response calculations of shells under wide band excitation, when using statistical energy analysis methods are studied. The limitations of data presented, and some guidance on the calculation of stiffened shell natural frequencies is given. Applications include estimation of the response of shells subject to high intensity acoustic loading and estimation of natural frequencies of chimneys subject to wind loads.

#### 79-2235

# The Seismic Response of a Column-Supported Cooling Tower

C.S. Gran

Ph.D. Thesis, Purdue Univ., 142 pp (1978) UM 7914901

Key Words: Cooling towers, Shells, Seismic response

Hyperboloidal reinforced-concrete shells are modeled using orthotropic quadrilateral flat plate finite elements. The supporting columns and top ring beam are modeled by beam finite elements. Natural frequencies and corresponding mode shapes are found for several different tower configurations. Results for fixed-base shells are in close agreement with those determined using alternate methods of analysis. A cooling tower in the 1200 MW Fossil Fuel Steam Generating Power Plant at Paradise, Kentucky (Tennessee Valley Authority) is studied.

# STRUCTURAL

#### 79-2236

# The Method of Quasimodal Form Solutions for the Dynamic Response of Rigid-Plastic Structures

U. Lepik

Tartu State Univ., Tartu, Estonian S.S.R., USSR, Mech. Res. Comm., <u>6</u> (3), pp 135-140 (1979) 1 fig, 1 table, 4 refs

Key Words: Dynamic response, Structural members

A technique for the analysis of a rigid-plastic thin-walled structure subjected to high dynamic loads, causing plastic hinges, is presented.

# 79-2237

# Accelerated Convergence of Dynamic Flexibility in Series Form

Y.T. Leung

Dept. of Civil Engrg, Univ. of Hong Kong, Hong Kong, Engrg. Struc., 1 (4), pp 203-206 (July 1979) 2 figs, 8 refs

Key Words: Dynamic structural analysis, Natural frequencies, Beams, Plates

In a natural vibration analysis of a structural system, the conventional dynamic flexibility (receptance) matrix in series forms is re-examined. Examples involving beams and plates are given. The method is suitable for dynamic substructure analysis.

# SEALS

### 79-2238

Aeroelastic Instability in F100 Labyrinth Air Seals D.A. Lewis, C.E. Platt, and E.B. Smith Pratt & Whitney Aircraft Group, West Palm Beach, FL, J. Aircraft, 16 (7), pp 484-490 (July 1979) 10 figs, 12 refs

Key Words: Seals (stoppers), Stability analysis

The aeroelastic instability in F100 labyrinth air seals is investigated.

#### 79-2239

# Stiffness of Straight and Tapered Annular Gas Path Seals

D.P. Fleming

NASA Lewis Research Ctr., Cleveland, OH 44135, J. Lubric. Tech., Trans. ASME, <u>101</u> (3), pp 349-355 (July 1979) 7 figs, 13 refs

Key Words: Seals (stoppers)

Radial stiffness of annular (ring-type) gas path seals is calculated for both constant-clearance designs and tapered designs for which the inlet clearance is larger than the outlet clearance.

### 79-2240

# Hydrodynamic Effects in a Misaligned Radial Face Seal

I. Etsion

Dept. of Mech. Engrg., Technion-Israel Inst. of Tech., Haifa, Israel, J. Lubric. Tech., Trans. ASME, 101 (3), pp 283-292 (July 1979) 6 figs, 23 refs

Key Words: Seals (stoppers), Alignment, Hydrodynamic excitation

Hydrodynamic effects in a flat seal having an angular misalignment are analyzed, taking into account the radial variation in seal clearance. An analytical solution for axial force, restoring moment, and transverse moment is presented that covers the whole range from zero to full angular misalignment. Both low pressure seals with cavitating flow and high pressure seals with full fluid film are considered.

# **SYSTEMS**

# **NOISE REDUCTION**

# 79-2241

# Impulse Wave Diffraction by Rigid Wedges and Plates J.H. Bremhorst

Naval Postgraduate School, Monterey, CA, 114 pp (Dec 1978) AD-A066 476/3GA

Key Words: Noise barriers, Wedges, Plates, Acoustic diffraction, Acoustic absorption

The problem of diffraction of acoustic signals by rigid barriers is studied empirically. Backward and forward diffraction from a 90 degree wedge and a thin plate are analyzed. Attempts to measure the diffracted energy in the illuminated region over the apex of the barrier, when direct and reflected signals coexist with diffracted, are discussed. Factors influencing the choice of the barriers physical dimensions and composition are listed, as are the problems surrounding the selection of an ideal sound source and receiver.

### 79-2242

# Practical Applications of Outdoor Noise Control Barriers

G.C. Tocci and W.H. Pickett Cavanaugh Tocci Associates, Natick, MA, S/V, Sound Vib., 13 (6), pp 10-16 (1979) 17 figs, 10 refs

Key Words: Noise barriers

An overview of noise barrier attenuation estimation procedures is presented for both general noise barrier problems and in forms which incorporate simplifying approximations for implementation in specific noise barrier problems. Estimation procedures for assessing the effect of wind and scattering of sound by trees are also described. Typical applications of outdoor noise barriers are discussed as well.

# **ACTIVE ISOLATION**

# 79-2243

# Design and Development of a Motion Compensator for the RSRA Main Rotor Control

P. Jeffrey and R. Huber

Sikorsky Aircraft, Stratford, CT, In: NASA Johnson Space Ctr., The 13th Aerospace Mech. Symp, pp 15-25 (1979) N79-22541

Key Words: Active isolation, Helicopter rotors

The RSRA, an experimental helicopter, is equipped with an active isolation system that allows the transmission to move relative to the fuselage. The purpose of the motion compensator is to prevent these motions from introducing unwanted signals to the main rotor control. A motion compensator concept is developed that has six-degree-of-freedom capability. The mechanism is implemented on RSRA and its performance verified by ground and flight tests.

# **AIRCRAFT**

### 79-2244

# Aeroservoelastic Encounters

L.R. Felt, L.J. Huttsell, T.E. Noll, and D.E. Cooley Air Force Flight Dynamics Lab., Wright-Patterson AFB, OH, J. Aircraft, 16 (7), pp 477-483 (July 1979) 13 figs, 23 refs

Key Words: Flight vehicles

Recent Air Force experiences that emphasize the need for aeroservoelastic considerations on a variety of research, development, prototype, and production aircraft are presented in this paper. Typical analysis and test techniques available to predict and prevent adverse aeroservoelastic effects are presented. The results of two in-house aeroservoelastic analyses are presented.

# 79-2245

# Wing Store Active Flutter Suppression - Correlation of Analyses and Wind-Tunnel Data

T.E. Noll and L.J. Huttsell

Air Force Flight Dynamics Lab., Wright-Patterson AFB, OH, J. Aircraft, 16 (7), pp 491-497 (July 1979) 14 figs, 8 refs

Key Words: Aircraft wings, Wing stores, Flutter, Vibration control

The results of an tallytical effort to study the behavior of an active flutter suppression wind-tunnel model are presented and compared with available test data. For this application, the model was aerodynamically represented by subsonic doublet lattice theory and stability was evaluated using modified Nyquist criteria.

#### 79-2246

# Physical and Subjective Studies of Aircraft Interior Noise and Vibration

D.G. Stephens and J.D. Leatherwood NASA Langley Research Ctr., Hampton, VA, Rept. No. NASA-TM-80084, 16 pp (Apr 1979) N79-23754

Key Words: Aircraft noise, Interior noise, Interior vibration, Helicopter noise

Measurements to define and quantify the interior noise and vibration stimuli of aircraft are reviewed as well as field and simulation studies to determine the subjective response to such stimuli, and theoretical and experimental studies to predict and control the interior environment. In addition, ride quality criteria/standards for noise, vibration, and combinations of these stimuli are discussed in relation to the helicopter cabin environment. Data on passenger response are presented to illustrate the effects of interior noise and passengers.

# **BRIDGES**

(Also see No. 2228)

# 79-2247

# Fatigue Tests of Full-Size-Prestressed Girders

B.G. Rabbat, P.H. Kaar, H.G. Russell, and R.N. Bruce, Jr.

Construction Technology Labs., Portland Cement Assn., Skokie, IL, Rept. No. FHWA/LA-78-206(P), 148 pp (June 1978) PB-294 291/0GA

Key Words: Bridges, Girders, Fatigue tests

An experimental investigation was carried out to determine the effect of repetitive loading on the behavior and strength of girders with draped and blanketed strands. Controlled variables in the test program were load level, development length, and use of ties to confine the concrete in the stress transfer region of the blanketed strands.

# BUILDING

(Also see No. 2261)

### 79-2248

# Earthquake Analysis of Belted High-Rise Building Structures

A. Rutenberg

Faculty of Civil Engrg., Technion-Israel Inst. of Tech., Haifa, Israel, Engrg. Struc., 1 (4), pp 191-196 (July 1979) 9 figs, 1 table, 6 refs

Key Words: Multistory buildings, Earthquake response, Seismic response, Modal analysis

A modal analysis procedure is presented for the seismic response of belted high-rise building structures within the framework of the response spectrum technique. The first 3-modes of vibration are considered. Natural periods, internal forces and deflections are computed, and design charts are presented for the parameters of interest. Based on the Applied Technology Council tentative seismic provisions, a numerical example is worked out to illustrate the use of the charts, and a comparison is made with the ATC equivalent lateral force procedure.

### 79-2249

# The Buffeting of Tall Structures by Strong Winds, Windload Program

E. Simiu and D.W. Lozier

Center for Bldg. Technology, National Engrg. Lab (NBS), Washington, D.C., Rept. No. NBS/DF-79/001 (1979)

PB-294 757/0GA

Key Words: Buildings, Wind-induced excitation, Computer programs

A computer program is presented for the calculation of the along-wind response of tall buildings. Program input includes building dimensions, natural frequencies, damping coefficients, modal shapes, and weight distribution, design wind speed, roughness of surrounding terrain, pressure coefficients on windward and leeward faces, and specific weight of air. The output consists of mean, rms, and peak deflections, and rms and peak accelerations.

# **FOUNDATIONS AND EARTH**

### 79-2250

# Turbomachinery Foundations Practical Aspects

J.S. Sohre

One Lakeview Circle, Ware, MA 01082, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 129-137, 10 figs, 2 refs

Key Words: Machine foundations, Turbomachinery

This presentation explains the practical and theoretical requirements for the design of foundations for high speed machinery.

### 79-2251

# Vertical and Torsional Stiffnesses of Cylindrical Footings

E. Kausel and R. Ushijima

Constructed Facilities Div., Massachusetts Inst. of Tech., Cambridge, MA, Rept. No. R79-6, 73 pp (Feb 1979)
PB-293 997/3GA

Key Words: Footings, Torsional response

A numerical evaluation of the vertical and torsional stiffnesses of a cylindrical foundation embedded in an elastic stratum is presented. Empirical formulas are given that relate stiffnesses and damping values with the embedment ratio and the depth of the stratum. Good agreement is found between the reported approximations and available analytical solutions for particular geometries. 79-2252

# Analysis of Lateral Response of Non-Uniform Section

H.G. Poulos and M.A. Adler Civil Engrg. Labs., Sydney Univ., Australia, Rept. No. R-330, 37 pp (Oct 1978) PB-294 255/5GA

Key Words: Pile structures, Lateral response, Finite element technique, Finite difference theory

Two alternative methods of analyzing the lateral response of a pile of non-uniform section in an elasto-plastic soil mass are presented. The first utilizes a finite element formulation for the pile while the second uses a finite difference formulation. Some parametric solutions are presented for a uniformly tapered pile, and these are presented as correction factors to the solutions for uniform section piles. Finally, two practical examples are given to illustrate the application of the analysis.

79-2253

# Dynamic Response of Elastic Plates on the Surface of the Half-Space

S.A. Savidis and T. Richter
Inst. of Soil Mechanics and Foundation Engrg., Technical Univ., Berlin, Germany, Intl. J. Numer. Anal.
Methods Geomech., 3 (3), pp 245-254 (July-Sept 1979) 8 figs, 13 refs

Key Words: Interaction: soil-foundation, Half-space, Foundations

A mixed method for the dynamic calculation of foundations on soil is presented. The half-space is computed analytically, the foundation with finite elements. The method is very we!! suited for the solution of three-dimensional problems including interaction. Numerical results for a simple case involving a dynamically loaded elastic plate are presented and the influence of plate stiffness is studied.

HELICOPTERS

(Also see Nos. 2243, 2246, 2285)

79-2254

Fatigue of Helicopters: Service Life Evaluation Method F. Liard

Helicopter Div., Societe Nationale Industrielle Aerospatiale, Paris, France, In: AGARD Helicopter Fatigue, pp 47-69 (Feb 1979)
N79-23079

Key Words: Helicopters, Fatigue tests

The general principle of fatigue substantiation for helicopter components consists in evaluating the fatigue strength of the component, determining the value and frequency of the loads to which it will be subjected during normal operation, and then deriving from these data the steps to be taken to make the possible occurrence of serious accidents due to the failure of the component extremely remote.

79-2255

# Present Fatigue Analysis and Design of Helicopters. Requirements and Qualification Procedures

P. Alli

Costruzioni Aeronautiche Giovanni Agusta S.p.A., Gallarate, Italy, In: AGARD Helicopter Fatigue, pp 29-46 (Feb 1979) N79-23078

Key Words: Helicopters, Fatigue tests

The state-of-the-art in AGUSTA in the area of structural fatigue and fail-safe strength evaluation is reported. The need of general regulations and procedures was pointed out. The convenience of automatic procedures was underlined.

79-2256

# Fatigue Life Estimation Methods for Helicopter Structural Parts

F Oct

Messerschmitt-Boelkow-Blohm G.m.b.H., Munich, West Germany, In: AGARD Helicopter Fatigue, pp 21-27 (Feb 1979) N79-23077

Key Words: Helicopters, Fatigue tests

Analytical fatigue life estimation mainly consists of three steps: prediction of loads, determination of fatigue strength, and application of a damage hypothesis linking these two aspects. Following the above mentioned three steps of fatigue life investigation, methods for the prediction of

loads are dealt with according to the available amount of information. Methods describing the fatigue strength of components, taking into account the influence of steady loads and the reduction of a mean S/N curve to a working level curve are investigated.

### 79-2257

### Helicopter Fatigue Evaluation. The UK Approach A.D. Hall

Westland Helicopters Ltd., Yeovil, UK, In: AGARD Helicopter Fatigue, pp 13-20 (Feb 1979) N79-23076

Key Words: Helicopters, Fatigue tests

The philosophies of fatigue substantiation are used satisfactorily for the Lynx. The main concern is with the safe fatigue life substantiation of the vital components of a helicopter and consideration is given to three phases in the life cycle, i.e., design, development, and production.

### 79-2258

### U.S. Army Helicopter Fatigue Requirements and Substantiation Procedures

R.A. Wolfe and R.W. Arden

Structures and Aeromechanics Branch, Army Aviation Res. & Dev. Command, St. Louis, MO, In: AGARD Helicopter Fatigue, pp 1-12 (Feb 1979) N79-23075

Key Words: Helicopters, Fatigue tests

The current fatigue criteria and testing requirements are provided for U.S. Army helicopter structures with primary emphasis on dynamic components. The comparative industry applications of the requirements were brought to light as a result of the Army's latest major helicopter competitions for the Utility Tactical Transport Aircraft System, recently designated BLACK HAWK, and the Advanced Attack Helicopter.

79-2259

Correlation Study Between Vibrational Environ-

### mental and Failure Rates of Civil Helicopter Components

O. Alaniz

Textron Bell Helicopter, Fort Worth, TX, Rept. No. NASA-CR-159033, 75 pp (May 1979) N79-23064

Key Words: Helicopters, Vibration control

An investigation of two selected helicopter types, namely, the Models 206A/B and 212, is reported. An analysis of the available vibration and reliability data for these two helicopter types resulted in the selection of ten components located in five different areas of the helicopter and consisting primarily of instruments, electrical components, and other noncritical flight hardware. The potential for advanced technology in suppressing vibration in helicopters was assessed.

#### 79-2260

# Rotary-Wing Aerodynamics. Volume 1: Basic Theories of Rotor Aerodynamics with Application to Helicopters

W.Z. Stepniewski

Boeing Vertol Co., Philadelphia, PA, Rept. No. NASA-CR-3082, 302 pp (Jan 1979) N79-22039

Key Words: Rotary wings, Helicopters, Aerodynamic loads

The concept of rotary-wing aircraft in general is defined. The energy effectiveness of helicopters is compared with that of other static thrust generators in hover, as well as with various air and ground vehicles in forward translation. The most important aspects of rotor-blade dynamics and rotor control are reviewed. The combined blade-element and momentum theory approach is described as well as the vortex theory which models a rotor blade by means of a vortex filament or vorticity surface. The application the the velocity and acceleration potential theory to the determination of flow fields around three dimensional non-rotating bodies as well as to rotor aerodynamic problems is described. Airfoil sections suitable for rotors are also considered.

HUMAN

(See No. 2278)

### **ISOLATION**

### PUMPS, TURBINES, FANS, COMPRESSORS

(Also see No. 2176)

### 79-2261

Optimal Design of an Earthquake Isolation System M.A. Bhatti, K.S. Pister, and E. Polak

Earthquake Engrg. Research Ctr., California Univ., Richmond, CA, Rept. No. UCB/EERC-78/22, NSF/ RA-780544, 120 pp (Oct 1978) PB-294 735/6GA

Key Words: Isolators, Buildings, Seismic design, Earthquake resistant structures, Energy absorption

Optimal design of an earthquake isolation system, consisting of natural rubber bearings and special nonlinear energy absorbing devices, is presented. An algorithm for efficient analysis of structural response, based upon the Newmark and Runge-Kutta methods with optional Newton-Raphson iteration, is given. The optimal design problem, incorporating this simulation algorithm, is formulated as a mathematical programming problem with time-dependent constraints and is solved using a feasible directions algorithm. Several numerical examples are presented.

### MECHANICAL

### 79-2262

### Don't Forget the Basics

J.P. Platt, Jr.

Standard Oil Co. (Indiana), Naperville, IL, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 51-55, 3 tables

Key Words: Machinery vibration

This paper presents five simple machinery vibration problems. It is the intent of this paper to make the modern machinery vibration analyst more effective by re-focusing his attention on the basics of machinery vibration problems.

### 79-2263

### Computer Aided Design of Mixed Flow Turbines for Turbochargers

N.C. Baines, F.J. Wallace, and A. Whitfield Dept. of Engrg., Univ. of Bath, Bath, UK, J. Engr. Power, Trans. ASME, 101 (3), pp 440-449 (June 1979) 10 figs, 1 table, 16 refs

Key Words: Turbines, Computer-aided techniques, Design techniques

The paper describes a comprehensive computer aided design procedure and its use to investigate mixed flow turbines for automotive turbocharger applications. The outside dimensions of rotor and casing as well as blade angles are determined from one-dimensional design and off design calculations, the detailed blade shape from quasi-three-dimensional analysis and mechanical stressing and vibration programs, and geometric data are presented as outside views and sections of the rotor by a graphics subroutine.

### 79-2264

### Low Frequency Gas Turbine Noise

J.R. Newman and K.I. McEwan British Gas, Hinckley, UK, ASME Paper No. 79-GT-196

Key Words: Gas turbine engines, Noise generation, Low frequencies

British Gas has experienced problems at some installations from low frequency turbine noise. The paper describes how the low frequency noise problems were investigated and then resolved by aerodynamic modifications and a silencer extension.

### 79-2265

### Instability Problem in a High Pressure Ammonia Syn-Gas Compressor

F.C. Aguilar

Instituto Mexicano del Petroleo, Mexico City, Mexico, Machinery Vibration Monitoring and Analysis

Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 63-71, 22 figs, 4 refs

Key Words: Compressors, Vibration response

This paper deals with the vibration problems experimented in a high pressure compressor installed in an ammonia plant of a large Pemex Petrochemical Complex located in the southeast part of Mexico. The various analytical studies, the field and laboratory analysis performed by the Instituto Mexicano del Petróleo IMP to pinpoint the cause of the problem, including a brief description of present rotor dynamics capabilities, are described. Some orbit shapes, acceleration and displacement frequency spectrums and other graphic results as unbalance response and Bode plots are illustrated. Finally, the corrective actions recommended by the compressor manufacturer and the current unit behavior are discussed.

### RAIL

79-2266

Urban Rail Noise Abatement Program: A Description L.G. Kurzweil and W.N. Cobb

Transportation Systems Center, Cambridge, MA, Rept. No. DOT-TSC-UMTA-79-23, UMTA-MA-06-0099-79-1, 26 pp (Mar 1979)
PB-295 545/8GA

Key Words: Rail transportation, Noise reduction

This report presents the background, current activities, and future plans for the Urban Rail Noise Abatement Program. This program, sponsored by the Office of Technology Development and Deployment of the Urban Mass Transportation Administration (UMTA) was initiated in 1972 and has been technically managed by the Transportation Systems Center. The problem of urban rail noise and vibration is described and the rationale for the UMTA funded program is given. The body of the report presents a definition of the program objectives, a discussion of the program organization, and a description of past, current, and future program activities. Major accomplishments of the program to data are listed in the final section.

79-2267

Dynamic Theories and Experiments of Alternative Guideway-Vehicle Systems. Part II J.F. Wilson

Dept. of Civil Engrg., Duke Univ., Durham, NC, Rept. No. DOT/RSPA/DPB/50-79/4, 189 pp (Mar 1979) PB-294 247/2GA

Key Words: Interaction: vehicle-guideway

In both the companion report (Part I) and the present study, the broad purpose is to investigate theoretically and experimentally guideway-vehicle system dynamics. Four alternative systems are studied in terms of nondimensional parameters.

### REACTORS

79-2268

Analysis of Containment Structures for Randomly Arriving Transient Loads

M.P. Singh and A. Al-Dabbagh

Dept. of Engrg. Science and Mechanics, Virginia Polytechnic Inst. and State Univ., Blacksburg, VA 24061, Engrg. Struc., 1 (4), pp 197-202 (July 1979) 7 figs, 4 refs

Key Words: Containment structures, Nuclear reactor containment, Hydrodynamic excitation

Hydrodynamic loads such as those due to safety relief valve discharges and a postulated accidental loss of coolant are some of the major loads on boiling water reactor (BWR) containments. The formulation of the response transfer function approach is developed for axisymmetric containment structures. The formulation to obtain the mean and standard deviation of response for uniformly distributed load arrival time is also provided and the numerical results for a typical BWR containment are given.

79-2269

A Comparison of Background Seismic Risks and the Incremental Seismic Risk Due to Nuclear Power Plants

Y.T. Lee, D. Okrent, and G. Apostolakis School of Engrg. and Applied Science, Univ. of California, Los Angeles, CA 90024, Nucl. Engr. Des., 53 (1), pp 141-154 (June 1979) 3 figs, 7 tables, 44 refs Key Words: Nuclear power plants, Seismic response

The seismic risk for the continental United States, in terms of the expected annual number of deaths and severe injuries, and the expected property damage, is evaluated in this work. Probabilistic models and correlations are developed and used in the evaluations of the risks, accounting for such important variables as the variability of property values, damage factors and so on. In addition, the incremental seismic risk due to the presence of nuclear power plants is evaluated utilizing results and methods available in the literature.

### RECIPROCATING MACHINE

(Also see Nos. 2173, 2174)

### 79-2270

### Engine Evaluation of a Vibration Damping Treatment for Inlet Guide Vanes

J.P. Henderson, L.C. Rogers, D.B. Paul, and M.L. Parin

Wright-Patterson AFB, OH, ASME Paper No. 79-GT-163

Key Words: Engine vibration, Vibration damping

This paper describes the results of engine test-cell tests and the comparison of these results with actual service experience obtained under operational conditions. Measured effects on engine performance, distortion tolerance, and anti-icing performance are presented along with measured stress reductions, as compared with increases in modal damping. Durability design considerations are discussed, along with the results of durability tests in an engine test stand and actual service experience.

### 70.9971

### Knock-Induced Cavity Resonances in Open Chamber Diesel Engines

R. Hickling, D.A. Feldmaier, and S.H. Sung Engrg. Mechanics Dept., General Motors Research Labs., Warren, MI 48090, J. Acoust. Soc. Amer., 65 (6), pp 1474-1479 (June 1979) 10 figs, 2 tables, 7 refs

Key Words: Diesel engines, Engine noise, Cavity resonators

Cavity resonances are investigated in detail for six openchamber diesel engines of different sizes. Spectral data are obtained from cylinder pressure-time traces and compared with predictions from finite-element calculations of the cavity resonances. Good agreement is found.

### ROAD

### 79-2272

### Nonlinear Rebound of a Rod After Impact Against a Deformable Barrier

H. Garnet and H. Armen

Research Dept., Grumman Aerospace Corp., Bethpage, NY, Intl. J. Numer. Methods Engr., 14 (7), pp 1037-1050 (1979) 8 figs, 10 refs

Key Words: Collision research (automotive), Guardrails, Ground vehicles, Mathematical models

The nonlinear impact of a vehicle against a deformable barrier and its subsequent rebound from that barrier are simulated. A one-dimensional elastoplastic model represents the vehicle as a series of rod finite elements and the barrier as a single mass, nonlinear spring. The solution procedure utilizes variable time step integration, contains an error control and eliminates numerical instabilities. A limited study assesses the influence of system parameters on both structure and occupants. The chief objective is to establish the feasibility of the proposed treatment of this class of problems.

### 79-2273

# Task 4 Test Report for Development of Compliance Test for Truck Rear Underride Protection

R. Baczynski and S. Davis

Dynamic Science, Inc., Phoenix, AZ, Rept. No. 8319-78-149A, DOT-HS-803 991, 261 pp (Sept 1978)

PB-294 785/1GA

Key Words: Trucks, Collision research (automotive), Experimental data

This report presents the results of the six passenger car-torear underride crash tests conducted in accordance with the requirements of Task 4 of the 'Development of Compliance Test for Truck Rear Underride Protection' program. The test vehicles selected for Task 4 tests were 1978 VW Rabbit and 1978 Chevrolet Impals four-door sedans.

### 79-2274

# Task 5 Report of Tests 5.1, 5.2, and 5.3 for Development of Compliance Test for Truck Rear Underride Protection

R. Baczynski, S. Davis, and R. Cropper Dynamic Science, Inc., Phoenix, AZ, Rept. No. 8319-78-193A, DOT-HS-803 990, 162 pp (Nov 1978) PB-294 831/3GA

Key Words: Collision research (automotive), Experimental data

This report presents the results of the first three of eight passenger car-to-rear underride crash tests conducted in accordance with the requirements of Task 5 of the 'Development of Compliance Test for Truck Rear Underride Protection' program. The test vehicles selected for these tests were 1978 VW Rabbits and a 1978 Ford Fiests. These vehicles were impacted into bolt-on, rigid, cantilevered guards mounted to a truck/trailer body simulator at selected heights above ground level.

### 79-2275

### Vibration Tests on Transit Buses

J. Anderson and H. Thomas
Gould Information Identification, Inc., Fort Worth,
TX, Rept. No. UMTA-MA-06-0041-79-6, DOT-TSCUMTA-79-13, 56 pp (Mar 1979)
PB-295 091/3GA

Key Words: Buses, Vibration measurement

The objective of this vibration measurement program is to quantify the vibration environment which is experienced by Automatic Vehicle Monitoring (AVM) equipment when installed on buses during typical city route service operations. Two buses are utilized in this measurement program; a General Motors Corporation Model 3100 provided by the Southern California Rapid Transit District, and a Flexible Corporation Model 207 provided by the City Transit of Fort Worth, Texas. The approach taken involved instrumenting the buses and representative electronic hardware on the buses with calibrated accelerometers and recording the output of these accelerometers while driving the buses over selected test routes at specified speeds.

### 79-2276

Improvement of Shock Measurements for Armored Vehicles - ILIR Task 4

W.S. Walton Aberdeen Proving Ground, MD, Rept. No. APG-MT-5192, 64 pp (Jan 1979)

Key Words: Shock tests, Shock measurement, Armored vehicles

A study was conducted at Aberdeen Proving Ground from April to September 1978. Data from piezoelectric and piezoresistive accelerometers subjected to short duration shocks were analyzed. Various configurations and materials were used to mechanically filter out high-frequency acceleration.

### 79-2277

AD-A066 303/9GA

# Optimal Control Concepts for the Characterization and Design of Highway Vehicle-Trailer Systems

M.A. Townsend, A.B. Shapiro, and K.T.A. Ho Dept. of Mech. Engrg. and Materials Science, Vanderbilt Univ., Nashville, TN, J. Dyn. Syst., Meas. and Control, Trans. ASME, 101 (2), pp 127-137 (June 1979) 11 figs, 41 refs

Key Words: Articulated vehicles, Dynamic stability, Optimum control theory

In this paper, design concepts are developed from optimal control theory to provide criteria for comparison and are then applied to one of the more innovative and potentially competitive concepts in commercial trucking: the multiple-trailer highway vehicle train. The definition of relevant models is given and criteria are then developed. Their applicability is demonstrated by the posing of optimal unloading schedules to improve dynamic performance, the sensitivity of such designs to changes in system parameters, and the design synthesis of couplers between the system components.

### ROTORS

(Also see Nos. 2154, 2161, 2164)

### 79-2278

### Calculation of Rotor Impedance for Articulated-Rotor Helicopters in Forward Flight

K. Kato and T. Yamane Univ. of Tokyo, Tokyo, Japan, J. Aircraft, 16 (7), pp 470-476 (July 1979) 8 figs, 5 refs Key Words: Helicopters, Mechanical impedance, Flexible rotors, Rotors (machine elements)

A procedure is presented to calculate the loads transferred from an articulated flexible rotor to the fuselage when the hub is forced to oscillate sinusoidally. Blade motions are determined from a set of linear algebraic equations derived from equations of motion with periodic coefficients. The aerodynamic loads are based on two-dimensional quasisteady strip theory.

79-2279

### Engine Rotor Dynamics, Synchronous and Nonsynchronous Whirl Control

R.A. Marmol

Government Products Div., Pratt and Whitney Aircraft Group, West Palm Beach, FL, Rept. No. FR-10632, USARTL-TR-79-2, 149 pp (Feb 1979) AD-A066 093/6GA

Key Words: Rotors (machine elements), Turbine components, Design techniques, Mathematical models, Experiments' results

A combined analytical and test program is performed to develop a method of designing highspeed power turbine rotors to minimize rotor-induced dynamic loads under normal operating conditions; minimize rotor tip-to-shroud clearance to maintain high flow-path efficiency; and minimize rotor deflections due to sudden abusive imbalance loads associated with blade loss. Using the results of the analytical models and experimental tests, a method of design optimization is developed to obtain the best trade-off between all the rotor design variables considered in this program.

SHIP

79-2280

## Response Analysis of a Moored Open-Bottom Floating Platform to Random Loadings

S.S. Fang

Ph.D. Thesis, Columbia Univ., 94 pp (1979) UM 7916402

Key Words: Off-shore structures, Random excitation, Time domain method, Harmonic excitation, Seismic excitation, Wind-induced excitation

The dynamic response of a moored open-bottom floating platform to random loading is examined by a time-domain simulation technique. The equations of motion of the floating platform in the time domain are derived from the impulse response method which takes into consideration the frequency dependence of the fluid reaction force terms, i.e., added mass and damping force coefficients. The sway and roll responses of the moored platform to random environmental loadings are evaluated by solving the equations of motion. The hydrodynamic coefficients of the open-bottom platform, with pressurized subdivided air chambers having a free air-water interface, are evaluated by a modified Frank's close fit method. Numerical examples of the motion response of the floating platform, to harmonic excitation, random wind loading and earthquake are illustrated and discussed in this study.

79-2281

### Spectral Dynamic Fatigue Analysis of the ANDOC Dunlin A Platform

D. Zijp

Volker Sterin Civil Engrg. and Construction, P.O. Box 3, 1940 AA Beverwijk, The Netherlands, Engrg. Struc., 1 (4), p 211 (July 1979) 15 figs, 2 refs

Key Words: Offshore structures, Fatigue life, Computer programs

The necessary computer programs have been developed by the IBM computer center in Zoetermeer and have been extensively tested by the ANDOC design team, using the Dunlin A geometry. A comparison is made between deterministic and a spectral analysis as well as between the harmonic solution and time step integration.

### SPACECRAFT

79-2282

### Flight Vibration Environments Defined From Mk 12 Booster Static Tests

N. Rubinstein and W.C. Caywood

Appl. Physics Lab., The Johns Hopkins Univ., Laurel, MD, J. Spacecraft Rockets, 16 (4), pp 214-217 (July/Aug 1979) 4 figs, 4 tables, 4 refs

Key Words: Booster rockets, Vibration tests

Results of a static firing test program concerning the environmental effects of rough burning of the Mk12 rocket motor booster on the Standard Missile components are discussed. Vibration and pressure data were recorded and processed using methods of time series analyses. The test procedures, methods of data processing, and significant results are presented. The results show good agreement with flight vibration data and theoretical acoustic pressure frequencies.

### STRUCTURAL

### 79-2283

Theoretical Study of the Dynamic Response of a Chimney to Earthquake and Wind

L. Shiau

Ph.D. Thesis, Purdue Univ., 168 pp (1978) UM 7914971

Key Words: Chimneys, Earthquake response, Wind-induced excitation

An analytical investigation of the response of a chimney to earthquake and wind is presented. The 823 foot tall chimney is modeled using Bernoulli-Euler beam finite elements. The modal superposition method is used for analyzing the elastic response while the numerical direct integration method is used to solve the equations for the inelastic response. A mathematical model that enables one to predict the vortex-excited resonant responses of two cylinders in line in the wind direction is developed.

### 79-2284

Earthquake-Induced Sloshing in Axisymmetric Tanks M. Aslam

Ph.D. Thesis, Univ. of California, 281 pp (1978) UM 7914532

Key Words: Tanks (containers), Fluid-filled containers, Sloshing, Dams, Off-shore structures, Seismic excitation

The present study was motivated by the concern about possible effects of seismic-sloshing in pressure-suppression pools of boiling water reactors. These suppression pools may be designed as annular or torus tanks. An analysis to predict the sloshing displacements and impulsive pressures in annular tanks, and a finite element technique applicable to all axisymmetric tanks with rigid walls and subjected to horizontal ground motions are presented.

#### 79-2285

Dynamic Structural Analysis with Substructures J.S. Arora and D.T. Nguyen

Div. of Materials Engrg., Univ. of Iowa, Iowa City, IA, Rept. No. TR-46, 34 pp (Dec 1978) AD-A065 937/5GA

Key Words: Dynamic structural analysis, Finite element technique, Natural frequencies, Mode shapes, Helicopters

A method for dynamic structural analysis with substructures and the subspace iteration is developed. The method uses only substructural stiffness matrices and the mass matrix for each finite element of the system.

### **TRANSMISSIONS**

### 79-2286

Keeping Hydrostatic Transmissions Quiet

S.J. Skaistis

Sperry-Vickers Div. of Sperry Rand Corp., Troy, MI, Diesel Gas Turbine Prog., 45 (8), pp 24-25 (Aug 1979) 7 figs

Key Words: Transmission systems, Noise reduction

Existing technology for the airborne, fluidborne, and structureborne noise abatement in hydrostatic transmissions is discussed.

### TURBOMACHINERY

(Also see Nos. 2171, 2172)

### 79-2287

Rotor Critical Speed and Response Studies for Equipment Selection

C. Jackson and M.E. Leader

Monsanto Co., Texas City, TX, Machinery Vibration Monitoring and Analysis Seminar and Mtg., Proc., Sponsored by Vibration Inst., Apr 1979, New Orleans, LA, pp 43-50, 17 figs

Key Words: Turbomachinery, Turbine components, Critical speeds, Unbalanced mass response

This paper addresses some of the latest techniques available for turbomachinery analysis.

# ANNUAL AUTHOR INDEX

A	Aizerman, M.A	Apetaur, M 1292
	Akai, T.J61	Apostolakis, G 2269
	Akhlaghi, M	Aprolan, P
	Akkas, N	Arafa, H 2089
Abaravicius, G.A 1405, 1413	Akky, M.R 1483	Arakawa, K
Abbagnaro, L.A 2186	Akolkar, P.M	Aravamudan, K.S
Abbas, B.A.H92	Alaniz, O 2259	Arden, R.W 2258
Abdel-Ghaffar, A.M 514, 1240,	Albrecht, H 1835	Argyris, J.H
1640	Albright, H.E	Ariaratnam, S.T 1931, 1997,
Abdelhamid, A.N 1074	Al-Dabbagh, A	2001
Abdelrahman, A.M.S.A 136, 1330	Alem, N.M 868, 869, 870,	Arii, M
Abdul-Wahed, M.N 2201	871	Ariman, T
Abedi-Hayati, S 271	Alexandridis, A.A	Armand, J.L 445
Abel, I 1843	Alfaro-Bou, E 151	Armen, H 2272
Abercrombie, G.E542	Alfrey, R.J 250	Armstrong, J.H 2042
Aboud, G.M 1272, 1273, 1274	Ali, M.R 1797	Arndt, R.E.A
Abraham, B	Ali, R	Arnold, J.M
Abramovich, H1206, 1829, 1830	Ali, S.M.J 695	Arora, H.L 976
Abrishaman, M	Allaire, P.E 700, 1566,	Arora, J.S 11, 1679, 2285
Achenbach, J.D 1160	1792, 1793	Arya, A.S 1506, 1509, 1647,
Acker, L.W 1069	Allen, R.R	1681, 1854
Ackermann, U 1331	Alli, P	Arya, J.C
Adamczyk, J.J 945, 1261	Almosnino, D 2067	Asavanich, S 1318
Adams, E 1892	Alwar, R.S	Ashford, R.A702
Adams, G.G	Ames, W.F 1892	Ashley, H 1156, 1442
Adams, R.D1779, 1818	Amiet, R.K 664	Aslam, M 1762, 2284
Adams, W.M., Jr922	A-Moneim, M.T 476, 925	Atanackovic, T.M
Adamson, T.C., Jr755, 1321	Anand, G.V 96, 286	Atassi, H
Adegoke-Anthony, C 2095	Anderes, J.R 1308	Athanasiou-Grivas, D 1618, 1672
Adler, A 1700	Anderheggen, E 909	Atkatsh, R 2040
Adler, M.A	Andersen, C.M 903	Atkočiūnas, J 1392, 1414, 1415
Agrawal, A.B	Anderson, G.L	Au, W
Agrawal, G.K	Anderson, J	Au, Y.H.J 1516
Agrawal, K.B 1524	Anderson, J.C 205	Audibert, J.M.E 1483
Agrawal, R.K	Anderson, J.G 572	Audoynaud, D 1502
Aguilar, F.C	Anderson, J.G 1504	Auerbach, E.I 1911
Ahmadi, G	Anderson, J.H.B 246	Auld, B.A
Ahmed, K.M 176	Anderson, J.M	Aumen, C.P
Ahmed, M.S	Anderson, J.S 1424	Aurora, P.R 1398
Ahmed, S	Anderson, T.L	Au-Yang, M.K 535, 1464
Ahuja, K.K	Anderson, W.J	Averbuch, A.J
Aida, H	Andersson, L.E 2016	Aydin, M 2140
Ailman, C.M	Andrews, R.S	Ayre, R.S
	Anglin, E.L 508	Aziz, T.S
Aizawa, K	Angrilli, F 1389	Azuma, A

В		Barney, B.G 2049	Benahm, R.A41
		Barney, C.B	Benedict, C.E875, 876
		Barney, G.B	Bennett, A.G 542
		Baron, M	Bennett, R.M
Baade, P.K		Baron, M. L 2040	Benson, J.B 868, 869, 870
Babson, P.E		Barr, A.D.S 1358	Benson, R.C 321
Babu, P.V.T		Barrett, L.E1095, 1792	Bently, D.E 1519
Bache, T.C		Barron, R.M 437	Benton, M.C 1107
Backasch, M		Barrows, J.F 1074	Bergamaschi, S
Baczynski, R		Barsch, H 1981	Bergamasco, G961
Badgley, R.H		Barschdorff, D 957	Berger, H 1983
Badlani, M 45		Bartenwerfer, M	Berglund, J.W 1211
BadriNath, Y.V		Barthel, K 2178	Bergmann, E 1643
Bagchi, J.K		Bartholic, K.R 68	Berman, A
Bagci, C		Bartlett, F.D., Jr	Berns, H 1965
Bagge, C.F	575	Barton, C.K	Bernussou, J 1705
Bahar, L.Y		Barton, J.R 288	Berry, G 1278
Baig, M.I		Barton, L.O	Bert, C.W 833, 1939, 1940
Bailey, C.M		Basak, A.K 1616	Bertero, V.V 1233, 1234,
Bailey, J.T		Basavanhally, N 131, 1868	1235, 1582
Baines, N.C		Basci, M.I	Beskos, D.E90
Bajaj, A.K		Basu, P.K 1391	Bessey, R.L
Bajons, P	1972	Basu, S 1509	Best, A 2083
Baker, C.J		Batchelor, B.DeV987	Bettess, P 440
Baker, R.N		Bates, L 1741	Bhandari, N.C 2038
Baker, W.E 44		Bätge, J 1869	Bhandari, R.K 1650
Balachandra, M.B		Bathe, K.J	Bhandwalkar, P.K 1655
Balakrishnan, R		Bathias, C 67	Bhaskara, R.K 2192
Balasubramanian, R		Battis, J.C 2080	Bhat, R.B 1229
Baldwin, R.M		Batts, M.E	Bhat, W.V
Balke, R.W		Bauer, A.B 343, 2065	Bhatia, K.G 1553, 1599
Balsara, J.P		Bauer, B.B 2186	Bhatti, M.A 2261
Balzer, L.A		Baumeister, K.J 1106, 1580	Bhave, M.V 1670
Bamer, F		Baumhoff, N 1973	Bhutiani, P.K
Bandyopadhyay, S.S		Bayer, A.R., Jr	Bianchi, V
Banerjee, D		Bayliss, A	Bicanic, N 1606
Banerjee, M.M		Bazzi, G 909	Bick, F.A 1942
Bannister, R.L 1072,		Bea, R.G1483, 1484	Bickel, H.J 1770
Banon, H		Beards, C.F 487	Bieniek, M.P 2040
Bansal, A.S 597, 791		Beason, W.L 1633	Bies, D.A 1345, 1396, 1428
Bapat, V.A	0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Beaufait, F.W 496	Biggs, J.M 518
Barach, D		Beazley, W.G 813	Bigler, W.B 1052
Barakat, R		Beck, C.J., Jr	Bigley, W.J 1375
Barber, J.P.		Beck, J.L	Billington, D.P 485
Barbosa, H.J.C		Beckemeyer, R.J 104	Bily, M 1291
Barclay, D.W		Becker, R.J	Birdsall, T.G
Bardowicks, H		Bediashvili, M.A 1860	Bishop, R.E.D
Baret, M		Beercheck, R.C 108	Biswas, J.K
Barker, T.G		Bellinger, E.D 1729	Bjorno, L 438
Barker, W.R		Bellomo, N 1495	Black, J.A 1485
Barnes, S.B	1232	Beltzer, A.I 1754	Blair, C.N

Blair, D.G 1170	Brady, G	Butterfield, M.H 1601
Blake, W.K 294	Bramberger, C 1256	Button, M
Bleich, H	Brander, O 103	Buxbaum, O
Blejwas, T.E 1078	Braun, S 955	Buyukozturk, O
Bloch, H.P	Brausch, J.F 347	Byrd, R.C
Blount, M.L	Bräutigam, H 2056	
Board, D	Bray, H.W 1538	
Bobichon, J.P 225	Breakwell, J.V 1442	C
Bodley, C.S	Bredehoft, M 1490	
Bodner, S.R 937, 1000, 2230	Breig, W.F	
Bogayevsky, V.N 1744	Bremhorst, J.H 2241	Cabak, G
Bogdanoff, J.L 480, 1991,	Bresler, B 1103	Cacko, J 1291
2008, 2020	Brinet, B	Cagliostro, D.J
Boghani, A.B	Brinkmann, K	Caldwell, S.R
Bogy, D.B 321	Broner, N 1254	Calistrat, M.M 1382
Bohm, G.J	Brouns, A.J 1227	Calkins, D.E 1279
Boillat, G 1489	Brown, F.W	Camacho, A.A 918
Boillot, D 601	Brown, J.M 467	Cameron, D 1622
Boisch, R 2047	Brown, N.A	Campbell, I
Bold, G.E.J 276	Brown, R 121	Campbell, R.L 1454
Boldman, D	Brown, S.D 894	Candel, S 569
Boldman, D.R 989	Brown, S.M	Cansdale, R
Bolton, A 916	Brown, T.J 667	Captain, K.M
Bonnecase, D 16	Bruce, R.N., Jr	Cardani, C
Book, W.J 1704	Brumaghm, S.H 1039	Carlson, P.O.L 2163
Booker, J.F 1567	Bryson, A.E., Jr 2212	Carlsson, G 1794
Boos, G 2116	Bschoor, O 1835	Carneiro, C.I 1812
Borg, M.F 964	Buch, A 150	Carney, J.F., III336, 1811, 2028
Borgwardt, P 652	Buchus, R.C 2096	Carpent, V 2144
Borisovna, M.J 1507	Buckens, F 1855	Carr, R.W 248, 1272, 1273, 1274
Bork, M 565	Bucker, H.P	Carrigan, B 1498
Bormann, V	Buckland, P.G 1641	Carson, J.M 269
Bosmans, R.F 1519	Buckley, B 2171	Carson, W.L1587, 1588
Bossler, R.B., Jr 1282	Budiansky, B 1894	Carta, F.O
Bouche, R.R	Bufler, H	Casciati, F
Bouchon, M	Bugeat, L	Cassanto, J.M
Bourgine, A	Buggele, A.E 989	Cassenti, B.N 401
Bouts, D 1166	Buhlert, KJ 2072	Castle, C.B
Bouwkamp, J.G 856	Bulanowski, E.A., Jr 584	Catchpole, A.P
Bowes, M.A 408, 1249, 1282	Bull, D.G 1424	Caughey, T.K
Bowman, B.M 868	Bulychev, N.S 1508	Cavagnaro, D.M
Bowns, D.E 195	Buono, D.F 182	Cawley, P 1779, 1818
Boxwell, D.A	Burdess, J.S 679, 1807	Cawthorn, J.M 159, 857, 1059
Boyce, J.W 242	Burgess, G 1949	Caywood, W.C
Boyd, D.E	Burke, M.E 157, 187	Cedolin, L
Boyden, R.P 846	Burns, A 1628	Celep, Z 786, 1020, 1987
Braaten, R.J 834	Burns, S.H	Cengiz Dokmeci, M 1755
Bracken, E.J 481	Burrows, C.R	Ceranoglu, A.N
Brackett, R 455	Burton, T.D	Cermak, G.W
Bradford, L.G 297	Butler, R.W 1625	Chai, K
Bradley, J.S 1929	Butler, T.G 743	Chakrabarti, S.K

Chamis, C.C	Cho, H.S 1458	Cook, L.M
Chan, H.C 2036	Cho, Y.C	Cooke, P.W 1115
Chanaud, R.C 231	Chokshi, N.C	Cooley, D.E
Chandler, R.F	Chon, C.T981, 2231	Cooper, J.D
Chandra, B 1509, 1647,	Chonan, S	Cooperrider, N.K 1080, 1081,
1854	Chopra, A.K 1934	1262
Chandrasekaran, A.R., 1496, 1540,	Chopra, I 1096, 1571,	Coppa, A.P 1799
1600, 1662	2106, 2112	Cops, A
Chang, C.H 615	Choros, J	Corley, J.E 686, 2174
Chang, C.T	Chou, C.C 711, 1102, 1898	Corley, W.G
Chang, J.D	Chou, R.C	Cornell, C.A 1932
Chang, N	Chou, Y.F	
		Corrall, D.R
Chang, R.Y 614	Chow, C	Cost, T.L 1401
Chang, P.Y 424, 498, 499	Choy, K.C	Cottin, N
Chang, Y.M 2018	Christ, A	Cottington, R.V
Chang, Y.W 476	Christiansen, H.N	Coulon, G 1497
Change, A.T 2152	Chu, F.H	Cox, C.R
Chapler, R.S 2135	Chu, K 1561	Cox, J.J 1081
Chapman, R.B 1153	Chu, K.K 329	Cozzarelli, F.A
Chapman, R.E 1115	Chu, M.L 431	Craggs, A 839
Chappell, D.P	Chung, T.J 414	Craik, R.J.M 2007
Char, C.V 1388	Chuprina, A.A 1862	Crandall, S.H 825, 2044
Chari, R.T	Chwang, A.T 1668	Crawford, C.C., Jr
Charman, J.C170, 1457	Chwieroth, F.S	Crawley, E.F 1402
Chatani, A	Cipra, R.J 1257	Crespo Da Silva, M.R.M 295,
Chatterjee, S.N307, 2225	Clapp, D.E 168	1549, 1783
Chavez, J 2171	Clark, J.C	Crews, S.T
Cheeseman, I.C 650	Clarke, R.J 197	Crighton, D.G 1607, 2019
Chen, C.C	Clement, G	Crill, W
Chen, E.P	Clements, R.M 1938	Crisp, J.N 1287
Chen, F.Y	Clevenson, S.A	Cromer, J.C
Chen, HT	Clough, R.W 1450	
		Crook, A
Chen, L.T	Coats, D.W	Cropper, R
Chen, S.J 1049	Cobb, W.N 2266	Crouse, J.E 1752
Chen, S.J.H	Cockerham, G 680	Crowe, C.T 158
Chen, S.S 114, 309, 1689	Cohen, H 1816, 2039	Crump, M.W 1467
Chen, T.L.C 833	Coladonato, R.J 739	Cudlin, R 886
Chen, W.W.H 1523	Colclough, A.R 1967, 1968	Culver, C.C 1115
Chen, Y.N	Cole, J.E., III 259, 1576	Culver, L.E 2159
Chen, Y.N		
	Cole, J.E., III 259, 1576	Culver, L.E 2159
Cheng, F.Y 571	Cole, J.E., III	Culver, L.E 2159 Cummings, A 808, 809,
Cheng, F.Y	Cole, J.E., III	Culver, L.E
Cheng, F.Y.       .571         Cheng, KM.       .1197, 1596         Cherry, J.T.       .42	Cole, J.E., III       .259, 1576         Coleman, P.L.       .42         Collings, A.G.       .1492         Collins, J.D.       .49	Culver, L.E
Cheng, F.Y.       .571         Cheng, KM.       .1197, 1596         Cherry, J.T.       .42         Cheung, M.S.       .1025	Cole, J.E., III       .259, 1576         Coleman, P.L.       .42         Collings, A.G.       .1492         Collins, J.D.       .49         Collins, J.F.       .1148	Culver, L.E.       2159         Cummings, A.       808, 809,         1426         Cumpsty, N.A.       395         Cunningham, H.J.       253         Cunningham, R.E.       2154
Cheng, F.Y.       .571         Cheng, KM.       .1197, 1596         Cherry, J.T.       .42         Cheung, M.S.       .1025         Cheung, Y.K.       .2048	Cole, J.E., III       .259, 1576         Coleman, P.L.       .42         Collings, A.G.       .1492         Collins, J.D.       .49         Collins, J.F.       .1148         Colpin, J.       .1076         Colson, H.J., Jr.       .1906	Culver, L.E
Cheng, F.Y.       571         Cheng, KM.       1197, 1596         Cherry, J.T.       42         Cheung, M.S.       1025         Cheung, Y.K.       2048         Chi, M.       636, 637         Chia, C.Y.       323	Cole, J.E., III       .259, 1576         Coleman, P.L.       .42         Collings, A.G.       .1492         Collins, J.D.       .49         Collins, J.F.       .1148         Colpin, J.       .1076         Colson, H.J., Jr.       .1906         Colton, D.       .1732	Culver, L.E
Cheng, F.Y.       571         Cheng, KM.       1197, 1596         Cherry, J.T.       42         Cheung, M.S.       1025         Cheung, Y.K.       2048         Chi, M.       636, 637         Chia, C.Y.       323         Chipman, R.R.       511	Cole, J.E., III       259, 1576         Coleman, P.L.       42         Collings, A.G.       1492         Collins, J.D.       49         Collins, J.F.       1148         Colpin, J.       1076         Colson, H.J., Jr.       1906         Colton, D.       1732         Colton, J.D.       45, 582	Culver, L.E.       2159         Cummings, A.       808, 809, 1426         Cumpsty, N.A.       395         Cunningham, H.J.       253         Cunningham, R.E.       2154         Curry, W.H.       844, 1631         Curtis, C.M.       121         Cutchins, M.A.       1635
Cheng, F.Y.       571         Cheng, KM.       1197, 1596         Cherry, J.T.       42         Cheung, M.S.       1025         Cheung, Y.K.       2048         Chi, M.       636, 637         Chia, C.Y.       323         Chipman, R.R.       511         Chishaki, T.       837	Cole, J.E., III       259, 1576         Coleman, P.L.       42         Collings, A.G.       1492         Collins, J.D.       49         Collins, J.F.       1148         Colpin, J.       1076         Colson, H.J., Jr.       1906         Colton, D.       1732         Colton, J.D.       45, 582         Colwill, W.H.       1074	Culver, L.E.       2159         Cummings, A.       808, 809, 1426         Cumpsty, N.A.       395         Cunningham, H.J.       253         Cunningham, R.E.       2154         Curry, W.H.       844, 1631         Curtis, C.M.       121         Cutchins, M.A.       1635         Czajkowski, R.L.       592
Cheng, F.Y.       571         Cheng, KM.       1197, 1596         Cherry, J.T.       42         Cheung, M.S.       1025         Cheung, Y.K.       2048         Chi, M.       636, 637         Chia, C.Y.       323         Chipman, R.R.       511         Chishaki, T.       837         Chitharanjan, N.       1646	Cole, J.E., III       259, 1576         Coleman, P.L.       42         Collings, A.G.       1492         Collins, J.D.       49         Collins, J.F.       1148         Colpin, J.       1076         Colson, H.J., Jr.       1906         Colton, D.       1732         Colton, J.D.       45, 582         Colwill, W.H.       1074         Comninou, M.       764	Culver, L.E.       2159         Cummings, A.       808, 809, 1426         Cumpsty, N.A.       395         Cunningham, H.J.       253         Cunningham, R.E.       2154         Curry, W.H.       844, 1631         Curtis, C.M.       121         Cutchins, M.A.       1635         Czajkowski, R.L.       592         Czarnecki, S.       22
Cheng, F.Y.       571         Cheng, KM.       1197, 1596         Cherry, J.T.       42         Cheung, M.S.       1025         Cheung, Y.K.       2048         Chi, M.       636, 637         Chia, C.Y.       323         Chipman, R.R.       511         Chishaki, T.       837	Cole, J.E., III       259, 1576         Coleman, P.L.       42         Collings, A.G.       1492         Collins, J.D.       49         Collins, J.F.       1148         Colpin, J.       1076         Colson, H.J., Jr.       1906         Colton, D.       1732         Colton, J.D.       45, 582         Colwill, W.H.       1074	Culver, L.E.       2159         Cummings, A.       808, 809, 1426         Cumpsty, N.A.       395         Cunningham, H.J.       253         Cunningham, R.E.       2154         Curry, W.H.       844, 1631         Curtis, C.M.       121         Cutchins, M.A.       1635         Czajkowski, R.L.       592

D	de Oliveira, J.G 1814, 1986	Doyle, G.R 431
	Derecho, A.T 139, 241,	Doyle, L.B
	1028, 1216	Drago, R.J 19, 194, 958, 2217
	DeRuntz, J.A441, 1127	Dragonette, L.R 1128
	Desai, A.R	Drechsler, J698, 1951
Dabell, B.J 1945	Deschamps, G.A	Drnevich, V.P
Dadone, L	Desmarais, R.N 229	Droms, C.R900
Dahlberg, T 1440	Destuynder, R 2064	Dubowsky, S 1683
Dale, B 1727, 1728	Devers, A.D	Duck, P.W
Dalzell, J.F 185	DeVilliers, A.L	Duff, C.G
Dambra, F	DeWitt, R.L888	534, 538
Damongeot, A 425, 930, 1244	Dhaliwal, R.S	Dufrane, K.D
Dancer, A 867	Dhar, C.L 1041	Dugdale, D.S 2027
Dancy, E	Dhotarad, M.S	Dugundji, J 1571
Daniele, C.J 1708	Dib, G.M	Duke, J.C., Jr
Daniels, E.F	Dickinson, S.M828, 1929	Duncan, P.E 546, 2118
Daniere, P	Diekhans, G	Dundurs, J 764
Dannan, R.E 520	Dieudonne, J.E 220	Dungar, R 444
Darden, C.M 1429	Diez, L	Dunnill, W.A 1741
Dareing, D.W	Dijksman, J.F 1214	DuParquet, J 1370
Darlow, M.S 278, 365,	Dikmen, M 2041	Dupas, J 1468
2154, 2164	Dilipkumar, D.D	Durelli, A.J 1348
Da Silva, M.R.M.C 992	Dillon, D.B	Durkin, J.M
Dathe, I 1741	DiMaggio, F.L 204, 493, 1827	Dutt, D.N
Datner, B 955	DiMarco, R.J 1848	Dutta, T.K 1856
Datta, S.K	Dimasi, F 1083	DuVal, R.W
Davidson, L.C	Dinkeloo, C.J	Dvorak, R.A 109
Davies, H.G 1419	Dittmar, J.H 1637	Dyka, C.T 1810, 1811, 2028
Davis, R.E	Dixon, K.O 276	Dym, C.L 625
Davis, S	Dizon, J.O	Dzgadlo, Z 155
Davis, S.S 1969	Djuric, S.V 1536	
Dawe, D.J 91, 126	Dobberschütz, J 1806	
Dawson, M.J 1501	Dobbs, N 1029	E
Day, S.M	Dodds, C.J 1970	
De, S	Dodlbacher, G 178	
Dean, J	Doelling, N 898	Eastep, F.E 397
Dean, P.D	Doige, A.G 1346, 1347	Eaton, R.A
Dear, T.A	Dokainish, M.A 805	Eckhardt, H.D 1134
DeFelice, J.J	Dokumaci, E 200	Edighoffer, H.H 1696
DeHoff, R.L	Dominguez, J 1045, 1047	Edwards, B.D 1245, 1865
Deksnis, E.B 533	Domis, M.A	Edwards, J.W
Delery, J	Dong, R.G	Edwards, R.M 648
DeLoach, R 159, 857, 1059	Dong, S.B 297	Egupov, K.V 1649
Delph, T.J	Dosanjh, D.S 345	Ehlbeck, J.M 219
Dempsey, K.M 1237	Douglas, B.E 87, 787	Ehle, P.E
Dempsey, T.K 1059, 1061	Dousis, D.A	Ehrlich, S.L
DeMuth, R.S 1950, 2165, 2166	Dow, A.L 212	Eidemiller, R.I949
Dendrou, B.A 1295	Dowell, E.H 462, 882, 1439	Eidinger, J.M 163
Denkhaus, H.G	Dowling, P.J 623	Eierman, R.G 1371
Denman, H.H	Downs, B 789	Einaudi, G549
Dennis, B.G., Jr 637	Downs, B.D	Einstein, H.H

Eisenmann, R.C 2191	Fagerland, H 265	Fisher, B.D 403
Eisinger, K 1135, 1136	Faltinsen, O.M63	Fisher, D.G 2213
Elder, F.C	Fandrich, R.T	Fitzpatrick, G.L 1739
Elder, S.A	Fang, S.S 2280	Flannelly, W.G 2081
Eldred, K.M	Fantino, B	Fleeter, S 1520, 1699
Elements, E.W 677	Fanuele, F	Fleming, D.P 278, 2165,
ElHakeem, H.A 2159	Farassat, F 667	2239
Elishakoff, I 1109, 1609, 2044	Faravelli, L 1293	Flink, J
Ellingwood, B.R 1115	Farmer, M.G 845	Florence, A.L 436
Elliott, G.L	Farr, M.K	Floyd, J.K
Elliott, J.L 1589	Farrell, P.A 154, 385, 642	Flüh, H
Ellis, R.W 1324	Fashbaugh, R.H 2135	Flynn, L
Elmadany, M.M 805	Fattal, S.G 1115	Foersching, H 1632
Elmallawany, A 640	Favier, D	Fontana, T
Elms, D.G	Fawcett, J.N 796	Foo, O 2036
Elsabee, F	Fawzy, I	Foss, R.N
El Sharkawy, A.I 612	Federn, K 1961, 1962	Foster, E.P 496
Elwany, M.H.S	Feiler, C.E	Fotieva, N.N
Ely, R.A 1227	Feldmaier, D.A	Fowler, G.F953
Emery, A.F	Feldmann, J 2072	Fowler, J.R 191
Emmerling, F.A 1782	Felippa, C.A 203, 207, 441,	Fox, C.H.J 679, 1807
Emori, K	1127, 1697	Fox, R.L
Engel, P.A 1994, 2200	Felsen, L.B 1377	Frazier, G.A
Engelbrecht, J	Felt, L.R	Frene, J
Enger, P.F	Feng, WH 603	Freskakis, G.N
Enserink, E 1880	Ferritto, J.M	Freymann, R
Epstein, A.H 1476	Fick, H	Frieze, P.A 623
Epstein, H.I	Fickes, J.D	Frisch, H.P
Erdman, A.G1001, 1002, 1005	Fields, S.R	Fritz, J.T.D
Ericsson, L.E 2069, 2070	Fiessler, B	Frohrib, D.A 1001, 1002,
Erkelens, L.J.J 1624	Filho, F.V	1005
Ertepinar, A	Fillod, R	Fronczak, F.J 797
Escudie, B		
Escudier, M.P	Finch, R.D 688 Findeisen, D 1961, 1962	Frost, W.G
Eshleman, R		Fruedenthal, A.M 1280
	Finger, R.A	Fuchs, G.L
Esmailzadeh, E 144, 162, 1677	Fink, M.R	Fugelso, L.E 1216
Espana, M	Finkelstein, G	Fujimori, Y 1997, 2001
Etsion, I	Finley, R.W	Fujimoto, S
Ettles, C.M.M	Finley, T.D	Fujimuru, M 687
Evensen, D.A	Finneran, T.J	Fujiwara, K
Eversman, W 1379	Finogenov, V.A 305	Fuks, Y.P 305
Everstine, G.C 1819	Fintel, M	Fukuda, M 289, 504, 505
Ewing, D.K 1974	1028, 1216	Fuller, C.R 1428
Ezekoye, L.I 281	Fiorato, A.E 138, 497, 517,	Funabashi, H
Ezzat, H.A 1564	1027, 2049	Funahashi, K 34, 64
	Fiorito, R 1822	Funakawa, M 1796, 1889
	Firth, D 635	Fung, KY 1444
F	Firth, I.M 550	Fung, R.C 1594
	Fischer, J 249	Fung, YC 1202
	Fischer, R	Fung, YT 1759
Fabri, J	Fish, R.B	Funk, J.G 1433

G CANADA	Ghosh, S.K 139, 241,	Green, G.C 672
	1028	Green, J.L
	Gianetti, C.E	Green, R.E., Jr
	Giannopoulos, F	Green, W.A
	Giencke, E	Greenberg, J.B 824
Gabel, R 1055	Giers, A 1909	Greenblatt, J.E
Gabrielsen, B.L 333	Gikadi, T 879	Greenfield, L.P 1878
Gabuzov, R.K 1860	Gilbert, L.J	Greenway, M.E 767
Gaffke, H 178	Gilles, E.D	Greiner, H.F 1094
Gajewski, R.R 928	Gilmore, D.R., Jr 1958	Grewatsch, R
Galaitsis, A.G 1462	Ginsberg, J.H 626, 770,	Griffin, O.M
Galbraith, T.J 1629	771, 1212, 1805, 2132	Griffiths, M.J
Gallagher, R	Girgis, R.S	Grittner, H
Gallagher, R.H 1825	Glattfelder, A.H	Groeneweg, J.F 1687
Galloway, W.J 1051	Glazik, J.L., Jr	Groger, K
Gambhir, M.L	Glienicke, J 2108, 2114	Grosche, FR
Ganapathy, S 1455	Glotzbach, R.W 1091	Grossi, R.O 128, 1409,
Ganesan, N 287, 628, 1408	Glynn, C.C 1549, 1783	1812, 2033
Garcia-Gardea, E	Gnoyke, R.E	Grosveld, F
Garniner, R.A	Gobetti, A	Grover, L.K
Garnet, H	Godden, W.G1230, 1762	Gruenwald, A 1289
Garrard, W.L	Goel, D.K	Gudehus, H
Gasch, R	Goethert, B.H	Guicking, D
Gasparini, D.A	Goldstein, M.E945	Guins, S
Gatchel, S.G	Golis, M.J	Gulbinas, A
Gatski, T.B 1928	Gomes de Oliveira, J	Gummlich, H
Gaudriot, L	Gomez-Masso, A.J 256	Gunter, E.J 700, 1095,
Gaukroger, D.R 1692	Gonzalez, J.J 1046	1793, 2162
Gaul, L	Goodling, E.C., Jr	Gupchup, V.N 1858
Gaunaurd, G	Goodno, B.J 1871	Gupta, A.K 478
Gauss, F 1277	Goodwin, R	Gupta, B.P 666
Gautesen, A.K 1518	Gopal, R	Gupta, K.K
Gazetas, G	Gorman, D.G	Gupta, L.K 1540
Gebman, J.R 509	Gorman, D.J 129	Gupta, M.K 1527, 1534,
Geers, T.L	Gossmann, E 556	1662
Geissler, W 653	Gottlieb, J.J 2136	Gupta, P.K 2204, 2205,
Gellert, M 400	Goudreau, G.L	2206, 2207
George, J 940, 1207, 1612	Gould, P.L 1015, 1391	Gupta, R
George, J.A 451	Gowan, E., III 760	Gupta, R.B 604
Gerasch, WJ	Goyal, M.R 890	Gupta, R.K
Gerber, N 491	Grabowski, B	Gupta, S.P
Gergely, P	Gracey, B 1167	Gupta, U.S 826, 2029
Geromel, J.C 1705	Grafov, C.C 1861	Gupta, V.K 280
Gersbach, V	Graham, T.S 1820	Gupta, Y.P 1616
Gerwig, W 2058	Gran, C.S 123, 2235	Guruswamy, P 1397
Geschwindner, L.F., Jr 1562	Gran, J.K	Guthrie, K.M
Geyser, L.C	Grant, H.P	Gutierrez, M 1162
Ghai, R.C 1791	Grant, S.J 796	Gutierrez, R.H616
Gharib, M	Graves, R.D 218	Guyton, R.W 469
Ghosh, M.K	Green, A.T 456	Gwinn, J.M 377

HT INCOME.	Harris, J.D	Hermanns, E 1981
	Harris, J.G	Heron, R.A 1777
	Harris, W.J	Herr, R.W
	Harris, W.L	Herrmann, G
	Harrison, I.R 401	Hershkowitz, H 264, 1150, 2182
Haasz, A.A	Hart, G.C 1451	Herting, D.N
Habeck, R	Harting, D.R	Hertzog, H
Haber, C.P	Hartman, W.F	Heveron, G.D
Habercom, G.E., Jr 13, 404, 409,	Hartmann, B 2138	Hibbert, J.H
410, 411, 412, 721, 722, 1717,	Hartmann, M.J	Hibner, D.H
1718, 1913, 1914, 1915, 1916	Hartung, C 630	Hickey, J.V
Hablani, H.B	Hasegawa, T	Hickling, R
Hacklinger, M 198	Hasenpusch, B	Hicks, J.E 1674
Haddow, J.B	Hashirizaki, S	Hidaka, T
Hafer, X	Hassan, H	Higashi, T 1570
Hagedorn, P	Hasse, T 1935	Higgins, P.B
Hagler, R	Hassel, R.L	Highter, W.H
Hahn, E.J 1478	Hatcher, D.S	Hilding, R.K
Hahn, W.F	Haug, E.J., Jr	Hill, A 1276
Haibach, E 1902	Hauger, W 1490	Hill, J.A
Haidl, G 1971	Haupt, W 2079	Hillberry, B.M 655
Hain, H.L	Havas, I 1757	Hillquist, R.K 1713
Haines, K.A	Hawker, K.E 1133, 1306	Hilton, D.A
Haisler, W.E 1500	Hawkings, D.L 665	Himmler, G 1420
Hale, A.L	Hayden, R.E 669	Hinchey, M.J 106
Hale, F.J	Hayes, D.J 1482	Hinckley, R.H 737
Haley, J.L	Hayes, M	Hinton, E
Hall, A.D 2257	Haynes, H.H 575	Hirano, Y 1209, 2031
Hall, D.D 1886	Hays, W.W	Hiromitsu, S 239
Hall, R.G., III 182	Hazell, C.R 1407	Hirsch, R 1497
Hall, W.E., Jr	Healey, A.J 1090, 1092, 1093	Hirt, C.W 703
Hall, W.J	Healey, T.J 1850	Hirt, M
Hallauer, W.L., Jr 79, 735, 1176	Healy, S.P 893	Hirtz, H 564
Halsted, D.M., III 1220	Heck, P.H	Hitch, H 1842
Ham, E.H 540	Heckel, H 2110	Hixson, E.L
Hamdi, M.A	Hedrich, J.K 1079	Ho, D.V 2042
Hamilton, J.F 2	Hedrick, J.K 1081, 1082	Ho, K.T.A
Hampton, J.R	Hegemier, G.A1187, 1746, 1747	Ho, M.T
Han, E	Hegner, H.R	Hoa, S.V
Hanaoka, M 1560	Heidelberg, L.J	Hoad, D.R
Haney, R.S 1587, 1588	Heidmann, M.F 1577	Hobaica, E.C 2133
Hannoyer, M.J 88, 1184, 1185	Hein, L.A	Hodges, D.H 1475
Hanschmann, D 1973	Heinen, R 1966	Hodgetts, D
Hansen, C.H	Helleur, C 1826	Hodulak, L 1925
Hanson, D.B 1372	Hellion, A 1502	Hoeppner, D.W 2158
Hanson, H.W 1865	Henderson, H.R 1052	Hoffman, E.P
Harari, A	Henderson, J.P56, 2270	Hoffmann, P.P 1957
Harder, R.L	Hengel, M.F	Hohenemser, K.H 1111, 2113
Hardin, J.C	Hennlich, HH	Hojo, A 1175
Harper, R.E	Henseleit, O	Holden, M.S 2121
Harrington, J.T 69, 451	Hensle, W 957	Holger, D.K

Holland, E	Hui, W.H	lyengar, K.T.S.R 320
Holland, J 2017	Hulusi, T.H 450	lyengar, N.G.R 1844
Holliday, B.G159, 857	Humes, B 606	lyengar, R.N 1988
Holmer, C.I	Hundal, M.S 1943	Izmailov, Y.V 1861
Holmes, H.K	Hung, Y.Y	Izumi, H 504
Holmes, P.J	Hunt, J.T 970	
Holmes, R	Huntley, B.L 1341	
Holstein, G.L	Huser, L 2116	ther J in teles
Holt, J.S 1905	Huss, M.F 2098	of sur
Holtzman, Z 1800	Hutchinson, J.R 1208	
Holzer, S.M 1121	Hutter, K 2223	Jacazio, G
Homyak, L 1621	Hutton, S.G	Jackson, C 527, 2170, 2287
Hontschik, H	Huttsell, L.J 2244, 2245	Jackson, E 1006, 1007, 1008,
Hoobler, G 2054	Hwang, C	1009, 1010
Hoogterp, F.B 1724	Hyer, M.W	Jackson, J.L
Hooley, R		Jacobs, W.R
Hope, P.S 1905		Jacoby, G 1973
Horgan, C.O 758	(1885). I (1885).	Jacquot, R.G 643
Horie, M		Jaeger, L.G 1493
Horikawa, H		Jagadish, K.S 1977
Horner, E.F	Ibidapo-Obe, O 2125	Jager, E.H 1613
Horner, J.E 1610	Ibrahim, R.A	Jain, A.K
Hosford, S	Ibrahim, S.R 78, 113, 273	Jakub, M
Hoshiya, S	Iding, R.H	Jandrasits, W.G 1003, 1004
Houghton, J.D 2172	leong, L	Jarchow, F 2014
Houstis, E.N 1295	Igaki, H	Jayaraman, G
Hovanesian, J.D 1348	Iguchi, M 1349	Jayasekaran, T 1559
Howard, G.F	li, J.M	Jeary, A.P
Howe, M.S 724, 1427, 1760	Ikui, T 2022	Jefferson, R.M
Howell, J.F	Imbert, J	Jeffrey, A
Howells, R.W 19, 194, 1283	Imbsen, R.A	Jeffrey, P
Howson, W.P 101	Imam, I.M.A 487	Jehlicka, P
Hoy, J.M	Ingard, U	Jendrzejczyk, J.A
Hruda, R.F	Inoue, T	Jennings, S.J 1072
Hsiao, M.H	Iqbal, M 139, 241, 1028 Irie, T 821, 823, 1018,	Jensen, A.P
Hsu, T	1022, 1552	Jensen, U
Hsu, TK 689	Irvine, H.M 1237	Jeyapalan, R.K
Hu, A.S	Irwin, A.W 1099	Jha, S.K
Huang, CC	Isenberg, J	Jines, R.H 1264
Huang, C.C	Ishida, Y	Johannesen, N.H
Huang, C.L 1398	Ishihara, K 1796, 1889	Johansson, I
Huang, H 1205, 1614	Ishihara, T	Johns, D.J
Huang, S 1451	Ishikawa, H	Johns, M.D
Huang, T	Ishioka, K	Johnson, A.W 1232
Huber, R	Itao, K 825	Johnson, E.R
Hubin, J 2144	Itou, S	Johnson, E.S 1228
Huckvale, S.A 195	Ivanov, P.L 1544	Johnson, G.R 1947
Huffington, N.J., Jr 193	Iwan, W.D 685, 1701,	Johnson, J.C 208, 1252
Hugg, S.B 1031	1750, 1751	Johnson, J.E 1031
Hughes, W.J	Iwatsubo, T 64, 697, 1118	Johnson, M.R 1263

Johnson, T.L201, 1893	Kaplan, K	Khanna, S.K 1690
Johnson, W 1057, 2106	Kar, A.K	Khazanchi, A.C 1856
Johnston, G.W 865, 1845	Kar, R.C	Khera, R.P 1526
Jonczyk, J	Kareem, A	Khmelevskaja-Plotnikova, G 2144
Jones, A.J 1278	Karkauskas, R 1392	Khot, N.S
Jones, D 276	Karmakar, B.M	Khozeimeh, K 979
Jones, D.I.G 55, 56, 99, 1715	Karnopp, D.C 180, 1225,	Kido, K 505
Jones, G.J 2202	1684, 1709	Kiger, S.A 245
Jones, H.W 1401	Karvelis, A.V	Kikuchi, K 1354
Jones, N 217, 416, 980,	Katayama, K 687	Kilimnik, L.S
1814, 1986	Katayama, T 1505	Killian, J.W 1819
Jones, P.J	Katholi, C.R	Kilmer, R.D
Jones, R 1064	Kato, K 1056, 2278	Kim, J.H
Jones, R.S	Kato, M	Kineke, J.H., Jr 578
Jones, S.W	Katsikadelis, J.T	King, W.F., III 530
Jordan, H.J 1958	Kaul, M.K	Kingsbury, H.B 931
Joseph, M.G 1651, 1857,	Kaul, R.K	Kino, G.S 1351
1863, 1864	Kausel, E	Kishioka, E
Joyner, R.G	Kavolėlis, A.P 1355, 1356,	Kiso, M
Juneja, B.L 2038	1421, 1479	Kitamura, Y 1663
Juran, D	Kawachi, K	Kitchens, C.W., Jr
Julian, D	Kawahara, T 1488	Kiusalaas, J
	Kawai, R	Klahs, J.W., Jr
Management of the second of th	Kawano, K	Klein, R.E
K	Kawashima, K 1231	Kleinhenz, W 458, 459, 982
	Vanting DN 1707	Viamont II D 1024
K BU 517 2247	Keating, P.N 1737	Klement, HD 1924
Kaar, P.H	Kelkel, K 1952	Klenner, J 1764
Kacena, W.J	Kelkel, K.       1952         Kellenberger, W.       457	Klenner, J
Kacena, W.J	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734
Kacena, W.J	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823,	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185         Kelly, S.G.       627	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219         Knop, WD.       2060
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185         Kelly, S.G.       627         Keltie, R.F.       1218	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219         Knop, WD.       2060         Knothe, K.       561
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185         Kelly, S.G.       627         Keltie, R.F.       1218         Kemmerling, P.T., Jr.       1542	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219         Knop, WD.       2060         Knothe, K.       561         Knott, P.R.       347
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185         Kelly, S.G.       627         Keltie, R.F.       1218         Kemmerling, P.T., Jr.       1542         Kempner, L.       608	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219         Knop, WD.       2060         Knothe, K.       561         Knott, P.R.       347         Ko, P.L.       1808
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185         Kelly, S.G.       627         Keltie, R.F.       1218         Kemmerling, P.T., Jr.       1542         Kempner, L.       608         Kenna, J.       1006, 1007, 1008,	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219         Knop, WD.       2060         Knothe, K.       561         Knott, P.R.       347         Ko, P.L.       1808         Kobayakawa, M.       1638
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38	Kelkel, K.       1952         Kellenberger, W.       457         Keller, A.C.       1307         Keller, C.L.       733         Keller, J.J.       26, 999         Kelly, J.M.       163, 645, 1823, 2013, 2150, 2185         Kelly, S.G.       627         Keltie, R.F.       1218         Kemmerling, P.T., Jr.       1542         Kempner, L.       608         Kenna, J.       1006, 1007, 1008, 1009, 1010	Klenner, J.       1764         Klippel, P.       135         Klosner, J.M.       734         Klud-um, W.       1381         Knight, W.A.       681         Knobloch, W.       2077         Knoell, A.C.       1219         Knop, WD.       2060         Knotthe, K.       561         Knott, P.R.       347         Ko, P.L.       1808         Kobayakawa, M.       1638         Kobayashi, A.S.       222, 913, 1925
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, H. 1687
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, H. 1687 Kobayashi, S. 1354
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, H. 1687 Kobayashi, S. 1354 Koebler, H.G. 1756
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, H. 1687 Kobayashi, S. 1354 Koebler, H.G. 1756 Koenigsberg, D. 756
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211 Kerber, G. 2142	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, S. 1354 Koebler, H.G. 1756 Koerber, E. 394
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kanatani, K.       1194	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211 Kerber, G. 2142 Kerr, A.D. 1876	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, B. 1354 Koebler, H.G. 1756 Koenigsberg, D. 756 Koerber, E. 394 Kohli, V.K. 1222
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kanatani, K.       1194         Kanber, H.       1284	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211 Kerber, G. 2142 Kerr, A.D. 1876 Kerrebrock, J.L. 1476	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, H. 1687 Kobayashi, S. 1354 Koebler, H.G. 1756 Koerber, E. 394 Kohli, V.K. 1222 Kolkman, P.A. 387, 1883
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kanatani, K.       1194         Kanber, H.       1284         Kandil, O.A.       470	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 2111 Kerber, G. 2142 Kerr, A.D. 1876 Kerstens, J. 125	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, A.S. 222, 913, 1925 Kobayashi, B. 1354 Koebler, H.G. 1756 Koerigsberg, D. 756 Koerber, E. 394 Kohli, V.K. 1222 Kolkman, P.A. 387, 1883 Kolodziej, R.M. 83
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kantani, K.       1194         Kanber, H.       1284         Kandil, O.A.       470         Kannel, J.W.       1795	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211 Kerber, G. 2142 Kerr, A.D. 1876 Kerstens, J. 125 Kessler, L.W. 959, 1352	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakhi, A.S. 222, 913, 1925 Kobayashi, A.S. 222, 913, 1925 Kobayashi, S. 1354 Koebler, H.G. 1756 Koerigsberg, D. 756 Koerber, E. 394 Kohli, V.K. 1222 Kolkman, P.A. 387, 1883 Kolodziej, R.M. 83 Komatsu, K. 1828
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kanatani, K.       1194         Kanber, H.       1284         Kandil, O.A.       470	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 2111 Kerber, G. 2142 Kerr, A.D. 1876 Kerstens, J. 125	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayashi, A.S. 222, 913, 1925 Kobayashi, A.S. 222, 913, 1925 Kobayashi, B. 1354 Koebler, H.G. 1756 Koerigsberg, D. 756 Koerber, E. 394 Kohli, V.K. 1222 Kolkman, P.A. 387, 1883 Kolodziej, R.M. 83
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kanatani, K.       1194         Kanber, H.       1284         Kandil, O.A.       470         Kannel, J.W.       1795         Kantola, R.A.       1259, 1930	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211 Kerber, G. 2142 Kerr, A.D. 1876 Kerrebrock, J.L. 1476 Kerstens, J. 125 Kessler, L.W. 959, 1352 Kettlekamp, D.B. 655 Khalil, T.B. 1447	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayakhi, A.S. 222, 913, 1925 Kobayashi, A.S. 222, 913, 1925 Kobayashi, S. 1354 Koebler, H.G. 1756 Koenigsberg, D. 756 Koerber, E. 394 Kohli, V.K. 1222 Kolkman, P.A. 387, 1883 Kolodziej, R.M. 83 Komatsu, K. 1828 Koncsek, J.L. 371 Kondo, H. 122, 946
Kacena, W.J.       190         Kachadourian, G.       1308         Kaestle, H.J.       565         Kaftka, P.G.       268         Kagawa, T.       1336         Kaiser, J.E.       611, 1723         Kaiser, W.D.       883         Kajita, T.       1399         Kalanta, S.       1392, 1414         Kalaycioglu, S.       1590, 2127         Kalinowski, A.J.       740, 1122, 1301         Kaliski, S.       38         Kamash, K.M.A.       694         Kamat, M.P.       794         Kamenskiy, Y.N.       1058         Kamperman, G.W.       1239         Kana, D.D.       454         Kanatani, K.       1194         Kanber, H.       1284         Kandil, O.A.       470         Kannel, J.W.       1795         Kanning, J.L.       2196	Kelkel, K. 1952 Kellenberger, W. 457 Keller, A.C. 1307 Keller, C.L. 733 Keller, J.J. 26, 999 Kelly, J.M. 163, 645, 1823, 2013, 2150, 2185 Kelly, S.G. 627 Keltie, R.F. 1218 Kemmerling, P.T., Jr. 1542 Kempner, L. 608 Kenna, J. 1006, 1007, 1008, 1009, 1010 Kennedy, R.P. 1592 Kennedy, T.E. 40 Kennedy, W. 1386 Kenton, E. 211 Kerber, G. 2142 Kerr, A.D. 1876 Kerstens, J. 125 Kessler, L.W. 959, 1352 Kettlekamp, D.B. 655	Klenner, J. 1764 Klippel, P. 135 Klosner, J.M. 734 Klud-um, W. 1381 Knight, W.A. 681 Knobloch, W. 2077 Knoell, A.C. 1219 Knop, WD. 2060 Knothe, K. 561 Knott, P.R. 347 Ko, P.L. 1808 Kobayakawa, M. 1638 Kobayakawa, M. 1638 Kobayakhi, A.S. 222, 913, 1925 Kobayashi, A.S. 222, 913, 1925 Kobayashi, S. 1354 Koebler, H.G. 1756 Koenigsberg, D. 756 Koerber, E. 394 Kohli, V.K. 1222 Kolkman, P.A. 387, 1883 Kolodziej, R.M. 83 Komatsu, K. 1828 Koncsek, J.L. 371

Konishi, T	Kurz, U.J 843	Leader, M.E
Kortum, W 1302, 2128	Kurzweil, L.G 2266	Leadbetter, S.A 1098
Korycki, J	Kusenberger, F.N 288	Leatherwood, J.D 1061, 1255,
Korytko, M.I 142	Kuznetsov, V.N 1104	2246
Kot, C.A	Kwak, Y.K 1872	LeDeunff, G
Kotera, T 600		Lee, A
Kounadis, A.N 1365, 2009		Lee, C.C 700
Koval, L.R 848, 1395	100	Lee, H.C 1994, 2057
Kozin, F 1995	the second secon	Lee, J.P
Kozlowski, H 570		Lee, K.L
Krag, B 1532	Laananen, D.H	Lee, M 1073
Krämer, E.O 1979	Labarge, W.L	Lee, R.A
Krasnikov, N.D 1544	Labra, J.J	Lee, S.W
Kratky, R.G	Labrujere, T.E 1624	
		Lee, T.C
Krätzig, W.B 631, 2122	Lahiry, K.C	Lee, T.H
Krauspe, P	Lai, S.S.P	Lee, T.N
Karuter, A.I	Laidlaw, B.G 1790	Lee, W.N
Kress, R 1732	Lakin, W.D	Lee, Y.T
Krey, G 1685	Lakshmanan, N 1653, 1661	Leech, C.M 1186, 2193
Krieger, W.F	Lakshmipathy, M 1620	Leehey, P 2018
Krishna, P 1645	Lal, R826, 2029	Lees, A.W
Krishnappa, G 1432	Lalanne, M	Legendre, R
Krishnaswamy, N.R 1658	Lallement, G	Leggat, L.J 290
Kronenberger, L., Jr 292	Lally, R.W	Leimbach, K.R618
Krosel, S.M 1708	Lam, P.CK	Leipholz, H.H.E 97, 985, 1990
Krumm, H	Lamb, D.G.S 1775	Leissa, A.W 729
Ku, A.B	Lambeck, M 1882	Lemonde
Kubo, K 1505	Lambert, R.G	Lemont, H.E 548
Kubo, T 1742	Lambiotte, J.J., Jr 905	Lenski, J.W., Jr 19, 194
Kudva, N.J 794	Lanati, G.A 963	Lenz, H.P 543
Kuhl, W 2021	Landau, I.D 1328	Leonard, J
Kuhlemeyer, R.L 1334, 1335	Landre, S.M	Lepik, U
Kuipers, M 2195	Lang, G.F 1530	Leppington, F.G 1329
Kulesz, J.J44	Lang, K 1323	Leung, A.Y 553
Kulig, T 1983	Lang, KW	Leung, Y.T 2237
Kulkarni, S.V307, 2225	Langham, T.F 1625	Leverton, J.W 1050
Kulys, L 1355, 1356	Langlois, H.J 1585	Levine, H 1329
Kumar, A 1557	LaPasso, L	Levine, L.S 1247
Kumar, K 1513	Lardner, R.W 2151	Levy, R 910
Kumar, M.K 1778	Lataye, R 425	Lew, H.S947
Kumar, P 1662	Latham, D	Lewandowski, J 2139
Kumar, S 1660	Latsch, R 544	Lewis, D.A 2238
Kumar, V 1617	Lau, J.L	Lewis, R.B 159, 857
Kumaraswamy, H.V 1836	Laura, P.A.A 128, 324, 616,	Lewis, R.P
Kunad, G 1869, 1870	827, 831, 1409, 1812, 2033	Li, D.F 1792
Kunesch, A.M 1841	Laursen, H.I 608	Li, J.C 592
Kunukkasseril, V.X629, 2030	Lauster, E	Liang, C.Y
Kurosaka, M 293	Lavan, M.J 1731	Liard, F 2254
Kurt Asmis, G.J 526	Laville, F	Liaugminas, R 768
Kurtz, R.L 780	Law, E.H 1080, 1262	Lilhanand, K 1320
Kurz, U 1975	Lea, P.A 858	Lim, S.P 492

Lin, T.H 1181	McCleary, L.E 970	Mahrenholtz, O 630, 708, 709
Lin, Y.K	McComb, H.G., Jr	Maidanik, G
Lin∞In, A.P 1710	McCue, G.M 242	Maier, W
Lindberg, H.E	McCurdy, D.A 847	Mains, R.M
Lindbo, T 1084	McDonald, J.R	Maiti, M 1400
Ling, R	McEwan, K.I 2264	Majima, H
Lingener, A1869, 1870	McGinness, H.D 1066	Majjigi, R.K
Link, H	McHugh, F.J 661	Majumdar, B.C98, 464,
Liou, D.DN	McIntyre, M.E	465, 605
Liou, M.S	McIvor, I.K	Makarewicz, R
Lipinski, J	McKenzie, J.R 1039	Makita, Y
Listwak, C.R	McKie, J	Malcolm, G.N 1969
Litshitz, J.M 1800	McKinnon, R.A 1228	Maley, R
Little, R.R 952	McLauchlan, R.A 285	Mall, S 222, 715, 913
Litz, L 1767	McNally, L 2003	Mallik, A.K 820, 1387
Liu, S.C	McNiven, H.D 257, 1707, 1748	Malone, J.B 511
Ljunggren, S	McNulty, G.J	Malsch, H 908
Lo, H 480, 1991, 2008, 2020	McNulty, G.M 1457	Mamalis, A.G
Lockhart, D.F 2043	McNutt, L.C	Mamode, A 1491
Loewenthal, S.H	McShane, W.R2098, 2099, 2100	Mang, H 1825
Long, G 385, 593, 642		Mangiavacchi, A
Longhouse, R.E 369		Mani, R 2092
Longinow, A 1643	M	Mankau, H 641
Loop, H 1258	200 C 100 C	Mann, F.I
Lopez, O.A 1141, 1934		Manna, M.M 1599
Lord, A.J.R	Ma, D 1561	Manning, J.E 342
Lorrain, P 1866	Mabey, D.G	Manning, R.E
	Mabey, D.G	Manning, R.E
Lorrain, P 1866		
Lorrain, P	Mabie, H.H	Manning, R.E 503 Mansbach, P.A 1173 Mantay, W.R 1454
Lou, Y.K	Mabie, H.H	Manning, R.E 503 Mansbach, P.A
Lorrain, P.       1866         Lou, Y.K.       1012         Love, W.J.       222         Lowen, G.G.       1003, 1004	Mabie, H.H.	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289
Lorrain, P.       1866         Lou, Y.K.       1012         Love, W.J.       222         Lowen, G.G.       1003, 1004         Lozier, D.W.       2249	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131
Lorrain, P.       1866         Lou, Y.K.       1012         Love, W.J.       222         Lowen, G.G.       1003, 1004         Lozier, D.W.       2249         Lu, S.C.H.       482	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690
Lorrain, P.       1866         Lou, Y.K.       1012         Love, W.J.       222         Lowen, G.G.       1003, 1004         Lozier, D.W.       2249         Lu, S.C.H.       482         Lu, Y.P.       1819	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382
Lorrain, P.       1866         Lou, Y.K.       1012         Love, W.J.       222         Lowen, G.G.       1003, 1004         Lozier, D.W.       2249         Lu, S.C.H.       482         Lu, Y.P.       1819         Lubomski, J.F.       1572, 1887	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732
Lorrain, P.       1866         Lou, Y.K.       1012         Love, W.J.       222         Lowen, G.G.       1003, 1004         Lozier, D.W.       2249         Lu, S.C.H.       482         Lu, Y.P.       1819         Lubomski, J.F.       1572, 1887         Lucas, J.G.       169	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marethe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023 Lutes, L.D. 1320	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747         Maezawa, S.       1890	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891         Marsh, J.E.       954
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023 Lutes, L.D. 1320 Luyben, W.L. 887	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747         Maezawa, S.       1890         Maga, L.J.       294	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891         Marsh, J.E.       954         Marteney, E.R.       1536
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023 Lutes, L.D. 1320 Luyben, W.L. 887 Lynch, J.W. 857	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         MacIsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747         Maezawa, S.       1890         Maga, L.J.       294         Magette, T.E.       2183	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891         Marsh, J.E.       954         Marteney, E.R.       1536         Martin, C.R.       145
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023 Lutes, L.D. 1320 Luyben, W.L. 887	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747         Maezawa, S.       1890         Maga, L.J.       294         Maglieri, D.J.       1052	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891         Marsh, J.E.       954         Marteney, E.R.       1536         Martin, C.R.       145         Martin, D.J.       160         Martin, F.A.       2202
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023 Lutes, L.D. 1320 Luyben, W.L. 887 Lynch, J.W. 857	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747         Maezawa, S.       1890         Maga, L.J.       294         Maglieri, D.J.       1052         Mahalingam, S.       1499	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marathe, P.D.       1690         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891         Marsh, J.E.       954         Marteney, E.R.       1536         Martin, C.R.       145         Martin, D.J.       160
Lorrain, P. 1866 Lou, Y.K. 1012 Love, W.J. 222 Lowen, G.G. 1003, 1004 Lozier, D.W. 2249 Lu, S.C.H. 482 Lu, Y.P. 1819 Lubomski, J.F. 1572, 1887 Lucas, J.G. 169 Ludwig, L.P. 1094 Luehr, L.H. 528 Luisoni, L.E. 827, 831 Lukkunaprasit, P. 1823 Lund, J.W. 726 Lundberg, B. 2016 Lundgren, S. 349 Lundgren, T.S. 2023 Lutes, L.D. 1320 Luyben, W.L. 887 Lynch, J.W. 857	Mabie, H.H.       988         Mabry, J.E.       521         MacBain, J.C.       1610         Macdonald, K.A.B.       512         Maciulaitis, A.       1574         Mackinnon, M.J.       169         Maclsaac, B.D.       2175         Macovski, A.       1738         MacPherson, P.B.       810         Madan, V.P.       994         Madigosky, W.       1822         Madsen, N.H.       1904         Maeda, H.       1638         Maekawa, A.       1570         Maestrello, L.       1224, 1735, 1759         Maewal, A.       1746, 1747         Maezawa, S.       1890         Maga, L.J.       294         Maglieri, D.J.       1052         Mahalingam, S.       1499         Mahapatra, G.B.       1989	Manning, R.E.       503         Mansbach, P.A.       1173         Mantay, W.R.       1454         Mantegazza, P.       1289         Marangoni, R.D.       131         Marcus, W.E.       382         Marcuson, W.F.       732         Marcuson, W.F., III       1522         Mardzanishivili, M.A.       1852         Maresca, C.       2224         Margolis, D.L.       279, 302,         1684, 1709         Markus, S.       1611         Marmol, R.A.       2279         Maroney, G.E.       502         Marples, V.       1891         Marsh, J.E.       954         Martin, C.R.       145         Martin, D.J.       160         Martin, F.A.       2202         Martin, H.R.       254

		14 20 1011
Maruszkiewicz, J 155	Messcher, W	Morgenstern, B.D 1641
Marze, H.J	Messier, R.H	Morosow, G80
Mason, A.B	Messiter, A.F	Morray, J.P
Masri, S.F	Mette, M	Morris, R.C 1847
884, 885, 1922	Midha, A1001, 1002, 1005	Morrison, D
Massalas, C 815	Miele, A 602	Morrison, P
Masso, J.F	Migliore, H.J 1919	Morrone, A 1085
Matheson, N 1436	Mikulcik, E.C	Moseley, P.K
Mathews, F.H	Milinazzo, F 1938	Mosher, M
Matsuhisa, H 690	Miller, H.A	Mota Soares, C.A 801, 802
Matsui, M	Miller, R	Mote, C.D., Jr 415, 1324, 1458
Matsuki, M	Miller, W.T	Moulton, A.E
Matsukura, Y1337, 1881	Milner, J.R 1682	Mroz, Z
Matsumoto, H	Milstead, R.M 1995	Mruk, G.K
Matsuo, K	Milz, U 1780	Mudunuri, B
Matsushima, M	Minami, T	Muelleman, N.F
Matsuzaki, Y	Mineck, R.E	Mufti, A.A 1493
Matta, R.K 2092	Minirudrappa, N 1644	Mugridge, B.D
Matthew, G.K 678, 1589	Mirza, S 1393	Mühle, EE 1955
Mattu, R	Misra, J.C 630	Mukerjee, D
Matuk, C	Mitchell, J.S 1340, 2189	Mukerjee, S 1698
Maunder, L 679	Mitsui, J 1195	Mukherjee, A
Maus, J.R 1741	Miura, H	Mukhopadhyay, M 130, 1411
Mayer, T.C 69, 451	Mixson, J.S 1229	Muleski, G.E 1198
Mayes, W.H	Miyachi, T	Muller, A.A
Maymon, G 1149	Miyakawa, S	Müller, E
Maza, V.M	Miyake, Y	Müller, J 1771
Mazumdar, J	Mizusawa, T 1399	Muller, P.C 1290, 1480, 1517
Mead, D.J53, 791, 793,	Mizutani, H	Munaswamy, K
820, 2026	Mlakar, P.F	Munson, A.G
Mech, S.J 2094	Model, R	Murakami, H 1746, 1747
Medearis, K	Modi, V.J 60, 85	Murali, B.N
Meek, J.W	Moehle, J.P 1043	Murata, S
Meggitt, D.J	Moffett, M.B	Murphy, J.D 1207, 1612
Mehta, L.C	Mohan, J	Murphy, M.J
Mehta, N.C 1091	Mohanty, B.P	Murray, B.E
Mei, C	Mohring, W	Murray, B.S 1248 Murray, M.G., Jr 1456
Mei, C.C	Mohsen, E.A 2073	
Meinke, P	Molnar, A.J	Murthy, P.N
Meirovitch, L	Mondkar, D.P	
Melvin, J.W	Monk, R	Muszyńska, A
Mengi, Y 257, 1707, 1748	Monteil, P 225, 226, 227, 228	Muthuveerappan, G 1408
Merchant, H.C 1135, 1136	Moodie, T.B	Myers, W.N
Mereau, P	Mook, D.T	Myles, M.M
Meredith, D	Moon, F.C	Myncke, H 426
Merhof, W	Moore, C.J	
Merkli, P	Moore, J.E., Jr 1635	N
Merklinghaus 1694	Moore, W.L	N
Merlet	Moran, M.S 1311	
Merritt, R.G	Morand, H	Nachtigal, C.L
Meskouris, K 2122	Morfey, C.L	Naftzger, R.A 1154

Nagamatsu, A 289	Newman, M	Oda, J 1288
Nagashima, T 607, 2005, 2006	Newmark, N.M	Odar, E
Nagaya, K 322, 1209,	Ng, K.W 1516	Oesterle, R.G 497, 517, 1027
1412. 2031	Nguyen, D.T 2285	Ogawa, K
Nagl, A	Nguyen, P.K	Ogden, S 188
Nagy, D.A	Nicholas, J.C 1793	Ogg, J
Nagy, K 688	Nichols, B.D 703	Ohara, K
Nahavandi, A.N 418	Nichols, C.S	Ohashi, M 1505
Nair, P.G.B 1658	Nicholson, D.W	Ohayon, R 1761
Nair, S	Nicholson, M.A 1239	Ohlson, J.F 1383
Nakagawa, N 34, 64	Nickels, R.C., Jr 111	Ohta, M
Nakahara, I	Nicolas, D 2201	Ohtsuka, N 260
Nakamura, A 29, 30	Niedzwiecki, A	Oishi, N 1881
Nakamura, T	Nielsen, L.E	Oka, F
Nakamura, Y	Niemann, HJ 632	Okazaki, K 1209, 2031
Nakano, M 260	Nier, E 1753	O'Keefe, W 1374, 1623
Nakayama, I	Nigam, N.C	Okrent, D 2269
Nandakumaran, P 1645, 1652,	Nikolakopoulou, G.A 327, 1827	Okubo, H 1638
1654, 1698	Nikolau, V.I 1669	Oldham, D.J 2073
Narayanan, G.V90	Nilsson, A.C 895	Oldham, K 585
Narayanaswami, R 1817	Nilsson, B 103	Oliver, L.R 1886
Narita, Y821, 1022	Nilsson, L	Ollerhead, J.B 648, 649
Naruoka, M 1399	Niordson, F.I	Olsen, W.A
Nashif, A.D 52, 54	Nishida, S 620	Olsen, M.D 1407
Nassar, E.A.M	Nishimura, M	Olunloyo, V.O.S
Nasar, E.M 832	Nissim, E 850	Oluyomi, M.A 911
Nath, B	Nittlinger, R.J 1286	Opicka, F 1292
Nath, Y	Niwa, A 524, 1204	Orlik-Rueckemann, K.J844,
Nathoo, N.S 1092, 1093	Niyogi, B.K	1443, 1631
Natke, H.G 567	Nobile, M.A	O'Rourke, M.J 1593, 1595,
Naudascher, E 609	Nogis, R 1404, 1405, 1413	1597, 1598
Nayfeh, A.H 470, 611, 627,	NoII, T.E 845, 2244, 2245	Orsero, P
757, 794, 803, 1723	Nolle, H	Ortner, N 1179, 1180
Nazin, V.V 1680	Noor, A.K903, 905	Osborne, R.L
Nazir-Ul-Haq 1503	Noordzij, L	Oshima, N
Nazli, Z	Nordmann, R2109, 2115	Osman, A.E.M 681
Neal, E	Nowack, H 1973	Osman, M.O.M
Neale, K.W 325	Nutt, R.V	Ostiguy, G.L 66, 776
Nebat, J 1296	Nyman, D.J	Ostrovsky, L.A
Neelley, C.E 168	Nypan, L.J 1563	Otomi, K 1362, 1551
Neise, W 1804	Nystrom, P.A	Ottl, D 2015
Nelson, D.J 1941		Ousset, Y 580
Nelson, H.M 284		Oved, Y 1938
Nelson, I	O EL WOR	Ovunc, B
Nelson, P.M	180 505	Owen, D.R.J 624
Nemat-Nasser, S 758, 829, 936		Ozdemir, H 1789
Nessler, G.L	Oates, J.A.H 576	
Nesteruk, K	Obal, M.W	Look P macroshub
Neubert, V.H84, 1985	Oberai, M.M 619	
New, R.W 1516	Obermayr, K	
Newman, J.R	Och, F	Packman, A.B 570

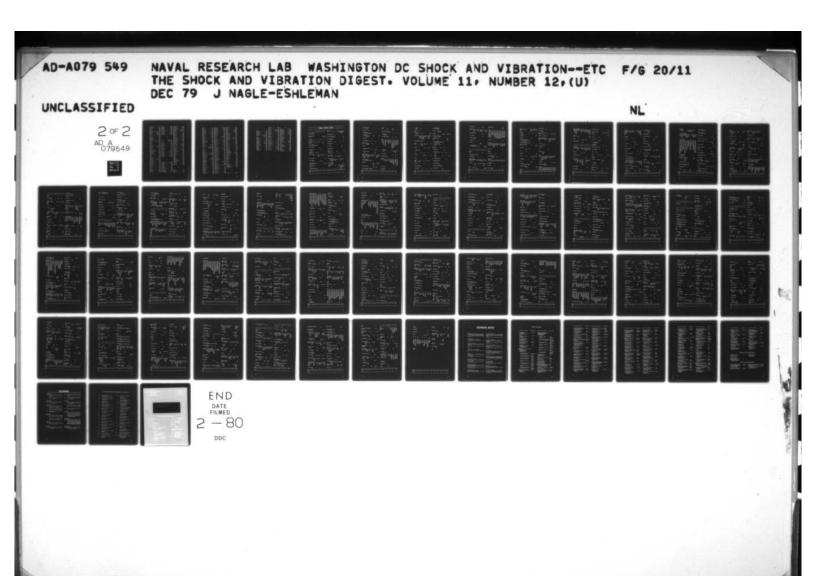
Paez, T.L	Perez, D.J 1634	Poon, C.J 2158
Paidoussis, M.P 88, 1184,	Perfect, N 1874	Poon, D.T85
1185, 1201, 1826	Perreira, N.D 1683	Pop, J.J
Pakstys, M	Perella, W.M., Jr 1849, 2063	Pope, J
Palaniappan, E.A 1521	Perrin, J.H	Popovici, A 1048
Pallett, D.S 660	Perrone, N	Popplewell, N 1487, 1749
Panayotounakos, D.E 2009	Peschier, T.D 849	Porcella, R 861
Pandalai, K.A.V 326, 490, 1603	Peters, D.A 356, 689, 990	Posehn, M.R 221
Pandey, A.D 1617, 1645	Peters, D.J	Poulos, H.G
Pandit, V.K	Petersen, C 658	Povzner, A.Y
Panfero, N.M 1104	Petersen, T.J 1629	Powell, C.A 847, 866, 1243
Pao, Y	Peterson, B.S 1143	Powell, G.H 419, 423, 1123
Pao, Y.C	Peterson, M.R	Powell, R.G
Parakh, G.C	Petrovich, S.A 1648	Prabhakara, M.K
Parameswaran, M.A 1455	Pettigrew, M.J 1201	Prakash, B.G 795
Parbery, R.D 1788	Petyt, M 492, 800, 801, 802	Prakash, R
Pardoen, G.C 132	Phelps, H.N., Jr 964, 967, 968,	Prakash, S 1513
Parin, M.L	971,972	Prasad, B.B 1550
Paris, P.C 509	Phillips, A	Prasad, B.K.R 1977
Park, A.C	Phillips, L.N 1946	Prasad, T
Park, K.C 203, 207, 441, 1697	Phillips, N.S	Prathap, G
Parkins, D.W 1565	Pi, W.S 2068	1410, 1603
Parkinson, A.G	Piau, M	Prause, R.H
Parmenter, W.W 50	Pickard, J	Price, H.L
Parr, V.B	Pickett, W.H	Price, P 1029
Parsons, J.D	Pierucci, M	Price, W.G468, 1481
Parsons, M.G	Piety, K.R	Priemer, R
Parthan, S	Pignolì, C.R	Priori, G
Parzygnat, W.J 822	Pike, A.C 1050	Priscu, R
Passari, L	Pikul, R.R	Pritz, T
Pate, M.L	Pilkey, W.D 836, 1546,	Przemieniecki, J.S 1446
Patel, B.M	1834, 2161	Psaraftis, H.N
Patel, J.S	Pinkham, C.W 1232	Pujura, K.K
Patel, M.H	Pinkus, O	Purdy, D
Patel, M.P	Pinson, L.D 1098	Puri, V.K 1509, 1654
Patrick, L.M 1265	Piombo, B	Pusey, H.C 1920
Paul, D.B	Piranda, J	Pyatnitskiy, Y.S 907
Paul, D.K 1506, 1600	Pircher, H 1896	Pye, C.J 1779
Paul, H.S	Pisano, A.D 1958	Pytko, S
Payne, S.G	Pister, K.S	1,100,000
Pearson, J	Pistone, G 1495	
Pease, C.B 1071	Pixton, T.A.H 472	•
Pecker, A	Platt, C.E	Q
Pecknold, D.A	Platt, J.P., Jr	
Pedersen, O.J	Platzer, M.F	Qamaruddin, M 1647, 1854
Peeck, A	Ploeger, D.W	Quade, D.A 1034, 1035,
Peeken, H	Plotkin, K.J	1036, 1037
Pegg, R.J	Plummer, M.C	Quadflieg, H 641
Peleg, K	Plunkett, R	Quindry, T.L
		Quinn, B
Penny, J.E.T	Polak, E 2261	
D	Pollock, A.A 1350	Quinn, R.W

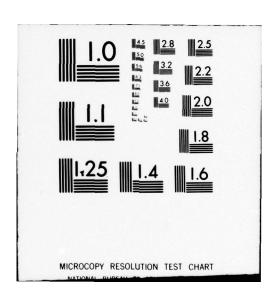
R A	Rao, V.R 1844	Rinehart, R.E 696
	Rasch, W	Rio, R.A1949, 2165, 2167
	Rasmussen, G 1343	Rivers, D.W 2146
	Rathnam, K	Rivin, E.I
	Rauch, T	Rizzetta, D.P 769
Rabbat, B.G 138, 517,	Rault, A 1497	Rizzo, V
2049, 2247	Ravanel, MA 601	Roberson, J.A 158
Rack, M 1982	Rawtani, S 1190	Roberts, J.B 238, 749, 784
Rackwitz, R 429	Ray, D 1664	Roberts, W.B 1752, 2156
Rades, M	Rea, D	Robinson, R.R1144, 1145
Radhakrishnan, R 1651, 1857,	Rebont, J 2224	Robson, J.D 693
1863, 1864	Reddy, D.V	Rodden, W.P 1729
Raftopoulos, D.D952	Reddy, J.N 728, 1939, 2035	Roesset, J.M 860, 950, 1045,
Raghavan, K.S 819	Reddy, T.Y	1046, 1047, 1666
Raghunandan, C.R 96, 286	Reding, J.P 2069	Royers, A 1164
Raider, J.W 2057	Reed, C.L	Rogers, A.M 1510
Rainer, J.H 1641	Reed, K.E	Rogers, L.C
Rajanna, B.C 1644	Reed, R.S., Jr 1125	Rogers, R.J 1419
Rajaraman, A	Reethof, G	Rogers, S.R
Rajkumar, C 1557	Reich, H	Rohde, S.M 1564
Raju, I.S 486	Reichenbach, F.M881	Rohrle, H 554
Raju, K.K 486, 818, 1019	Reid, S.R 1026, 1221	Rollvik, S 1511, 1512
Ram, B.S 1524, 1650	Reilly, M.J 153, 1264,	Rom, J 2067
Ramachandran, J 1833	1265, 1266, 1267	Romander, C.M 475
Ramaiah, G.K 127	Reinhold, T.A 659	Romberg, T.M
Ramakesavan, S 2151	Remington, P.J 1462	Romeo, D.J
Ramakrishna, B.S 313	Remmers, E.P 811	Romilly, N 417
Rama Murthy, T.V 1778	Rempel, J.R 1126	Ronneberger, D 1331
Ramamurti, V 413	Renger, A 1706	Roos, H.J 2086
Raman, J 1657, 1659	Reynolds, R.S 1545	Roos, R 1624
Raman, P.V	Rhodes, D.J	Rosemeier, G
Ramer, D.J 1242	Ribner, H.S	Rosenblueth, E 917, 1448
Ramsey, K.A962	Rice, E.J 105, 1577, 1578, 1579	Roskam, J
Rand, R.H	Rice, J.R	Ross, C.F 841
Randall, S.E 1220	Rice, J.S 175	Ross, D
Raney, J.P	Rich, B.L 141	Ross, S.M 577
Rangaiah, V.P 1985	Richards, E.J 1459	Rossin, R 1569
Rangaswami, R 1559	Richards, R., Jr 1619	Rothaug, K 265
Ranjan, G 1660	Richards, T.L 1470	Rouverol, W.S 2011
Ranken, R.E 1948	Richardson, J.M 942	Row, D.G 1123, 1124
Ranlet, D 204, 493, 734	Richey, A.E	Rowe, W.T 1228
Ranshi, A.S 176	Richter, T 2253	Royal, A.C 1282
Rao, B.M 292	Ricker, R.E 44	Rubayi, N.A 283
Rao, B.V.A 287	Ricker, T.W	Rubin, D
Rao, C.K	Rickert, B.M 2177	Rubin, H
Rao, D.K 89, 595, 790	Rickley, E.J	Rubin, S 956
Rao, G.V 486, 779, 818,	Rieger, N.F 1303	Rubinstein, N 783, 2282
1019, 1817	Riffel, R.E 1520	Rudnick, I
Rao, N.S	Rijnja, H.A.J 28	Ruetenik, J.R 2101
Rao, P.V	Riley, P.P 1298	Ruf, G
Rao, S.S 819, 1117, 1844	Riley, W.W 1865	Ruggeri, T

Rugh, W.J 1712	Sankaran, K.S 1658	Schoen, B 1226
Rumerman, M.L 1734	Santhakumar, A.R 1559,	Schöllhorn, K 2109
Ruo, S.Y923, 924	1620, 1646	Schomer, P.D 1171
Ruscheweyh, H 706	Saran, S 1513, 1660	Schrage, D.P
Russell, H.G 497, 2049, 2247	Saravanamuttoo, H.I.H 2175	Schreyer, H.L 993
Russell, M.F 1269, 1270	Sarna, S.P 695	Schroeder, E.C 1031
Russell, R.E	Sarpkaya, T	Schubert, K
Russell, T.E	Sathikh, S 413	Schuetz, D
Rutenberg, A 515, 2194, 2248	Sathyamoorthy, M 484, 1604	Schuller, K 1787
Rüter, G 1063	Sato, K	Schultz, T.J
Rutherford, S.R	Sato, S 690	Schulze, B 1531
Rutledge, J 2167	Sato, T	Schumacher, R.T 196
Ryan, W.W., Jr	Sato, Y	Schwartz, C.W 1528
Ryden, L 1256	Satter, M.A 1608	Schwarz, M 1838
Ryde-Weller, A 1891	Saunders, A.S 164	Schwer, L.E 45, 475
Rylander, R	Savidis, S.A 2253	Schwerdlin, H 978, 2220, 2222
	Savy, J.B.U 1933	Schwerdtfeger, H 1955
	Sawatari, T 1737	Schwieger, H 934
S	Sawdy, D.T	Schwirzer, Th 1896
	Sax, M	Sciarra, J.J 19, 194
	Sayers, M.W 1079	Scott, R.A
Sachse, W 1733	Scalise, D.T	Scott, R.F
Sackman, J.L2150, 2185	Scanlan, R.H 352, 353, 2228	Scott, I.G 1315
Sadek, M.M 681	Scavuzzo, R.J 610	Scott, W.A
Safar, Z.S 2199	Schaeffer, E.G 194, 1250	Screwvala, F.N 1526
Safford, F.B	Schapery, R.A 1474	Seaman, P.E 968
Sagartz, M.J	Scharnhorst, K.P 1332	Seborg, D.E
Saini, S.S	Schary, M	Sedney, R 491
St. Hilaire, A.O 1763	Schauer, J.J	Seebass, A.R 1444
St. John, D.L	Schiff, A.J	Seed, H.B 1926, 1927
St. John, R.C 1885	Schiff, M.I1422, 1423	Sehitoglu, H 1711, 1907
Saito, H 1362, 1551	Schiffman, M.C 1954	Seifferth 1694
Sakata, T 830, 1714, 1918, 2037	Schildt 1694	Seireg, A
Sakata, Y 2037	Schilken, R 704	Sela, U
Sakurai, S 1663	Schirmer, W	Selleck, R.A 798
Salama, A.L	Schlack, A.L., Jr	SenGupta, G 147, 1430
Salama, M 2120	Schlesinger, A 1678	Sensburg, O
Salamone, D.J 2162	Schliekelmann, R.J	Senseny, P.E 1772
Saliba, G 1868	Schlinker, R.H 1376	Sentek, J
Salvadori, M.G 816, 817	Schlitzer, L.D 182	Sertour, G
Salvidge, A.C 2097	Schmid	Seshadri, T.V
Samaha, M.A	Schmid, H	Sethna, P.R
Samant, C.G 1858	Schmid, I 177	Seto, K
Sandercock, D 1752	Schmidt, E	Seybert, A.F 2, 781
Sanders, J.R 812	Schmidt, L.V	Shah, A.H
Sandford, J 1626	Schmit, L.A., Jr 559	Shah, L.C
Sandler, B.Z 1976	Schmitz, F.H 671, 1053	Shah, V.N
Sandler, I.S	Schneider, B 1982	Shahabadi, A854
Sandman, B.E	Schneider, C.P 1695	Shahinpoor, M
Sankar, S	Schneider, J.F 589	Shaishmelashvili, V.N 1860
Sankar, T.S	Schnobrich, W.C 1030, 1853	Shakal, A.F
odinar, 1.5	Jointobrich, 14.0 1000, 1003	Gridadi, M.1

Shaker, B.S 611, 1723	Singer, J 1206, 1829, 1830	Snyder, M.R 1038
Shanks, J.M 1186	Singh, A.K 1599	So, W
Shantaram, D	Singh, A.V 1393	Sobel, P.A
Shapiro, A.B 2277	Singh, B.M	Sobieczky, H 1444
Sharan, S.K	Singh, D.V 1791	Socie, D 1965
Sharma, C.B 1831	Singh, K 1387	Sodhi, D.S
Sharma, R.K 1652	Singh, M	Soedel, W 340, 1460, 2024
Sharma, S.K 243	Singh, M.P	Sofrin, T.G 1577
Sharma, V.P 2233	Singh, P.S 1654	Sofronie, R 1040
Sharp, B.H 495	Singh, R 274, 1460, 2024	Sofue, Y
Shaw, J	Singh, R.D 1525	Soh, C.H
Shaw, L.L	Singh, V.K 1190	Sohre, J.S 2250
Shaw, R.C.J	Singhal, M.K 1693	Sokolova, Y.A 1058
Shaw, R.J	Sinha, B.K	Soldatos, K 815
Sheets, H	Sinha, K.N 1657	Soleimani, D 2215
Shefrin, J 1265	Sinha, P.K	Solla, E
Sheinman, I	Sinha, S.C 711, 1102, 1898	Soni, S.R 1409
Shepherd, K.P 1241	Sinhasan, R	Sonoda, T
Sherkat, V.R	Sislian, J.P	Sotiropoulos, G.H594
Shevchuk, G.J 1017	Sisto, F	Soustova, I.A
Shiau, L.C	Skaff, A 242	Southwood, B.J 1050
Shibata, H	Skaistis, S.J 523, 2286	Sozen, M.A 1043
Shidler, P.A670, 1454	Skibo, M.A	Spalding, G.R
Shieh, R.C	Skinkle, M.E 1515	Spandrio, A.M 187
Shifflet, G	Skinner, D.W	Spanos, PT.D 430, 912,
Shih, P	Skop, R.A	1138, 1701
Shilling, R.B., III 1012	Skow, A.M 1630	Sparks, P.R 659
Shimogo, T	Skrikerud, P.E 1086	Sparmann, R 701
Shin, Y.S	Sleeper, R.K 403	Speakman, J.D146, 344
Shinozuka, M	Slonim, A 1976	Spector, S.R 675
Shiu, K.N	Slonim, M 1976	Spencer, A.J.M
Shivashankara, B.N 167	Slutsky, S 2098, 2099, 2100	Sperry, W.C
Shkola, A.V	Smalley, A.J	Spielhagen, D 1870
Short, S.A	2154, 2164	Spiker, R.L 1720
Shostak, A.G	Smiley, R.F	Spindel, J.E 1902
Showalter, J.G 1920	Smith, C.C	Spurk, J.H
Shrivastava, S.K	Smith, D.A 1682	Sreekantiah, H.R 1656
Shum, K.L	Smith, D.L 1447	Sridharan, A 1659
Siddorn, T.E 290	Smith, E.B	Sridharan, K
Siegner, H 2052	Smith, G.M	Srifuengfung, D 571, 1042
Siegrist, G	Smith, J.H	Srinivasan, K
Sienkiewicz, A 965	Smith, J.R	Srinivasan, R.K 1400
Sigillito, V.G 783	Smith, N	Srinivasan, R.S 851
Sigman, R.K 684	Smith, P.W., Jr 319, 625, 1294	Srinivasulu, P 1653, 1661
Silver, M.L 2096	Smith, R.R	Srivastava, L.S1509, 1540, 1667
Simiu, E	Smith, R.T	Stadelbauer, D.G 215
Simmonds, J.G	Smullin, J.I 1846	Stadter, J.T 783
Simpson, D.G 1775	Smy, P.R 1938	Stafford, J.F
Simpson, H.M 1802	Smythe, R.C	Stagliano, T.R 1720
Sinclair, G.B 953	Sneckenberger, J.E 236	Stahl, B
Sinclair, J.H	Snowdon, J.C	Staid, P.S
Oniciali, 5.11 1999	5110Wd011, 5.C	State, 1.5

Stakolich, E.G 1069	Stuurman, A.M	Takahashi, Y
Standing, R.G 500	Subrahmanyam, M.S 1656	Takayanagi, T 1030
Stanway, R 1342	Subramanian, R 717	Takemiya, H 951
Stapleford, R.L 1848	Succi, G.P 299	Takeuchi, R
Stapper, M	Sugimoto, N 206	Takeyama, H 1815
Starace, J.J 2100	Suharwardy, M.I.H 1373, 2210	Talaslidis, D
Stasyszyn, N 2074	Suhner, O.H	Talbot, R.J 1446
Stavsky, Y824, 1609	Sullivan, B.M.S	Tam, D.S.F 1931
Stea, W	Sullivan, J.W	Tam, P.K.Y
	Sullivan, P.A	Tamura, A
Steckler, K.D		
Steenackers, P 426	Sun, C.T 480, 2008, 2020	Tanaka, S
Steenken, W.G 799	Sundaram, S 1858	Tang, D.T
Steiger, A.R	Sundararajan, C 896	Tani, J
Steininger, M 1971	Sung, S.H	Tanida, Y 2005, 2006
Stenschke, R 380	Suresh, S	Taniguchi, H.H
Stephen, R.M	Sussman, H 969	Tanimura, S
Stephens, D.G 159, 857, 866,	Sussman, N.E	Tann, T.A
1062, 1253, 2246	Sutin, A.M	Tanner, A.E 1264
Stephens, R.W.B 438	Sutphin, H.W 69, 451	Tansirikongkol, V901, 1923
Stepniewski, W.Z 2260	Sutton, H.B	Taylor, D.L
Stere, C 1048	Sutton, J.L 1736	Taylor, J.I
Sternfeld, H., Jr	Suzuki, H	Taylor, R.E 546, 547
Stetson, K.A 401	Suzuki, K	Tecza, J.A 2154
Stevenson, A.E956	Suzuki, S	Tee, G.J 1492
Stevenson, J.D 537	Suzuki, S 1070	Teh, K.K
Stewart, S	Suzuki, Sl	Teichmann, D 1782
	Swaddiwudhipong, S 2048	Teipel, K
Stiewitt, H		Teramoto, M
Stockmaier, H	Swan, P	
Stoddard, F.S 2000	Sweetser, E.I	Terauchi, Y
Stoke, K.H	Swisdak, M.M., Jr	Tesar, D
Stokey, W.F 610	Sylvester, J 960	1011, 1589
Stone, B.J 1779	Symmons, G.R 680	Tesch, W.A 799
Stone, D.E.W	Symonds, P.S 981, 1000,	Tester, B.J
Stotler, C.L	1210, 2230, 2231	Tezak, E.G 803, 1897
Stott, S.J 873, 884, 885	Szemplinska-Stupnicka, W 1702	Thajuddin, M.D 102
Stoykovich, M 536	Szenasi, F.R 613	Thakkar, S.K
Strandberg, M.W.P 1380	Szenaski, F.R	Thambiratnam, D.P 1816, 2039
Strange, W.A 1610	Szewczyk, V.M 747	Thandavamoorthy, T.S 1661
Strasberg, L		Thiele, F
Strasberg, M		Thomas. H
Strauss, A.C		Thomas, HJ 699, 2107
Strenkowski, J 836	T	Thomas, J
		Thomas, R.E 1031
Stringas, E.J	T M 1011	
Struebel, R	Taat, M	Thompkins, W.T., Jr 1476
Stubbs, S.M	Tabarrok, B	Thompson, J.P 1628
Stubley, P.H	Tada, M	Thompson, J.R 2045
Stubstad, J.M	Taha, M.M.A	Thoms, R.L949
Stuehlen, B 957	Takada, S 1199	Thomsen, C
Stühler, W	Takahashi, I	Thomson, W.T 1451
Sturgeon, J.B 1946	Takahashi, K 837, 1786	Thornton, W.A 6, 2129
Sturmath, R 2014	Takahashi, S 983	Thullen, P 1017





Thurman, R.G 1033	Tsubuku, T 1584	van Selst, A.M 1641
Thurston, G.A 716	Tsujimoto, Y	Van Tuyle, G.J 1466
Tiagi, S.S 1693	Tsztoo, D.F645	Van Zanten, A 1472
Tichy, J 929	Tucker, P.B 156	van Zanten, A.Th 2044
Tichy, J.A	Tuichiyev, N.D 1859	Varadan, T.K 86, 490, 1410
Tieleman, H.W 659	Turney, D.L 1068	Varadan, V.K
Tielking, J.T 1309, 1310, 1474	Tuten, J.M 1262	Varadan, V.V
Tiersten, H.F761, 2143	Twomey, W.J	Vargas, L.M44
Tindle, C.T	Tyler, J.W 2105	Vasilakis, J.D
Ting, E.C 1110, 1689	Tylikowski, A 2227	Vaskor, J.G 1929
Ting, T.C.T		Vasudeva, R.Y
Tison, J.D 902		Vedros, P.J., Jr691, 692
Titiriga, A., Jr 1630	U Province	Vehlow, C.A 183
Tittemore, G 1368		Veluswami, M.A 1408
Titterington, D.M 1494		Venkataramana, J 1400
Tiwari, R.N	Überall, H 218, 940, 1207,	Venkatesan, S 629, 2030
To, C.W.S 1346, 1347, 1361	1332, 1612	Venkayya, V.B
Tocci, G.C	Ueda, T 1824	Venkitarama, S 1741
Tokle, P	Ueng, C.E.S	Verchery, G
Tollin, P	Ueno, H	Verderaime, V
Toluoka, T 1740	Ueyama, H	Verma, U.S.P1558, 1599
Tomisawa, M 1337, 1881	Uffelmann, F	Verykios, X.E
Tomlinson, G.R 1418, 1908	Uher, R	Vesser, W
		Viano, D.C
Tonin, R.F	Uhlig, C	Viergever, M.A
Toridis, T.G	Ujihashi, S	Viergutz, O.J
Torisaki, T	Unger, R	Vigstad, M
Torkamani, M.A.M 1451		Vijayakumar, K 127
Torres-Cabrejos, R.E932	Upton, H 548	
Torzicky, P 1825	Urabe, Y	Vijayvargiya, R.C 1660
Townsend, F.C	Urashima, C	Vincent, J
Townsend, M.A	Ushijima, R	Vinson, T.S
Tran, C.T	Ushijima, Y	Vislavičius, K
Trask, Y	Utley, W.A 1912, 2097	Vito, R.P
Trechsel, H.R	Uygur, E.M 263	Vogel, A.O
Tretout, R		Vogel, S
Triebstein, H 1675		Völckers, J 1996
Trifunac, M.D 572, 973, 1504	V	Volin, R.H 1920
Trikha, D.N		VonderDecken, J 1531
Troeder, Ch		von Nimitz, W.W 613
	Vaidya, P.G 298	von Seggern, D.H 2146
Trolinger, J.D 1545	Vaidyanathan, C.V 1581, 1653	Vrijer, A 1883
Trompette, P 601	vanAken, J 782	Vugts, J.H
Trout, E.M	Van Blaricum, P 1942	Vujanovic, B 199
Trubert, M 2120	Vance, J.M 902	
Trygg, B	Vance, O.L	
Tsai, C	vanDam, C.P.G842	did W F1 S years did
Tsai, M.S997	van der Toorn, J.D 892	
Tsakonas, S 1797	Van Eijk, J 1214	
Tsao, M.C.C	Van Fossen, D.B	Waal, J.C
Tslaf, A 1976	Vanmarcke, E.H	Wachel, J.C 889
Tso, W.K	van Oossanen, P 373	Wagner, R.A 676

Wehrli, R 660	Wilson, A.H	Xistris, G.D 66, 776
Wedpathak, A.V 1655	Willson, A.J	
Wedig, W	Willmert, K.D 6, 2129	
Weck, M 2091	Willis, T 173	X
Webster, W.C 1192	Williamson, G 1758	
Webster, R.L 1919	Williams, R.S 1158	
Weaver, D.S	Williams, R.M 650	Wysocki, E.M
Waymon, G.R 156	Williams, R.J 2131	Wyn-Roberts, D 389
Wauer, J 2090	Williams, R.C	Wünsch, D
Watson, R.B	Williams, F.W 20, 101, 1360	Wunderlich, W 1014
Watson, P 1945	Williams, D 1230	Wu, Y
Watson, J.H 1285	Wilharm, H 1978	Wu, S.T 2153
Watanabe, T 1890	Wilgen, F.J 1547	Wu, R.W.H 1720
Watanabe, M	Wilby, J.F 1248, 1846	Wu, J.J 1359
Wasserman, Y 2010	Wilbeck, J.S48	Wu, A.K 602
Washizu, K	Wijesinghe, A.M	Wright, J.P
Washio, S 1809, 2226	Wierzcholski, K	Wright, J.C 1390
Warudkar, A.S	Wierzbicki, T	Wright, C.J
Warren, R.E	Wieneke, S.A	Wosik, J
Warnaka, G.E	Wienele S.A	
		Woonley, B.L
Ward, D.W	Wiedenmann, R	Woolley, B.L
Ward, D.W	Wickens, A.H	Woollett, R.S
Warburton, G.B 598, 599, 2034	Wichman, K	Woodward, R.P 169, 1069
Wanhill, R.J.H	Whitman, A.M	Woodward, K.A 1417
Wang, Y.S 1077	Whitfield, C.E 545	Woodhouse, J 57
Wang, T.G	Whitfield, A 2263	Wood, W.L 702
Wang, P.C 1330	Whitemarsh, S.L	Wood, W.E 452
Wang, M.E	Whitehead, D.S 607, 1129	Wood, E.W
1595, 1596, 1597	White, R.P., Jr 1116	Wood, C.J
Wang, L.RL 1197, 1593, 1594,	White, R.N 539	Wong, F.S 1725
Wang, J.T.S 2042	White, J.L	Wollherr, H 2021
Wang, J.S	Whaley, P.W 76, 148	Wolff, F.H
Wang, D.T	Wetton, R.E 1327	Wolfe, R.A 2258
Wang, C.C	Westine, P.S 44, 578	Wolf, R.J 1169
Wan, C.H 1445	Westcott, M.E 1459	Wolf, J.P
Wambsganss, M.W 1689	West, H.H 1562	Wolf, E.J 1878
Walton, W.S	Werkmeister, R.F 1223, 1435	Wojcik, G.L
Walter, P.L	Wentz, R.A 1091	Wittenburg, J
Walsh, J.P 510	Weng, G.J 2211	Witmer, E.A 422, 489, 1720
Wallrapp, O 2102	Wen, Y	Wisniewski, H.L 193
Wallin, A	Welp, E.G 2050, 2051	Wirt, L.S
Waller, H	Wells, E.W	Winther, B.A
Waller, D.A 1425	Weller, W.H	Winkler, G
Wallace, F.J		
	Welch, R.E 1088	Wing-King, A.M 1426
Walker, R.E 40, 134	Weissman, S 1029	Winer, D.E
Walker, M.J	Weisshaar, T.A	Wilton, D.T
Walgrave, S.C	Weisberg, M.W	Wilton, C
Walcott, W.B	Weir, R.M 2002	Wilson, J.F 1268, 2267
Wakai, H	Weinstock, H 1083	Wilson, J 1963
Waite, J.B	Weinberg, M 1976	Wilson, E.L
Wahba, N.N	Weidlinger, P	Wilson, D.S 1338

TENTENT Y BEST MARKET	Yang, H.T.Y 1445	2
	Yang, J.C.S	
	Yang, J.N 1280	Zable, J.L
	Yang, T.Y 123, 1397, 1991	Zachman, N.J 655
Yadav, D	Yao, J.T.P932, 1110	Zagajeski, S.W 1582
Yaeger, R.C	Yasuda, K	Zajaczkowski, J 1313, 1357
Yahraus, W.A	Yasue, M	Zakic, B.D
Yakovlev, P.I	Yasumoto, Y30	Zammert, W.U 1384, 1960
Yakovlevich, D.I 1507	Yates, J.E 2137	Zarek, J.H.B 840
Yamada, G 821, 823, 1018,	Yazaki, Y 620	Zarur, G.L
1022, 1552	Yeghiayan, R.P510	Zaveri, K
Yamada, T 1195	Yeh, T.T	Zbieranowski, W965
Yamada, Y 951	Yeung, K.S 1088	Zebarjadian, A
Yamamoto, F 1568	Yim, S.J 1785	Zharov, A.M 1851
Yamamoto, T 986	Yocum, A.M., II 878	Ziebarth, H 1955
Yamamoto, T 1353, 1781	Yokel, F.Y 732	Zieglar, G 1998
Yamamoto, T 1390	Yoshimura, H.R	Zienkiewicz, O.C
Yamamoto, Y 2022	Young, M.E919, 920	Zijp, D
Yamane, T 1056, 2278	Youngdahl, C.K	Zilch, K 657
Yamanouch, M	Yousri, S.N 784	Zilinskas, G 1737
Yamanouchi, M 174	Youssef, N.A.N 1487, 1749	Zimmermann, H
Yamazaki, K 1288	Yu, N.J	Zimmermann, W
Yan, M.J	Yu, Y.H 671, 1053	Zini, G 961
Yanabe, S 1354	Yuhas, D.E 959, 1352	Zinn, B.T 684
Yanagisawa, E 1766	Yun, C.B	Zorea, C 2067
Yancey, C.W.C	Yuruzume, I 1584	Zorumski, W.E 346
		zur Lippe, C.F 1158

STRE Hongoter TOTAL GLOSS PM

### ANNUAL SUBJECT INDEX

	· A -			Acoustic Linings 1580	103 2	4	1426	997	998	469
				1000			-	427	1378	1579
bsorbers (Equipment)									1428	
642				Acoustic Measures	ment					
				Accountic measure.	67	4				
bsorbers (Materials) 840 1621			1838 839			3				
840 1021			1839	Acoustic Measurin	g Instrumer	ate				
			1009		1173					959
ccelerometers				Atis Missassas						
170 591 1773	75	76 2187		Acoustic Microsco						
				1002						
coustic Absorption				Acoustic Propertie						
30 2241 73	74 1165	1316	28	31	68	4		27		16
840			1428							
				Acoustic Radiatio	n					
coustic Attenuation				31						
use Acoustic Abs	orption									
				Acoustic Range					2058	
Acoustic Detectors		1736							2058	
		1.00		Acoustic Reflection						
Acoustic Diffraction				330	on					
2241		237		330						
				Acoustic Resonan	re					
Acoustic Emission				1470 311		1165				112
1350 1821	2184 1315									
				Acoustic Resonat	ors					
Acoustic Excitation							26			
192		1306 627								
	555	857		Acoustic Respons			.1.			
	635			1920 493	202	24 225	226 626	227		
Acoustic Holography										
			1349	Acoustic Scatteri	ng					
					443 157	4 1735		1207	1128	
Acoustic Imaging				1731 1732	2 1733 173	34		2137		
		1736 1737		2233	2					
				ear and						
Acoustic Impedance	074		2018 1579	Acoustic Signatur					***	
300 781 362 1173	214		2010 1319	124					688	
Acoustic Insulation				Acoustic Techniq						
640				260 1351	128	34	456		1158	77
<b>OFO</b>				620			1736		1738	
Acoustic Liners									1968	
use Acoustic Lin	inge							1737		
			MIN.					1967		
stract				02-1287 1288-1487	1400 1700	1701 1001	1000	2124	2126.2	222
mbers: 1-198 199-395 39	6-550 551-7	10 711-902	903-1101 11	02-128/ 1288-148/	1400-1700	1701-100/	1000	2124	- 120-2	.20/
ume 11										

100

Acoustic Transmission 1822			SHE BI	Air Blast 40	193			436			
A								1126			
Acoustic Waves 443				Airborne Eq	wipment Re	monae					
						154		76			
Acoustical Data	Dete										
use Experimenta	I Data			Air Compres	seors ompressors						
Active Control	4000		Aug d								
850 841 1082 313 1842 1843	1906		1439	Air Conditio	oning Equipn	nent		1676		808	
Active Damping											
serve pamping	145			Aircraft							
				150 51	152 1443	844	155	76	147	68	34
Active Flutter Control				510 651	512 1633		175	156	157	148	
512	354	507		850 1311	652 2063			266	267	508	
				1630 1441 1531	922	1634 2064	1625	346 1036	397 507	0.000	162
Active Isolation 1440 1622 1623	1995			1631		2004				1038	
1440 1622 1623 2062 2243	1225			2071	7.7.7					1628	100
2002 2240					1632			The state of the s	1717		
Adhesives								1626	1727		
		93	8					1716 1846	1847		
Aerodynamic Characterist	ina							1040			
2121	1695	447 50	R	Aircraft Eng	ines						
	2070	1717			542		775		2157	268	199
				2101					2167		-
Aerodynamic Excitation										1708	
		2067									
				Aircraft Equ	ipment						
Aerodynamic Loads	844 945 1796	1407 44	B 1639						267		14
	2224 1485 1916		8 1699	Aircraft Lan	ding Areas						
2260 1441 1543		172		Ancient Dan	213					258	
1631 1763		222	8								
2001				Aircraft Nois	se e						
				1430 521	782 343		345	146	727	348	15
Aerodynamic Response	O			551	842 1113	1774	865	866	737	648	20
use Aerodynamic	STADUITY				1112 1343			1636	847	668	52
Aeroelasticity							2005	2066 2246	857 1227	1228	849
880	446	70	8 769						1297	1200	105
	1156	historyal sh	1729						1637		122
	2106										129
Agricultural Machinery				Aircraft Res	ponse						
2001 Tex Mills	1686	467 106	В	711101011 1001	Ponse			176			
Air Bags (Safety Restraint	Systems)			Aircraft Seat	Belts						
1272	1275			351							
stract .											
mbers: 1-198 199-395 396	8-550 551-710 711	902 903-	1101 110	2-1287 1288-14	87 1488-170	00 170	1-1887	1888	-2124	2125-	2287
ume 11											
unie i i											

Aircraft Seats 351	153							Anisotropic Pr	operties nisotropy			
Aircraft Tires								Anisotropy				
140								линостору	2033	1104		
46									2223			
Aircraft Vibration									Anna .			
1971		1964					2069	Antennas				
								1790		705	1066	1318 89
Aircraft Wings												
462	653	654	155	846	2067		1969	Anthropomorp				
	923	924		1156		1638		351	1063	1274		
	1843					1728						
		1844				2068		Antifriction Be	earings			0170
			2245					2200				2178 2208
Air Cooking I andi	0											2200
Air Cushion Landin		1634						Approximate N	Mathoda			
		1034							pproximati	on Method		
Airfoils									PP.OZ.	oncenou		
1520 61	1763	294	945	1796	437		769	Approximation	Methods			
		1444						711		1194		
		2224						1381				
Airframes								Arches				
				1636		1728		2010 1121		304	326	
Airport Noise								Armored Vehic	cles			
use Airpo	rts										2276	
Airports								Articulated Ve	hicles			
	213		1305		737			1461	2103	2105	2277	
								1471				
Algorithms												
	3			1806			909	Asymmetry				
			915					461 1881		515	Evolust-E-	160
Alienine								1001				
Aligning				1456				Asymptotic Ap	nnrovimetic	\n		
				1400				111	pproximate		127	
Alignment											-	
	1383		995		2207	978		Attitude Conti	rol Systems			
2240 2222								21				
Amplifiers								Automated Te	sting			
72									2183			
Analog Simulation	1463							Automated Tra	ansportatio	n Systems 174		
Angular Vibration		1704		76			700	Automatic Con	ntrol	005		
		1794		10			709			935	W 6215	
								(Fail)		103		
ostract						000 11			1400			0405 0005
umbers: 1-198 199-3	95 390	6-550	551-71	0 711	902	903-11	01 1	102-1287 1288-1487	1488-1700	1701-188	7 1888-2124	2125-2287
olume 11												

Automobile No					1217			Beam- 1810	Plate :	Systen	76					2028	
								1010								2020	
lutomobiles																	
	92 1093		- 100		177	178	179	Beams 90	91	92	93	84	205	86	07	00	
	92	694		1996	407		249	280	281	982	573	114			87 217	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	18
20	52			2056			1219	790	100000	1182	643	594	595		597		27
	-4 D-14-							980	TOTAL TOTAL	1362	14 5 15	1184		100000000000000000000000000000000000000	787		59
Lutomobile Se	at Deits				1087			1030		1552	( ) ( ) ( ) ( ) ( ) ( )	-	A CONTRACTOR		1077		78
					1007			1180	981	1782	1553	1554	1365	936	1357	908	97
utomobile Ti								1360	1181		1783	1754	1555	1366	1367	1178	117
					1217			1550	1361		1853	1784	1785	1786	1617	1358	154
								1710	1551				100000000000000000000000000000000000000	-	The state of the	1988	204
lutomotive Tr	ansmissio	n										2194	1985	1986	2237		
4	72																
								Beams	-Colu	mns							
Axial Excitatio											243					1368	
	93																
xial Force								Bearin	gs								
				786				1340	•	1342	463	1564	1515	796	877	98	136
				1206				1370	1371	1622	1623	1794	1795	2206	1177	1188	77.00
								2200	2201	2202	1793	2204	2205		2207	2178	219
Axisymmetric											2123					2208	
1611 20	42 1393	824	2045			818	1609				2203						
							2029										
								Belt C	onvey	ors							
																1868	
			B -														
and at								Belt D	rives								
Baffles								1100									
1380					237			Belts (	Marria	-\							
Relensing								Delta (	WIOV III	8)		1994					
Balancing use Balar	oing Tec	hnione										.,,,					
use Data	cuig rec	mique						Bernou	alli-Ev	ler Me	thod						
Balancing Mach	ines									982	573		1985				
			215							1182	643						
Balancing Tech	niques							Bibliog	raphi	es							
530 1951 19				1546		1768	1909		211	12	13	404	405	406		1498	40
950 2161 21	62	2164	2165	2166	The same of the same of		1949	920	411		1913	1914	1915	1916	1717	1718	919
					2167				721	722							
								D:	·								
Ball Bearings	1000			000	000=	000	900	Bioeng	meeri 161	ng	513						
	1353 1563		955	2206	2207	288			101		313						
	2203					988 1188		Bird St	rikes								
	2200					1100										48	
lars																-	
- COO THE	92 953	64					1779	Blade I	LOSS T	vnami	ics						
		284					1989			182						798	
tract		101111															-
nbers: 1-198 1	99-395 3	96-550	551-71	10 711	902	903-1	101 110	2-1287 1	288-14	87 14	88-170	0 170	1-1887	1888	-2124	2125-2	287
										114.18							
me 11																	

1073 and Graph Techi chnique 1583 1684 9-395 396-550	18 nigue	146	27	279 1709	Buckli Buildir Buildir	751 851 1041 1231 101 101 101 108 8411 591 721 901	722 852 1642 1642 0ck Ap 412 722 1232 1852	993 proach 1123 1113 1233 1863 2013	1124 164 164 564 1234 1854	515 855 1115 1235	16 566 1126 1216 1236	97 517 707 857 1237	2028 158 518 658 858	159 519 659 1059
nd Graph Techi chnique	18 nigue	146	Aleccie Plus		Buildi Buildi 660 1140 1650	751 851 1041 1231 ng 101 ng Blo	722 852 1642 nek Ap 412 722 1232	993 proach 1123 1113 1233 1863	1644 2194 1124 164 564 1234	515 855 1115	16 566 1126 1216	97 517 707 857	2028 158 518 658	159 519 659
nd Graph Techi chnique	18 nigue	146	Aleccie Plus		Buildin Buildin 660 1140	751 851 1041 1231 ng 101 ng Blo	722 852 1642 sek Ap 412 722	993 proach 1123	1644 2194 1124 164 564	515 855	16 566 1126	97 517 707	2028 158 518	159 519
nd Graph Techi chnique	18 nigue	146	Aleccie Plus		Buildi Buildi Buildi 660	751 851 1041 1231 ng 101 ng Blo	722 852 1642 ock Ap	993 proach 1123	1644 2194 1124	515	16 566	97	2028	159
nd Graph Techi chnique	18 nigue	146	April 1989 Physical Indiana (1989)		Buckli Buildir Buildir	751 851 1041 1231 ng 101 ng Blo	722 852 1642 nek Ap	853 1643 993 proach 1123	1644 2194		1776	97	2028	
nd Graph Techi chnique	18 nigue	146	April 1989 Physical Indiana (1989)	270	Buckli Buildi	751 851 1041 1231 ng 101	722 852 1642	853 1643 993 proach	1644 2194		1776	2247		1209
nd Graph Techi	18	146	April 1989 Physical Indiana (1989)		Buckli	751 851 1041 1231 ng 101	722 852 1642	853 1643 993 proach	1644 2194		1776	2247		1209
65 H 80 80 80	18	146	April 1989 Physical Indiana (1989)		Buckli	751 851 1041 1231 ng 101	722 852 1642	853 1643 993 proach	1644 2194		1776	2247		1209
1073		146	April 1989 Physical Indiana (1989)			751 851 1041 1231	722 852	853 1643	1644	1043		2247		1209
1073		146	April 1989 Physical Indiana (1989)			751 851 1041 1231	722 852	853 1643	1644	1043		2247		1900
1073		146	April 1989 Physical Indiana (1989)			751 851 1041 1231	722 852	853	1644	1043			2220	
1073	14	146	April 1989 Physical Indiana (1989)			751 851 1041	722 852	853	1644	1045				
1073	14	146	April 1989 Physical Indiana (1989)			751 851 1041	722 852	853	1644	1045			2220	
1073	14		Arrest de			751	722	853	1644	1045			2220	
1073	14									1043			2220	
1073	14		16			721			854	1045	0.00	707		
1072	1.			1079	1230		412	423			2000			1099
		166 05	77 1909	1500			350	352	564	1505	696	627	700	1000
					D.1									
				1599			1472							
							852							
					y = 181 m s	9		1473						
593					Brakin	g Eff	ects							
										033				
1513					Braces					925				
A CONTRACTOR OF THE PARTY OF TH	245				164									
						2051								
						111								
				1509	Box T	ype S	tructu	res						
333	3	116		1029										
Structures							1642	623						
is recommended off	actuics.				Box B	eams								
THE RESERVE AND ADDRESS OF THE PARTY OF THE	nctures										1140			
<b>.</b>														
st Resistant Str	uctures				1490						100000			
Construction					1180			993	1154		2 -0 -0	1747	1828	1179
										795	206	1517	758	1109
	3	16			Bound	ary V	alue P	roblem	18					
				1329	Dound	ary L	ayer L	A CI (AC)	on 1444					
				1590	Round	amı I	awan E	- ait ati						
					1830	601				595		827	818	1829
	855	112	7	1239			onditio	on Effe	ects					
					eri w		2282							
			U12 - 128		Booste	r Roc	kets							
	Les Services and Market								104					
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Damage	Deflection Bound Technique
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Damage Prediction	Deicing Systems
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Dampers	Design Techniques
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	2261	1232	1483	1594	1999		1417	2008				2132							213
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		932		944	355			2248	1449	Liasto	nydro	dynam	ic Pro	perties				2208	
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mbers:	1-196	199-3	95 39	6-550	551-71	0 711	-902	903-11	01 110	2-1287 1	288-14	87 14	88-170	0 170	1-1887	1888	2124	2125-2	287
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Elastomers	1000 1000 00	Energy Methods					
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use Electric Power Plants		341			406 407		
Electric Power Plants		P N.					
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1503	107 2000	1621 1343 2271	3 504	505			53
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2070		Engine Roughness	3 544				
Electrical Machines		34.	, 344				
1503		Engine Vibration					
		2270 542				888	88
Electrodynamic Shakers		1572				303	-
271 1962	2188						
		Engines					
Electrohydraulic Shakers						1958	
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		<b>Environmental Effects</b>					
Electromagnetic Excitation			704		1507		58
1962							
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Electromagnetic Properties 1065			704				
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Electromagnetic Shielding		581 202	814	595	736		105
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Electronic Instrumentation		. 744	1764				
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		Equipment Response					
Energy Absorbers		2150		35		2088	
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THE REPORT OF THE PARTY.				2185			
Energy Absorption							
	336 337 498 499	Equivalent Linearization		d			
	1186 1837 1838 919	1701 1523		285			
2261 2053 2054	2057 1219						
P		Error Analysis					191
Energy Dissipation		2 203			77		57
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stract mbers: 1-198 199-395 396-550 551-71	0 711-902 903-1101 11	02-1287 1288-1487 1488-17	00 170	1-1887	1000 2124	2125	202
INCELS. 1-190 199-390 390-000 551-/1	0 /11-902 903-1101 11	UZ-1207 1200-1467 1488-17	00 1/0	1-106/	1888-2124	2125-	25/

52 302 Expansion Joints Experimental Data	25		960 1070		1752					528	529
Expansion Joints  Experimental Data										838	879
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Experimental Data											1259
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Explosion Effects					.,,,						1,0,
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200	Elem	ent Te	hniqu	e						Flexural Wa	ives				
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800	801	792	743		Towns of the Park	1446	1077	728	839						
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Flexil	ole Sha	afts								use	Fluid-Induc	ed Exci	itation		
								1548							
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Flexu	ral Re	sponse												117	
					825					64-11					
		2.2								Fluid Coup	lings	P.L			
	ral Sti	ffness										394			
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Frequenc	y Analyz	ers						Gas Bearing	,		464				98
1530	962										-00				70
Frequenc	y Domair							Gas Turbine 1071		les	2264	1435		2157	
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Frequenc	y Equation	n						Gear Boxes							
	2192							810	472			275	1246	877	
Frequenc	y Meters							Gear Coupli	ings						
				1975					1382						
Frequency 74		<b>s</b> e						Gear Drives		2123					
Frequenc	y Respon	se Me	thod					Gear Noise							
	1712					198 1108	1119	811			1584				
Friction								Gears 1910 811	682	613		305	2216	107	2218
	1292							2180 2011				1195		2217	
Friction E	Bearings							Geometric l	Effects					roje	
						2108		481	-		924	875	486	57	838
Friction I	amping	1463						811 821	792 2202	1413			976	307 1797	1998
								Girders							
Frozen Sc	oils 592									423				2247	
								Glass							
Fuel Flam	mability						1849				934				
								Gradient Me	thods						
Fuel Tank	<b>.</b>	2063					1849		162						
Fundame	ntal Frequ	uency						Graphic Me							
83		993		125	916			1220	1682				1886	1587	
stract mbers: 1-	198 199-3	95 3	96-550	551-71	0 711-90	02 903-1	101 110	2-1287 1288-14	487 1	488-170	0 170	1-1887	1888	-2124	2125-2287
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Grids (Beam Grids) 2193 1194		Hankel Tra	nsformation 952	on				
			702					
Cirilia Madia								
Grinding Machinery 1743	1838	Harbors						
1745	1030					186		
Ground Effect Machines		Hardened I	nstallation					
2102 1913 1914 1915 106				13	245 575			
Ground Motion					2135			
42 43 1934 855 1146	1858				2100			
1742 973		Hardened S						
1523		nardened 5		d Installat				
1943		use	nardene	I Installat	ions			
Carrad Charle			REL					
Ground Shock 1722 1985		Harmonic A						
1722 1985		1701				46		
Ground Vehicles		Harmonic B	Balance Me	thod				
210 431 852 1253 1114 2105 336 1277	179					1786		
1440 891 892 1724 1686	279							
2061 2272		Harmonic E						
Ground Vibration		800 931		03 2034		626 62		149
81		2280		23		1136 189	7	154
				53	1555			
Group Velocity			16					
763			19	45				
		Harmonic R	esponse					
Guard Rails		580 1021	442				598	59
2272 45 1276		1520	622					
C:-1			1132					
Guideways 532		U	,					
THE REAL PROPERTY OF THE PARTY		Harmonic W	aves	214		1816		
Guyed Structures				214		1010		
2	198	Head (Anate	omy)					
		630	10	63		1447		
Gyroscopes								
1807	679	Heat Exchar						
			1012				308	5
		1201					1808	
·H·		Haliaal Sanin	_					
		Helical Sprin	-Ra	124	1215			
Half-Space				134	1213			
953		Helicopter B	lades					
2253			Rotary W	ings				
Handbooks		Helicopter E	ingines					
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			To be	125			-00	
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	3-1101 1102	-1287 1288-14	87 1488-1	700 170	1-1887	1888-2124	2125-22	87
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Helicopter Noise							Highway Transportation	
	63 674		666	667		669	1222	
		1245		1247		1249		
	63 1054		1246		1248		Hitches	
	53 1244		2246				use Drawbars	
12	43 1454						white standar	
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Helicopter Rotors							1992	
A CONTRACTOR OF THE PARTY OF TH	83 234		356	667	548			
		1475	1056	797	798		Hate Contact to Made	
		2085					Hole-Containing Media 322	:
1111 1251	864 1064						322	
2111	1454						ANIA TARRETT ANIA MARIE	
2111	1404						Holographic Techniques	
							780 1545 1957 1828	173
Helicopter Seats							1610	
. 1	53							
							Honeycomb Structures	
Helicopter Vibration							115	
2081							Uambinana Day Tarkainan	
11 11 - A - V11 - A	P. C						Hopkinson Bar Technique	
Helicopter Vibration	Lilects	1055			1058		1175	
		1033			1030		Mosnitale 4 100 100	
U-V							Hospitals 918	
Helicopters 810 451 662 14	E2 054	1865	1056	1057	2250	69	710	
2260 661 1242 16						7 7400	Hovercraft	
741 2082	real matter at	2285	-	1000000	2210	2439	use Ground Effect Machines	
141 2002	2234	2200	2256	2201			use Ground Effect machines	
			2200				Human Head	
Helmholtz Resonator							use Head (Anctomy)	
reminionz resonator		25					and item (random))	
							Human Organs	
Hemispherical Shells							use Organs (Biological)	
					1828			
							Human Response	
High Frequencies							870 521 1062 1253 234 675 866 357 648	64
				1377			1060 871 1252 854 865 867 868	80
							1061 1244 1255 1058	103
High Frequency Reso	nance Te	chnique	e				1091 1254	105
				587	958		1241	10
				777				109
U:-L F	1000						Hunting Motion	
High Frequency Resp	onse 554						Hunting Motion 1081 1082 1873 696	
	334						1001 1002 1010	
High Speed Rotors							Hydraulic Equipment	
ingh opeca itotors			1566				501 502 523 254 2226 1097	
			1000				1962 374	
High Speed Transport	ation Sva	tems						
530 172							Hydraulic Presses	
690							142	
stract						State Contraction		
mbers: 1-198 199-395	396-550	551-71	10 711	-902	903-1	101 110	2-1287 1288-1487 1488-1700 1701-1887 1888-2124 2125-	220/

					Impact Te	Impac	t Tests					
Hydraulic Systems					Impact Te	ate.						
1693			1777		1010		1263 12	274 1175	1276			100
1883							1273					187
Hydraulic Valves							1743					
		996	387									
					Impedance							
Hydrodynamic Excitation					40 25	l				317		
2246 1192 703	445			B 1279								
	925		2268	3	Induction							
						882	21	74				
Hydroelectric Power Plants												
		1896	1698	•	Industrial							
Hydrostatic Excitation						22	503 13		506	807	1438	145
Hydrostatic Excitation			9000				843	425	1256			
			2088				1513					
Hyperbolic Parabolic Shells					Industrial 1	Voies						
122					use		rial Facil	ities and	Noise C		diam.	
					use	and dell		Lice and	VOISE O	cherat	HOII	
Hysteretic Damping					Inertial Fo	rces						
	34 835		1138	749	Alexander of	812	1	74	1196		1798	
1521 8	84 2015								2196			
1751												
					Inflatable S	structure						
								85				
	-1-											
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I D					use	Influen	ce Coeff	icient Me	thod			
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use Shock Absorber					minutate C	CIICE	it Metilo	875	876		698	
								1635	0.0		070	
Impact Load Prediction			48									
Impact Load Prediction			70		Infrasonic l	requenc	ies					
Impact Load Prediction												
							12	54	1966			
Impact Load Prediction Impact Noise				1459			12	54	1966			
				1459	Initial Defo	rmation		54	1966			
				1459		rmation	Effects	54 94	1966			
Impact Noise				1459		rmation	Effects		1966			
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Impact Noise Impact Pairs 1890 Impact Response (Mechanica				1459	Initial Defo	e Problei	Effects 4					
Impact Noise Impact Pairs 1890 Impact Response (Mechanica 1380 2231 2152 1653 198	34 45	46 1	847	689	Initial Defo Initial Valu	e Problei Bounda	Effects 4	94				
Impact Noise Impact Pairs 1890 Impact Response (Mechanica 1380 2231 2152 1653 196 1550 213	34 45 34	1026	847		Initial Defo	e Problei Bounda	Effects 4 ns nry Value	94 e Problem				
Impact Noise Impact Pairs 1890 Impact Response (Mechanica 1380 2231 2152 1653 196 1550 213	34 45 34		847	689	Initial Defo Initial Valu	e Problei Bounda	Effects 4	94 e Problem				
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Impact Noise  Impact Pairs 1890  Impact Response (Mechanica 1380 2231 2152 1653 196 1550 213 1650 1890 2230  Impact Shock 2053 205 205	34 45 34 34 2025 34 2055	1026 1086	47	689 1999	Initial Defo Initial Valuese Instruments Instruments use	e Probler Bounds ation Instrum Rail-Mo	Effects 4 ns ry Value 45	94 Problem		2124	2125-22	287

530	1462	1100000	1874			1077	1078		1470	782	863		695	Company of the Compan	1637	848	849
		1873		1875			1308							2246			
nteraction:	Rotor-	Stator		395					Interior Vil	bration							
nteraction:	Soil-Fe	nundat	ion											2246			
1660		2253	The second second					1659	Intermitten	t Motion	n						
			1664													1888	
Interaction:	Soil-St	ructur	es						Internal Co	mbustio	n Eng	ines					
1550 951	732	1	474			1157		1139	341							888	
1730 1651	952		1334		111111111111111111111111111111111111111		1528		T I.D.								
1661		1333		1005		1507	1948	1529	Internal Da 740	mping 1552	633				57		
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Interaction: 1 1281			undati	ion	386		1658		Internal Re	sonance				2126			
1201	1002	413			536		2078							2120			
									Isolation								
Interaction:	Tire-Pa	weme									2053	2054	2055				
1310			1474					1309	Isolators								
Interaction:	Vehicl	e-Guid	leway						2261		163	164	165	166			
	1872		•			2267	1268					2084	645				
	2102												2085				
Interaction:	Vehici	Stru	cture						Isotropy								
1041							1078				die.	1104		826		828	
1691																	
Interaction:	Vehicl	e.Terr	ain						Iteration						397		
interaction.	Venici		144												٠,,		
			224														
Interaction:	Wheel-	Pavem	ent										J.				
						1277											-
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Interface: So		iid 1203							570 1741			1224	345	646	347		
		1203							1930						727		
Interference	Respo	nse Sp	ectra												141		
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	605				1696		
	1195		Layered Damping				
	1565		,			788	
		di resimper	Layered Materials 250 251 942	323	1044		
	-K-		2030 1732	323	1946 8	758	-
			1.02		75		16
Knee (Anatomy)					78		
	655						
			Liapunov's Method				
			use Lyapun	ov Functions			
	.L.		Linear Analysis				
			use Linear	Theories			
Laminates							
use Layered Mate	erials		Linear Systems				
			430 1 1290 1901	3	1326 113	7	
Lamps			1290 1901				
32			Linear Theories				
Landing Fields			951				
use Aircraft Land	ling Areas						
	and recome		Linings				
Landing Gear			612			1838	4
403	1634	149	1452				80
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Landing Impact	Inches Charles		Linkages				
use Landing and	unpact Snock			313 814 585			221
Landing Shock				003 1004 1005			1
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Landing Simulation			use Fluid Fi	lled Containers			
use Landing and	Simulation		Liquids				
Laplace Transformation					104	7 2138	
952	1385	47 119			179	2100	
	2000	119	Longitudinal Respons				
Lasers			Toughtanian respons	634 155			
1950 1172	1775 1976			2224			
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ateral Response			Longitudinal Vibratio	n			
aterai Response 1262	1876	1997	1661		1626	1	1809
2252		123 <i>7</i> 1987	Low Francisco				
	ing.	Marie La Marie C	Low Frequencies 1430	2264		1770	
ateral Vibration				~204		1778	
2191	1815 1626	1368 1989	Lubrication				
	2226		680	1094 1515	2017	2208 2	2199
tract nbers: 1-198 199-395 396-	550 551,710 711	902 903-1101 110	02-1287 1288-1487 1488-	4700 4500			
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Lumped Mass Method use Lumped Pa	arameter Meth	od			Machine Tools 360 2091			2087	2	2089
					2090					
Lumped Parameter Met 552	1704 1985			1919	Machining					
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Luanun au'a Mathad					Magnetic Bearings					
Lyapunov's Method			38	8 1899	1622 1623	3				
					Magnetic Properties					
2102	- M -	at En								969
					Manifolds	2024				
Machine Diagnostics						2024				
use Diagnostic	Techniques				Manuals and Handbook	8				
Machine Drives					11	224				19
		20	087		Marine Engines					
Machine Elements							265			
	Components				W · D					
					Marine Propellers 291 373	3 374	405 1436	1177	9	2209
Machine Foundations		1056 1		0.1650	271 010	404	403 1430	1797	•	.20
2250 1581 1652 165	3 1054 1055	1656	57 165	2079						
		1000		20.7	Masonry					
Machine Noise					1232 1033	3			1748 1	049
use Machinery	Noise							1707		
Machinery					Mass Beam Systems					
Machinery	264	66	587 77	8 2189	1362				1	1359
		776								
		1456 2	177		Mass Coefficients 1690 903		1696			158
		2116			1070 700	10 176	1070			30
Machinery Components					Mass Matrices					
2050 2051		20	017 205	8	73	3				
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Machinery Foundations					Mass-Beam Systems 1551 792 783	3				
use Machine F	oundations				79:					
Machinery Noise										
1131	235	1676		1459	Mass-Spring Systems					
2021	425				882 793	•				
	975				Material Damping					
	1835				52 53	3 54	55 56	967		8
Machinery Vibration							785 966			939
2170 2262	874 1355	1676 20	087 97	8 1769	W					
	1044	1936	216	8	Materials Handling Equi	-	455 2086			
	1944				1992	1	4JJ 2000			
ostract imbers: 1-198 199-395	396-550 551-71	10 711-90	02 903	1101 11	02-1287 1288-1487 1488-17	700 1701-	1887 1886	8-2124	2125-22	287
olume 11										
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	ematic use		ematic	al Mod	lels					Mechanical Ad					1967		
Math	ematic	al Mad	ala							Mechanical Dr	rives						
220		42		134	15	366	7	8	499			394					
1030	161	162		1414		606	107	498		Mechanical El	emente						
1450	171			1474		856	577	708		2221	CINCILL			66			
1460	Contract Con			1944		876		1108						•			
1870	341	532		1994	100000	1226			2279	Mechanical Ex	citation						
2090	531	662	753		885	1466		1658		1961							
2130	581	732	953		1005		1447	1708									
	1101	1092	1053		1295		1467	1868		Mechanical Im	pedance						
	1111	1392	1073		1395		1707	1978		1	692 2113		1985	1056		2278	
	1141	1442	1093		1415		2077	2008									
	1281	1482	1193		1495			2078		Mechanical Pr	operties						
	1471	1662	2103		1905							404	55				
	1521	2272	2193		1985								405				
	1601				2065												
	1681				2095					Mechanical Re	eliability						
	1691				2125					use R	Reliability						
	2081				2145												
	2131									Mechanical Sy							
											962 1683				197		
Matri	x Meth										682				1257		
		552	1493	124			1347		859	2	222						
							1617										
						1346				Mechanical Te	elemetry						
										1700							
Maxir	num R	espon	se														
							1487			Mechanisms							
										1011	812	814	875		2127	678	212
Measu			ument									1684		876		1888	
	use	Meast	ıring İı	ıstrum	ents					Membranes							
Mass	ramar	t Took	niques							110	62		1015	616			
50	41	732	•	274	275	276	707	1778	889	1120	02		1013	010			
380	81	782		974		1966			009	1120							
450					1345			2100		Membranes (S	tructural N	lambar					
AUT CONC.	1131	10,2		1804	1040	2276	171.			Membranes (5	2223	iciimei		306			
1780	1101		1963	1001							2220		010	1386			
2130			1,00											1000			
										Metal Working							
Measu	ring L	strum	entatio	on						681	•				1067		
	use		iring Ir		ents					001					100.		
			•							Method of Cha	aracteristic						
Measu	ring I	strum	ents								1523						
	961			964	275	1166	797	2188	1539								
900	1131	1172	1343	1344		1966			2179	Method of Har	rmonic Bal	ance					
1540	1171	1802	1773		1775		1917		2189			1				1908	
1770			1963				2187										
										Method of Init	tial Function	ons					
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		, 199-	38	J-000	331-71	5 /11	302	203-1		2-1207 1200-1407	1400-170	0 1/0	1-100/	1000	2124	2120-2	207
olume 1	1																

Military Vehicles													206		218	
501							Mode	Shape	.5							
							1360	121	712		1874	115	826	797	148	
Mindlin Theory								681	862	823		2285		-	1208	1109
		625	126						1402					1407	1408	
								1381	1562					1447		
Mines (Excavations)									1642					1557		
1462	1	745	576			1239			1782							
						1509			2042							
M: 1 W.:.LAD:							W. J.	T4								
Minimum Weight Design	1044 1	1015			550		Modal		ng 1512	1049		905	1996	1647	848	1650
1560 911 602	1844	1215	6		558 1358				1512	1693		893	1330		2068	103
					1300		1230	1911		2073				1001	2000	
Missile Silos										2015						
2080							Modal	Tests								
								use		l Testi	ng					
Missiles																
	704	1695	156	187	188		Modul	us of	Elastic	ity						
	- 1	1725	166		358					583					2058	
Modal Analysis	1004	100	100	015	70	70	Moiré	Litec	ts		004				1940	
	1924	105	176	217	78	79					934				1348	
350 741 1822 1923		435	356		1578 2038	219	M	Carl	. W.al.							
990 901 1922 1800 951		735 1095	376 836		2248	1499	1320		Metho	Da						
1800 951 2120 1951		1125	030	1307	2440		1520	091								
2120 1931		1120		100.			Moori	nøe								
Modal Damping							500	-6-								
	1874			1897												
							Motor	cycle								
<b>Modal Minimization Meth</b>	od								302							
1140									382							
Modal Models		Fun	Liver				Motor	Vehi	cle Eng	gines						
		15	16													146
Modal Superposition Met				1055	410			Vehi	cle Noi		1114			1140		
1401 1482	104			1857	418		1470		1252	1713	1114			1147		

Motor Vehicles			400	40=			Natura					,,,,	TO STATE OF	105	10	
			406	407			20	1	602	113	514	115	6	127	18	559
			1916				830	131	712	283	624	125	826	297	148	979
							910	281	822	433	794	525	916	987	- promote control	1779
Motors				10/5			1020	801	862		1394					2029
	1044			1867			1360				1654		1890			
											1714	2285			1818	
Mountings								1501	1562	1633				100000	1918	
				1867			1810		1642		1924				2028	
							2010		1782		2194			1807		
Moving Loads			2222						2042		2234			2027		
250 851 1182 633		1415												2047		
1041	1644		2196											2237		
1691	2104															
							Naval	Ships								
Moving Strips														617		
		415														
		1995					Noise									
							2060	2241	22	23	24					205
Mufflers									342	843						
340									THE REAL PROPERTY.	1033						
									2242	1423						
Multi-Beam Systems																
1360							Noise	Contr	lo							
								use	Noise	Redu	ction					
Multidegree of Freedom	System	18														
240 901 1702 1923		875	876		1238	1889	Noise	Gene	ration							
1701		1495		1897			100	231						1687	298	
							160	681	1372	1243	294	425	1116		338	29
Multiple Resonance							170	1061		1683	234	545	2096		368	33
				197			210	1841		2093	404	665			1078	87
							230				664	1745				122
Multistory Buildings							290				1164					123
1030 1451 1042 1043		145	516	657	638	1859	530				1874					145
1450 1871 1853		1855	856	1857	1238		650				2124					
1850			1646		1648		690				2264					
					1858		730									
					2248		930									
Musical Instruments							Noise	Meas	ureme	at						
550			196	57	198		570	671	892	343	24	975	146	847	168	
				197			1050	1171	1052	2073	344	1305	676	1217	1298	
								1741	2072		1514	1845	1636	1227		
								1911			1774		2186	1717		
														2097		
		N-														
							Noise	Mete	rs							
Nacelles								use	Soun	d Leve	el Mete	rs				
371																
							Noise	Predi	ction							
NASTRAN (Computer P	moren	na)					730	541	1372		1134	665	666	737	348	66
740 741 742 123	-	and the same	1006		738	739	- 1	1431	2142				806	1247		
743		1 770	1,,0		.00	1729		1841								
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olume 11																

Nonlir 2030		espons	e	1004			137 2027	908	1019	Nuclea	r Read	ctors							187
Nonlin	near D	912				36				Nuclea	r Rea	ctor Co	ontain 143	ment			1827	2268	
			near T	heorie	2-1694									1464	1085 1685				
		nalysis												804	535	536	1827		
		1002					1,01	1100				422		534	315	526	887		16
1000	1001	1352	. 13	074	1919			1158	1119	Nuclea									
	1351		773	200	1315		267		1779									2,0	
1000000		ive Te		774	455		67	258	269	- ucica		Sicu S	he	424				498	4
N		T								Nuclea	r Pow	ered S	hip:						
	use	Nond	estruct	ive Te	sts											1936			
Nonde	estruct	ive Te	sting														2197	1688	
														1084	1465				
	9 P.	-			55	56									1085			1338	22
Nomo	graph													804	885	536	537	618	15
	use	Sound	Trans	missio	on					2020		,02	000	534	565	376	497		
20000		nission								Nuclea 1260	r row		533	364	175	176	377	378	3
										Nuclea	- D	or Di							
		1252		234	1255						1721	42	43		245	1126			
Noise	Tolera	nce								Nuclea	r Exp	losion							
								1458							2133				
								1248		1510		1942			1725 2135	1146			
370		1502	1053	864			167		1259		2101			1144	1145	436			
Noise	Source		tificati							Nuclea	- Table 1007 Co.		Effect						
						2280										_00			
						2266 2286			2099	570				1224		236	347		5
						2066			2059	Nozzle									
							2007		1719		2141								
2100					2105	1686	1637		1429		201					1306	2027		
2050						1436		The contract of		610		2192	1893		2195	276	987	698	:
1840	100 D. T.			2009		1256				Norma	d Mod	les							
1430			1433		1425 1435			1438										1370	-
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Railroad To									Record	ing Ir	atrım	onto						
171		883		2095	1876	1077		1079	Iccord	mg n	ibtium	CIILD		1965				116
														1,00				
Railroad To	rains								Rectan	gular	Bars							
690 1041						2097		2099			2192			795				
1080 1461																		
2100									Rectan	gular	Memb	ranes						
F 8018												2223		1385				
Railroad To																		
use	Kail T	ranspo	ortatio	n					Rectan		Panels							
Railroad V	shieles									111							2018	
namroau v		ad Tra	ine						D		D							
usc	reamic	au 110							Rectan 130	•	832	323	904	1605	126	127	128	12
Rails									830		1812	The State of		2035	486	827	628	82
use	Railro	ad Tra	cks						1400	001	1012	Ser Washington	1604	2000	826	837	828	-
												-000	2034			1407		130
Railway Ve	hicles															1957		
use	Railro	ad Tra	ins													2037		
Railway Wi	reels								Reduct	ion M	lethod	8						
			1874										554				1918	
D J F.													1714					
Random Ex 240 431		873	784	825	26	1217	220	920										
900 781		1013	884	885	66	1317	238 1318	239 429	Re-enti		hicles							
1970		1293	004	1935	766		1608	749	900 2	121								18
2280		1270		1995			1000	. 47	Regula	ions								
					2056				210		1112	863	1114	2105				20
									720		1912							
Random Pa	ramete	rs																
750			64						Reinfo	rced (	Concre	te						
									1850		122	243	1234	1235		37	138	53
Random R									2210			1043		2215	436	497		187
1330 951						1137	1138	429			1582	1103			1236	517		
stract											9117			THE STATE OF				
mbers: 1-19	8 199-3	95 39	6-550	551-71	0 711	-902	903-11	01 110	2-1287 12	88-14	87 14	88-170	0 170	1-1887	1888	-2124	2125-2	2287
ume 11																		

Reinforced Concrete (Contin	ued)	- ACTION		Reverberation	on Cha							
1233		1616 1027				73	74					
1373		1776		Reviews								
1853				730 1121	212	919	014	015	016	015	400	
Dainfanna I Denam						213				217	-	
Reinforced Plates				1120 1301	402	403	414	415	416	417	-	111
10:	24			1300 1921		413	724	725	726	727		129
Reinforced Structures				1920	1302			1715	1116			191
			638		2132	1303	2134		1716	1917	1918	
			030			2133					2128	
Reliability				Dibe (Sumo								
1110			400	Ribs (Suppo	2232							
1110			429		2232							
				D:1 D								
Remote Control				Ride Dynam								
			1709	1090 1091	1082	693	694	1915			1878	107
					1092	893	1724					
Resonance Bar Techniques						1093	1914					
961 772 1613	1765	56	2079			1253						
						1913						
Resonance Equalization Tech	nique					2083						
	1375											
				Rigid Found	ations							
Resonance Pass Through						1663	1664					
135	4					1000	1001					
136				Rings								
The state of the s				1720 1421	129	133			326		9099	000
Resonance Tests				1720 1421	132	833					2028	
icesonance Tests			1418						1416			2029
			1410			1213						2119
Passant Day Trabailan												
Resonant Bar Technique				Ritz Method								
use Resonance Bar 1	ecnnique										128	
Resonant Cavities				Road Rough	ness							
use Cavity Resonato	rs .			180 181		383	694					
The state of the s				380		693						
Resonant Frequencies												
121 832	525	197	748	Roads (Paver	nents)							
251 1322	785	2217		381			2104					
1661 1702												
2082				Road Tests (	Ride D	vnam	ics)					
					Ride D	•						
Resonant Response					L	yman						
The second secon	4 1375	186 1207	408	Rock (Soil)								
2223		100 1201	100	record (SOII)								
												949
Resonators				0.4								
				Rods								
31				30		1183		985		47		
)				1800			984			97		
Response Spectra				1990						557		
1863 53	4		618									
				Roller Bearin	gs							
Retaining Walls							2204	955				
			1618					2205				
tract												_
ract ibers: 1-198 199-395 396-550	551.710	711.902	903-1101 1	102-1287 1288-148	7 140	8-1700	170	1-1887	1000	124	2125 2	207
	551-710	711-002		102-120/ 1200-148	, 148	0-1700	170	1-106/	1000-2	124	2125-2	26/
ime 11												

Roller Coaster				100-			Rotors (Mac	1692 2113		SAF	1096	697	408	43
				1287			880 1261			70 30 201	1116	-	-	
Rolling Contact Page							1480 1881			7 7 2 2 4				
Rolling Contact Bearings							1700 1951				1476	100000		
use Antifriction	Bear	ngs					2110 2161						1798	
Dalling Printer							2110 2101	2102	2164	2103	2100	2107	2278	
Rolling Friction 2012									2104					19
2012					2208									19
Roofs														21
410 641						400								22
410 041			496			409	Rubber							
Potem Inantia Effect							use	Elastomers						
Rotary Inertia Effects							usc	Liastomers						
use Rotatory In	ertia E	litects					Rubber Bear	-i						
D.4 C 1.							rempher Dear	ungs			1006			
Rotary Seals 700	1004										1996			
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Rotary Wings		1/					North A	Q THE ST OF	0 4	s.		77		
650 991 862 1243	674	1675								2.	14 14			
2260 1251			1056											
				797	2 500		Safety Belts							
				1997				Seat Belts						
Datating Came							-							
Rotating Structures 700 372 2183	954													
	264					1339	Safety Devic	es						
1610 1212	984				1118							1287		
Rotation							Safety Restra							
321							351	1272 1273	1274				248	
D-4-4 I T-66														
Rotatory Inertia Effects 980 91 92 93	004	1000	100			455	Sand							
980 91 92 93 1550 982 1403		1365	-	217		459			1524		1766	1927		
The second secon	484		486		1208			1980						
2032 1553			1016				Sandwich La							
1603			1366				use	Sandwich St	ructure	:8				
	1814		1986											
			2046				Sandwich Par							
Datas Danis C.							use	Panels or Sar	ndwich	Struct	tures			
Rotor-Bearing Systems	0114	100=					The sale as	0.00						
	2114	1095		697		2179	Sandwich Str							
				1177			790	2032 283		595			938	48
				1477	2108									181
Rotor Blades							048.5	1. WHAT P						
290 1571					1000	1100	SAP (Compu		)			H Ti		
990 2001					1798	1189	420	123				17		
770 4001							0							
Rotor Blades (Rotary Win							Satellite Ante							
use Rotary Wing							use S	Spacecraft A	ntenna					
use notary wings	10 74						0							
Rotor-Induced Vibration							Saws			. with				
	1064	900-	1000				100		1324	415		1457	1458	
	1004	2085	1020	4-17-1										
stract													1000	_
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mbers: 1-198 199-395 396	6-550	551-71	0 711	-902	903-11	01 110	02-1287 1288-148	37 1488-170	0 1701	-1887	1888-	2124	2125-2	267
nbers: 1-198 199-395 390 ume 11	6-550	551-71	0 711	-902	903-11	101 110	D2-1287 1288-146	97 1488-170	0 1701	1-1887	1888-	2124	2125-2	267

	Scalin	g									Seismi	ic Wav	res							
		•	1512	683	1504			747										2147	2148	949
	170			973																2149
	340										Seismo	omete	rs.							
	2190										1540	Jame ve	•							
	Seals	(Stop)	pers)										****							
	2240			2003	1094	995			2238	2239	Self-E	4				9115	104	207	1110	600
											340	2211	1004	1883		2115	196 996	307	1118	699
	Seat I	Belts															1516			
			1272	1063													2116			
				1143							0									
	Sanor	dary \	Wayaa								Semiti	rauers		1473						1089
	Secon	1161											1412	1475						100
		1101									Shaft	Coupl	ings							
	Seism	ic Des	ign									P		1383						
	1670	571	732	1233	1234	565	526	377	478	1199										
	1680	731	752	1373	1594	645	1506	537	538	1649	Shafts									
	1860				1854	-	1856	917		1859	1530	701		783	1354	1355	686	277	278	459
			1592			1115		77.00	1448			1781		2123			976	457	458	
		G-PROFESTO	1852			1235			1468			1881						1177		
			1862			1465			1508			2191					1546	1547		
		2261				1595		1977										1767		
	Saiem	ic Det	ection								Shafts	(Man	hine F	lemen	tel					
	CIBILI	ik Det	CCHOIL				2146	2147	2148	2149	1980						1956	977	978	
												2161		1353				21	1978	
	Seism	ic Exc	itation											1983					2108	
	710	1751	952	953	444	435	36	37	1198	539										
	1030		1042	973	1664	1045	136	117	1558	1049	Shaker	rs								
	1620				1934		256		1698		70	71	72		1534		1176		548	
	2080		2122		2284	1935	816	947		1599	1450						1336			
	2280			1923			Colorado actividado.	1487			CI II	CI								
							1086				Shallo		Шв							
	Seigm	ic Isol	etion									331								
	LI FORMAL	1681									Shear	Defor	matio	Effec	ets					
											J.1.C.1			1393		2035				
	Seism	ic Res	ponse																	
	480	411		123	454	315	386	377	418	379	Shear	Stren	gth							
	1140	621			534	835		1197		449						1525				
	1200	751	412		1204	1595				479	Shear	Vibra	tion							
	1230	901	622			No francisco San	1506			1139	450									709
			1232				1596				CL -II									.0,
			1672			2235	1616	1667 2197			Shells	101	400	100		110	200			
	2130			1523			1666	2191		1739	630 1830		422 632	417700000	624	115 325	326 416	57	To the same	489
		1001	1,02	1813			1936			2079	2040						410	327 1827		1829
				-525			-,00			2269				1393				2047		
														1613					1020	
	Seism	ic Res	ponse	Spectr										1823						
						515			1858	719				1833						
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	bstract		241.00		22															
N	umbers	1-19	8 199-	395 3	96-550	551-7	10 71	-902	903-1	101 11	02-1287 1	288-14	187 1	488-170	00 17	01-1887	1888	3-2124	2125-	2287
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stract		550 551-710		903-1101 110	02-1287 1288-1487 1488-1		1-1887	1888			287
Shock Tube	2022				Sliding Friction 2012	1854					
Shock Tests 1341	453	22	76		Slider Bearings	2114					
								400			
2120					Sicoro Dominigo			466			
Shock Respo	onse Spectra				Sleeve Bearings						
oll. D					Mar Cara Tara	184					
1920 121		175 14	76 577		Slamming						
Shock Respo	onse							1500			
				1339	Slabs			1506			
451				2178 69	0.1						
Shock Pulse	Method										2209
use	Measurement T	Techniques and	d Shock I	Response	Skew Plates 1410	484		1406		2038	139
Shock Meas											
use	Shock Excitation	on			0	3 1504		1836			
Shock Load					Single Degree of Freed	om System	ms				
			1627			1934	1745	2136			
30			1487		431	1144		7707070			
Shock Excit	ation				1850 271 1872	454	435	1146	1257	498	170
1720	1002 1100 1		331	300 1009	Simulation						
Shock Abso 1420	rbers 1032 1753 1	144	337	358 1839	use Missile Sil	OB				14 300	
CL L AL					Silos (Missile)						
		895									
		445		1278	2061		1425	1426			
1481	1192 1	184 185 385	2117	208 468	Silencers						
Ships	1100 1	104 105	0115	200					2177		1769
					Signatures						
		185									
Ship Rolling					Signal Processing Tech	uques			1737		
	683 20	794 10	66 247	358	Signal Propagains Tool	nimes					
Shipping Co		12: 14:									2119
					Shuttles (Spacecraft)						
	0.2		677								
onip Structu	ral Components 642		337		2151 2022	754	1 (45	246	1127	1938	39
N					Shock Waves	~~.	274-	046		1020	
		143	36								
Ship Noise					2151		RE			1	
				.,,	1721	1744	2000			438	
omp nuus	4	124		498 499	1321 60		755		437	38	
Ship Hulls					Shock Wave Propagation						
					2101 33						

Sloehing 491 1762 6	63 2284		Sound Measure		1004	1066		-
	33 2204			1713	1804	1966		17
Sluice Gates	12	387	Sound Pressure	Lamela				
		387	Sound Pressure	Levels				338
Snap Through Problem								,,,,
1121	304		C1 D					
Soils			Sound Pressure 820	8	525	1106		17
	23 1524 1525 152		020		333	1100		17
1671 732	1534 192	26						
772	1544		Sound Propagat					
1522			1740 301 1301	233	104 1575 2214 1805			218 9
Solar Cells			1301	1133	2005	1370		198 138
	125			1100	2003		-	30
Solid Propellant Rocke	at Engines		Sound Reflection					
	93		Sound Reflection	OII	2214			
Solid Rocket Propellar	ats		Sound Transmi	ssion				
		2119	1130 471 29	92 23	895	1376	417 8	808 4
			1131		1395		2007 8	48
Sonar Arrays			1601					
872			2021					
Sonar Equipment			Sound Transmir	esion Loss				
971 972		967	Sound Haiseill	BOIOII LIUBE		1426		8
		,0.			***	1120		
Sonar Transducers			Sound Waves					
970	96	66 968 969	770 611 2	32	2214 105	926	427 4	28
			2140 771		1345	2006	927	5
Sonic Boom	213	6 07 1710 1400	1331				1367	6
	213	36 27 1718 1429 867						13
		1717	Spacecraft					
			390 21		1694 225	226	227 3	88 3
Sound Analyzers			2120 191		1884	1486		8
1891			391					
			1491					
Sound Attenuation 1760 612		140	1531					
1760 612		469	C 0 F					
Sound Generation			Spacecraft Equi	pment Re	esponse			28
370	724 2025	2137 1928 1329	170				-	20
1160			Space Shuttles					
			1	92	1034 1035	1036	1037 10	98
Sound Insulation					1884 1485			
use Acoustic I	nsulation							
Sound Level Meters			Spectral Analysi					
Country Devel Metels	1344 1535 153	36 77 1168	use Spe	ectrum Ar	nalysis			
	1000 100	1167	Spectral Energy	Distribut	ion Technic	ıe		
		1537	129		434			
	396-550 551-710 7	711-902 903-1101 11	02-1287 1288-1487	1488-170	00 1701-188	7 1888-	2124 21	25-228
bstract umbers: 1-198 199-395 olume 11 sue: 1 2	396-550 551-710 7	711-902 903-1101 11 5 6	7 8	1488-170	10	7 1888-		21

473	504			618		1910 1911		1713	564		300	1777	2210	
pectrum Analyzers						Standards	and C	odes						
270										565	1266	917	208	51
770										1115		1297	1298	190
pheres														
940		926	927			Statistical .								
								2 1543		225		1997	1238	23
pherical Shells							100	2 2183	•					175
490 331 332 1 1121 1392	614		1207				193							172
						Statistical	Energ	v Metho	ods					
piral Vibrations						640	- Barre	,	1294			617		
			457									2007		
pring Constants														
	64			1878		Stators								
										525				
pring-Mass Systems						Steady Sta	to Fr	aitation						
use Mass-Spring S	ystems					use			citation					
prings														
	1214					Steady-Sta use		sponse iodic Re	esponse					
Springs (Elastic)														
1421 2053		1096				Steam Ger use		rs ilers						
squeeze Film Bearings														
		606		1478		Steam Har 170	mmer							
squeeze Film Dampers						110								
182			2157			Steam Tur	bines							
								72 43	894			367		
Stability								2093	3			687		
290 1471 1452 1903	174 1475	106	2107		1369									
1901 2102	1695	786		1898		Steels								
1931	1705			2238				22				1757		
		1706					104	72						
		2106					104							
Stability Analysis						Steepest D	Descen	t Metho	d					
use Stability						51	1							
Stability Methods						Steering G	ear							
Amount Medicals			717								1276	-		
Stabilization						Stick-Slip	Reary	onee						
651 1463						680		32		2145				
Stabilizers (Fluid Dynamic 1633	ce)					Stiffened 1830	Shells							18:
strect mbers: 1-198 199-395 391	8-550 551-7	10 711	-902	903-1	101 110	2-1287 1288	-1487	1488-1	700 170	01-188	188	8-2124	2125	-228
100 100 300 300							010000							

Stiffened Stru	ctures							Structural F	Response						
851								40		1174		136	1487	1418	
								1330		1934					
Stiffening															
2	232						329	Structural S							
								1581	712				1587	678	
Stiffness									2212					1588	198
321	1633	1324			397										
								STRUDL (C	Computer Pro	gram)					
Stiffness Coef	ficients								853						
90 481	733		465		1047	98									
700 1791	903			1696	2077			Subharmon	ic Oscillation						
	1793	1214							1353			96			
Stiffness Meth	rods							Submerged	Structures						
			1095		17			330	1612 493	944	115		1127	1408	32
										1154			1207	1688	
Stochastic Pro 10 531	172 1293		1495		= 7.7	1238	749	Substance	o Courtin						
560 1291			2125		511	1238	1109	Substructur use	Component	Mada 9	Synthe	oi.			
	292		2123				1107	use	Component	Mode	ynaic	919			
								Subway Rai	ilwavs						
Stone Buildin	gs gs								1462						
1861 1	862														
								Supernarmo	onic Vibration	1					
Storage Tank												286			
710		524 944		946				C	A:						
		944						Supersonic	Aircraft				1627	1228	
Strings													1727	1220	
550	413		95	96	197										
600			2195	286				Supersonic	Vibrations						
				986				1520							
				1186											
C								Supports 880 1581	210 1012			1006		1900	160
Structural Dec 910 911 1								880 1981	312 1813			1776		1388 1528	108
910 911 1	1042													1320	
Structural Co	mponents							Surface Rou	ughness						
	tructural	Member	rs						532 1093						
									1092 2203						
Structural Ele	ements														
use S	Structural	Member	rs					Surveys							
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Structural Me			125	111	215	==0	400	C	C4						
810 901 1030 2051 1		564 1834		416 636		558 638	429 639	Suspended :	Structures			496			
1030 2051 1 1620	142	1034	100000	836			709					490			
2050			000			1718		Suspension	Bridges						
				1126	Marits.	1 1 1	134	1040 951		354					
				2236				1640 1641		514					
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Suspension System 1440 531 162	383 1914 1065 1913 1225 1 2083 1285 edings	166 696 1677 1066	1079	Test Instrumentation use Test Equipm  Test Models 732  Test Stands 1960  Testing Apparatus	756 1507 1098
1440 531 162 1461 212 2062 Switches Symposia use Proces Synchronous Motor System Identificat 10 1712 1110 1922	383 1914 1065 1913 1225 1 2083 1285 edings edings 613	1066	1079	use Test Equipm Test Models 732 Test Stands 1960	756 1507 1098
1440 531 162 1461 212 2062 Switches Symposia use Proces Synchronous Motor System Identificat 10 1712 1110 1922	383 1914 1065 1913 1225 1 2083 1285 edings edings 613	1066	1079	use Test Equipm Test Models 732 Test Stands 1960	756 1507 1098
Symposia use Proce Synchronous Moto System Identificat 10 1712 1110 1922	2083 1285 edings ors 613 ion Technique	2000 C		Test Models 732 Test Stands 1960	756 1507 1098
Symposia use Proces Synchronous Moto System Identificat 10 1712 1110 1922	1285 edings ors 613 ion Technique	586		732 Test Stands 1960	
Symposia use Proces Synchronous Moto System Identificat 10 1712 1110 1922	edings ers 613 ion Technique	586		732 Test Stands 1960	
Symposia use Proces Synchronous Moto System Identificat 10 1712 1110 1922	edings ers 613 ion Technique	586		Test Stands 1960	
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System Identificat 10 1712 1110 1922	ors 613 ion Technique	586		1960	900 mil
System Identificat	613 on Technique	586		Aug Will	
10 1712 1110 1922	on Technique	586		Testing Apparatus	
10 1712 1110 1922				Testing Apparatus	
10 1712 1110 1922					
1110 1922	914 915			use Test Equipm	nent and Instrumentation
			719		
1140 1982				Testing Equipment	
				use Test Equipn	nent and Instrumentation
				Tastina Instrument	
				Testing Instrumentation	nent and Instrumentation
	•т•			use Test Equipm	nent and instrumentation
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ibration Absorpt	ion (m	arenai	•)		1977			Vibrati	ion m	оши	, mig					2168	
ibration Analyze	rs							Vibrati	ion R	educt	ion						
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			1715					1920	891		1903		1195	2036	187	628	18
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								2060						1616	517		
iscoelastic Dampir	ng				1	away.									1417	1618	2049
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	633	1364	765				259	1390									
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Abstract Numbers:	1-198	199-395	396-550	551-710	711-902	903-1101	1102-1287	1288-1487	1488-1700	1701-1887	1888-2124	2125-2287
Volume 1	1											
Isaue:	1	2	3	4	5	6	7	8		10	11	12

# **TECHNICAL NOTES**

B.R. Mace

The Evaluation of Infinite Sums with Special Reference to the Response of a Simply Supported Beam

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Pulse Response of a Non-Linear System

J. Sound Vib., <u>63</u> (4), pp 593-596 (Apr 22, 1979) 1 fig, 7 refs

A. Michalke and U. Michel

Relation Between Static and In-Flight Directivities of Jet Noise

J. Sound Vib., <u>63</u> (4), pp 602-605 (Apr 22, 1979) 3 figs, 3 refs

A Brot

A Dynamic Analysis of Landing Impact

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Remarks on the Stability of Flexible Rods Under Follower Forces

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G.J. Erickson

Some Frequencies of Underwater Noise Produced by Fishing Boats Affecting Albacore Catch

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Simulating System Dynamics in APL

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Free Vibration of Circular Rings on Radial Supports

J. Sound Vib., <u>65</u> (2), pp 297-301 (July 22, 1979) 1 fig, 1 table, 3 refs

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Aerospace Meeting [SAE] Los Angeles, CA (SAE Meeting Dept.)

2-7 Winter Annual Meeting [ASME] Statler Hilton, New York, NY (ASME Hg.)

#### JANUARY 1980

22-24 Reliability & Maintainability Symposium, San Francisco, CA (ASME Hq.)

#### **FEBRUARY 1980**

- 3-7 Energy Technology Conference and Exhibition [ASME] New Orleans, LA (ASME Hq.)
- 19 Current Techniques in Vibration Measurement and Recording [SEE] London, England (SEE Hq.)
- 26-29 Congress & Exposition [SAE] Cobo Hall, Detroit, MI (SAE Meeting Dept.)

#### **MARCH 1980**

- 9-13 25th Annual International Gas Turbine Conference and Exhibit [ASME] New Orleans, LA (ASME Hq.)
- 24-27 Design Engineering Conference and Show [ASME]
  McCormick Place, Chicago, IL (ASME Hq.)

#### **APRIL 1980**

21-25 Acoustical Society of America, Spring Meeting [ASA] Atlanta, GA (ASA Hg.)

#### MAY 1980

5-8 Offshore Technology Conference, Astrohall, Houston, TX (ASME Hq.)

- 19-23 Fourth International Conference on Pressure
  Vessel Technology [ASME] London, England
  (ASME Hg.)
- 25-30 Fourth SESA International Congress on Experimental Mechanics [SESA] The Copley Plaza, Boston, MA (SESA Hq.)

#### **JUNE 1980**

- 11 Experimental Techniques for Fatigue Crack Growth Measurement [SEE] British Rail Technical Centre (SEE Hq.)
- 17-19 International Conference on Vibrations in Rotating Machinery [ASME] Cambridge, England (ASME Hq.)
- 22-26 Summer Annual Meeting [ASME] Waldorf-Astoria, New York, NY (ASME Hq.)

#### **JULY 1980**

7-11 Recent Advances in Structural Dynamics Symp., [Institute of Sound and Vibration Research] University of Southampton, Southampton, S09 5NH, UK (Mrs. O.G. Hyde, ISVR Conference Secretary, The University, Southampton, S09 5NH, UK - Tel (0703) 559122, Ext 2310)

#### OCTOBER 1980

6-8 Computational Methods in Nonlinear Structural and Solid Mechanics [George Washington University & NASA Langley Research Center ] Washington, D.C. (Professor A.K. Noor, The George Washington University, NASA Langley Research Center, MS246, Hampton, VA 23665- Tel (804) 827-2897)

#### **NOVEMBER 1980**

18-21 Acoustical Society of America, Fall Meeting [ASA] Los Angeles, CA (ASA Hq.)

## CALENDAR ACRONYM DEFINITIONS AND ADDRESSES OF SOCIETY HEADQUARTERS

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AFIPS:	American Federation of Information Processing Societies	IEEE:	Institute of Electrical and Electronics Engineers
	210 Summit Ave., Montvale, NJ 07645		345 E. 47th St.
ACMA.			New York, NY 10017
AGMA:	American Gear Manufacturers Association		
	1330 Mass. Ave., N.W. Washington, D.C.	IES:	Institute of Environmental Sciences
	washington, D.C.		940 E. Northwest Highway
AHS:	American Helicopter Society		Mt. Prospect, IL 60056
	1325 18 St. N.W.	IET-MAA.	
	Washington, D.C. 20036	IFToMM:	International Federation for Theory of
			Machines and Mechanisms U.S. Council for TMM
AIAA:	American Institute of Aeronautics and		c/o Univ. Mass., Dept. ME
	Astronautics, 1290 Sixth Ave.		Amherst, MA 01002
	New York, NY 10019		Annerst, WA 01002
		INCE:	Institute of Noise Control Engineering
AIChE:	American Institute of Chemical Engineers		P.O. Box 3206, Arlington Branch
	345 E. 47th St.		Poughkeepsie, NY 12603
	New York, NY 10017		
4554		ISA:	Instrument Society of America
AREA:	American Railway Engineering Association		400 Stanwix St.
	59 E. Van Buren St.		Pittsburgh, PA 15222
	Chicago, IL 60605		
ARPA:	Advanced Research Projects Asses	ONR:	Office of Naval Research
	Advanced Research Projects Agency		Code 40084, Dept. Navy
ASA:	Acoustical Society of America		Arlington, VA 22217
	335 E. 45th St.	SAE:	Society of Automotive Engineers
	New York, NY 10017	JAL.	400 Commonwealth Drive
			Warrendale, PA 15096
ASCE:	American Society of Civil Engineers		77477677416,774 13030
	345 E. 45th St.	SEE:	Society of Environmental Engineers
	New York, NY 10017		6 Conduit St.
			London W1R 9TG, UK
ASME:	American Society of Mechanical Engineers		
	345 E. 45th St.	SESA:	Society for Experimental Stress Analysis
	New York, NY 10017		21 Bridge Sq.
ASNT:	American Carles for No. 1		Westport, CT 06880
7514).	American Society for Nondestructive Testing 914 Chicago Ave.		
	Evanston, IL 60202	SNAME:	Society of Naval Architects and Marine
	274131011, 12 00202		Engineers
ASQC:	American Society for Quality Control		74 Trinity Pl.
	161 W. Wisconsin Ave.		New York, NY 10006
	Milwaukee, WI 53203	SPE:	Seeint of December 5
		Src.	Society of Petroleum Engineers 6200 N. Central Expressway
ASTM:	American Society for Testing and Materials		Dallas, TX 75206
	1916 Race St.		Dallas, 1 × 75206
	Philadelphia, PA 19103	SVIC:	Shock and Vibration Information Center
			Naval Research Lab., Code 8404
CCCAM:	Chairman, c/o Dept. ME, Univ. Toronto,		Washington, D.C. 20375
	Toronto 5, Ontario, Canada		
		URSI-USNC	: International Union of Radio Science -
ICF:	International Congress on Fracture		U.S. National Committee
	Tohoku Univ.		c/o MIT Lincoln Lab.
	Sendai, Japan		Lexington, MA 02173

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